



COMUNE DI CANCELLO ED ARNONE
PROVINCIA DI CASERTA

**LAVORI DI “RISTRUTTURAZIONE E ADEGUAMENTO SISMICO DI
MIGLIORAMENTO E MESSA IN SICUREZZA DELLA SCUOLA DELL’INFANZIA
DI VIA SETTEMBRINI DELL’ISTITUTO COMPRENSIVO STATALE “U.
FOSCOLO” DI CANCELLO ED ARNONE (CE)”**
(C.U.P.) : E11E16000060003 (C.I.G.) : 6559280915



PROGETTO ESECUTIVO - POST GARA -

ELABORATO :

RELAZIONE GEOTECNICA E SULLE FONDAZIONI

RAPP:

TAV. ST-C

IMPRESA APPALTATRICE:

DITTA FABIANA COSTRUZIONI SRL

IL PROGETTISTA:

Dr. ing. Francesco COLARULLO



Data: GENNAIO 2018

COMUNE DI CANCELLO ARNONE

PROVINCIA DI CASERTA



LAVORI DI RISTRUTTURAZIONE E ADEGUAMENTO SISMICO DI MIGLIORAMENTO E MESSA IN SICUREZZA DELLA SCUOLA DELL'INFANZIA DI VIA SETTEMBRINI DELL'ISTITUTO COMPRENSIVO STATALE "U. FOSCOLO"

PROGETTO ESECUTIVO OPERE MIGLIORATIVE

PROGETTO STRUTTURALE EDIFICIO SCOLASTICO

RELAZIONE GEOTECNICA E SULLE FONDAZIONI

Caratteristiche del terreno

Terreno1- Cost.Winkler=2.00 kg/cm2 Falda assente										
Strato n°	Spessore	γ	γ_{Sat}	ϕ	Addensato	OCR	Coesione	Cu	E	v
	cm	kg/mc	kg/mc	°			kg/cmq	kg/cmq	kg/cmq	
1	520	1600	1600	24	No	--	0.02	0.00	1E02	0.30
2	2480	1600	1600	30	No	--	0.10	0.00	2E02	0.30

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
	Coordinate [mm]			Vincoli						
1	0	0	0	1	1	0	0	0	1	0
2	5451	0	0	1	1	0	0	0	1	0
3	11051	-10	0	1	1	0	0	0	1	0
4	16571	28	0	1	1	0	0	0	1	0
5	22251	41	0	1	1	0	0	0	1	0
6	27866	70	0	1	1	0	0	0	1	0
7	34151	14	0	1	1	0	0	0	1	0
8	39520	23	0	1	1	0	0	0	1	0
9	46158	18	0	1	1	0	0	0	1	0
10	0	5204	0	1	1	0	0	0	1	0
11	5601	5194	0	1	1	0	0	0	1	0
12	11201	5194	0	1	1	0	0	0	1	0
13	16801	5212	0	1	1	0	0	0	1	0
14	22401	5245	0	1	1	0	0	0	1	0
15	28016	5274	0	1	1	0	0	0	1	0
16	34301	5218	0	1	1	0	0	0	1	0
17	39820	5227	0	1	1	0	0	0	1	0
18	46458	5222	0	1	1	0	0	0	1	0
19	0	10355	0	1	1	0	0	0	1	0
20	5496	10345	0	1	1	0	0	0	1	0
21	11351	10495	0	1	1	0	0	0	1	0
22	16951	10513	0	1	1	0	0	0	1	0
23	23127	10357	0	1	1	0	0	0	1	0
24	27994	10357	0	1	1	0	0	0	1	0
25	34151	10369	0	1	1	0	0	0	1	0
26	39520	10378	0	1	1	0	0	0	1	0
27	46158	10373	0	1	1	0	0	0	1	0
28	22021	12018	0	1	1	0	0	0	1	0
29	27398	13782	0	1	1	0	0	0	1	0
30	12117	16043	0	1	1	0	0	0	1	0
31	24627	16506	0	1	1	0	0	0	1	0
32	31556	16367	0	1	1	0	0	0	1	0
33	8703	18174	0	1	1	0	0	0	1	0
34	14809	18674	0	1	1	0	0	0	1	0
35	17739	20623	0	1	1	0	0	0	1	0
36	24558	20427	0	1	1	0	0	0	1	0
37	26918	20495	0	1	1	0	0	0	1	0
38	12262	22144	0	1	1	0	0	0	1	0

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Alt. sup.	Base sup.	Alt. inf.	Base inf.	Larg.mag.
T		cm	cm	cm	cm	cm
	T100	50	40	40	100	120

Aste - Geometria e vincoli

9001	33	30	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8586	0	0	0	-0	0	0	Fond.	402	402
9002	5	14	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	521	521
9002	14	23	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	516	516
9003	1	10	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	520	520
9003	10	19	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	515	515
9004	19	20	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	550	550
9004	20	21	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	586	586
9004	21	22	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9004	22	23	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	618	618
9004	23	24	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	487	487
9004	24	25	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	616	616
9004	25	26	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	537	537
9004	26	27	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	664	664
9005	2	11	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	520	520
9005	11	20	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	515	515
9006	33	38	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	533	533
9007	23	28	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	200	200
9007	28	35	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	961	961
9008	35	36	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8685	0	-0	0	0	0	0	Fond.	682	682
9008	36	37	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	236	236
9009	7	16	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	521	521

9009	16	25	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	515	515
9010	10	11	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9010	11	12	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9010	12	13	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9010	13	14	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9010	14	15	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	562	562
9010	15	16	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	629	629
9010	16	17	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	552	552
9010	17	18	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	664	664
9011	3	12	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	521	521
9011	12	21	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	530	530
9011	21	30	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9012	1	2	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	545	545
9012	2	3	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	560	560
9012	3	4	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	552	552
9012	4	5	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	568	568
9012	5	6	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	562	562
9012	6	7	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	629	629
9012	7	8	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	537	537
9012	8	9	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	664	664
9013	34	38	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	430	430
9014	31	35	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	802	802
9014	29	31	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	389	389
9015	30	34	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8584	0	0	0	0	0	0	Fond.	376	376
9015	34	35	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8486	0	0	0	-0	-0	0	Fond.	352	352
9016	4	13	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	519	519
9016	13	22	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	530	530
9016	22	35	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	Fond.	1014	1014

						CLS_Travi Fondazion e												
9017	25	32	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	654	654
9018	28	31	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8785	0	-0	0	0	0	0	0	Fond.	519	519
9019	31	36	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8580	0	0	0	-0	-1	0	0	Fond.	392	392
9020	20	33	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8885	0	0	0	0	0	0	0	Fond.	846	846
9021	32	37	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	621	621
9022	8	17	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	521	521
9022	17	26	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	516	516
9023	31	32	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	693	693
9024	6	15	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	521	521
9024	15	24	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	508	508
9024	24	29	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	348	348
9025	9	18	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8587	0	0	0	-15	-1	0	0	Fond.	521	521
9025	18	27	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8788	0	1	0	0	-0	0	0	Fond.	516	516
9026	22	28	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	529	529
9026	28	29	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	566	566
9026	29	32	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8580	0	0	0	-0	-0	0	0	Fond.	490	490
9027	22	30	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	734	734
9028	22	34	I-I	T100	C25/30	CLS_Travi Fondazion e	0	8585	0	0	0	0	0	0	0	Fond.	844	844

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo : Set_NT_SLV_SLD_A2_STR/GEO

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
			kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq
9001	33	30	0.48(2)	0.48(2)	0.48(2)	0.48(2)	0.48(2)	0.48(2)
9002	14	23	0.52(2)	0.51(2)	0.50(2)	0.50(2)	0.50(2)	0.50(2)
9002	5	14	0.50(2)	0.48(2)	0.48(2)	0.48(2)	0.50(2)	0.52(2)
9003	1	10	0.51(2)	0.48(2)	0.47(2)	0.47(2)	0.48(2)	0.49(2)
9003	10	19	0.49(2)	0.49(2)	0.49(2)	0.50(2)	0.51(2)	0.53(2)
9004	22	23	0.52(2)	0.50(2)	0.48(2)	0.48(2)	0.49(2)	0.50(2)
9004	21	22	0.53(2)	0.52(2)	0.51(2)	0.50(2)	0.51(2)	0.52(2)
9004	20	21	0.50(2)	0.50(2)	0.50(2)	0.51(2)	0.52(2)	0.53(2)
9004	23	24	0.50(2)	0.50(2)	0.50(2)	0.50(2)	0.50(2)	0.51(2)
9004	26	27	0.49(2)	0.48(2)	0.46(2)	0.46(2)	0.49(2)	0.54(2)

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
9004	24	25	0.51(2)	0.49(2)	0.48(2)	0.48(2)	0.49(2)	0.50(2)
9004	25	26	0.50(2)	0.50(2)	0.49(2)	0.49(2)	0.49(2)	0.49(2)
9004	19	20	0.52(2)	0.49(2)	0.47(2)	0.47(2)	0.49(2)	0.50(2)
9005	2	11	0.48(2)	0.46(2)	0.46(2)	0.47(2)	0.49(2)	0.51(2)
9005	11	20	0.51(2)	0.52(2)	0.51(2)	0.51(2)	0.50(2)	0.49(2)
9006	33	38	0.48(2)	0.48(2)	0.48(2)	0.49(2)	0.51(2)	0.53(2)
9007	23	28	0.50(2)	0.50(2)	0.50(2)	0.49(2)	0.49(2)	0.48(2)
9007	28	35	0.48(2)	0.41(2)	0.35(2)	0.34(2)	0.39(2)	0.49(2)
9008	36	37	0.47(2)	0.48(2)	0.49(2)	0.50(2)	0.51(2)	0.52(2)
9008	35	36	0.51(2)	0.48(2)	0.46(2)	0.45(2)	0.46(2)	0.47(2)
9009	16	25	0.53(2)	0.52(2)	0.52(2)	0.51(2)	0.50(2)	0.50(2)
9009	7	16	0.50(2)	0.49(2)	0.48(2)	0.49(2)	0.51(2)	0.53(2)
9010	15	16	0.52(2)	0.51(2)	0.50(2)	0.50(2)	0.51(2)	0.53(2)
9010	12	13	0.53(2)	0.53(2)	0.52(2)	0.52(2)	0.53(2)	0.54(2)
9010	16	17	0.53(2)	0.52(2)	0.52(2)	0.51(2)	0.51(2)	0.51(2)
9010	10	11	0.48(2)	0.47(2)	0.47(2)	0.48(2)	0.50(2)	0.52(2)
9010	13	14	0.54(2)	0.53(2)	0.52(2)	0.51(2)	0.52(2)	0.52(2)
9010	17	18	0.51(2)	0.48(2)	0.45(2)	0.44(2)	0.46(2)	0.51(2)
9010	11	12	0.52(2)	0.52(2)	0.51(2)	0.51(2)	0.52(2)	0.53(2)
9010	14	15	0.52(2)	0.51(2)	0.51(2)	0.51(2)	0.52(2)	0.52(2)
9011	3	12	0.49(2)	0.48(2)	0.48(2)	0.49(2)	0.51(2)	0.53(2)
9011	21	30	0.53(2)	0.50(2)	0.48(2)	0.47(2)	0.48(2)	0.49(2)
9011	12	21	0.53(2)	0.53(2)	0.53(2)	0.53(2)	0.53(2)	0.53(2)
9012	4	5	0.49(2)	0.48(2)	0.47(2)	0.48(2)	0.49(2)	0.50(2)
9012	2	3	0.48(2)	0.48(2)	0.47(2)	0.47(2)	0.48(2)	0.50(2)
9012	1	2	0.51(2)	0.49(2)	0.48(2)	0.47(2)	0.48(2)	0.48(2)
9012	8	9	0.49(2)	0.46(2)	0.45(2)	0.46(2)	0.50(2)	0.57(2)
9012	6	7	0.50(2)	0.48(2)	0.47(2)	0.47(2)	0.48(2)	0.50(2)
9012	7	8	0.50(2)	0.50(2)	0.50(2)	0.50(2)	0.49(2)	0.49(2)
9012	3	4	0.50(2)	0.49(2)	0.49(2)	0.49(2)	0.49(2)	0.49(2)
9012	5	6	0.50(2)	0.50(2)	0.49(2)	0.49(2)	0.50(2)	0.50(2)
9013	34	38	0.46(2)	0.47(2)	0.49(2)	0.50(2)	0.52(2)	0.54(2)
9014	31	35	0.44(2)	0.42(2)	0.40(2)	0.40(2)	0.44(2)	0.51(2)
9014	29	31	0.47(2)	0.46(2)	0.45(2)	0.45(2)	0.44(2)	0.44(2)
9015	30	34	0.49(2)	0.48(2)	0.47(2)	0.47(2)	0.47(2)	0.47(2)
9015	34	35	0.47(2)	0.47(2)	0.48(2)	0.48(2)	0.50(2)	0.51(2)
9016	4	13	0.49(2)	0.48(2)	0.48(2)	0.49(2)	0.51(2)	0.53(2)
9016	13	22	0.53(2)	0.54(2)	0.53(2)	0.53(2)	0.52(2)	0.49(2)
9016	22	35	0.49(2)	0.40(2)	0.34(2)	0.33(2)	0.39(2)	0.50(2)
9017	25	32	0.49(2)	0.46(2)	0.44(2)	0.43(2)	0.44(2)	0.45(2)
9018	28	31	0.48(2)	0.46(2)	0.44(2)	0.44(2)	0.44(2)	0.44(2)
9019	31	36	0.44(2)	0.44(2)	0.44(2)	0.44(2)	0.45(2)	0.47(2)
9020	20	33	0.49(2)	0.45(2)	0.42(2)	0.41(2)	0.44(2)	0.48(2)
9021	32	37	0.45(2)	0.45(2)	0.45(2)	0.46(2)	0.48(2)	0.52(2)
9022	8	17	0.49(2)	0.48(2)	0.48(2)	0.49(2)	0.50(2)	0.52(2)
9022	17	26	0.52(2)	0.51(2)	0.49(2)	0.49(2)	0.49(2)	0.49(2)
9023	31	32	0.44(2)	0.43(2)	0.42(2)	0.42(2)	0.43(2)	0.45(2)
9024	6	15	0.49(2)	0.48(2)	0.48(2)	0.49(2)	0.51(2)	0.52(2)
9024	24	29	0.50(2)	0.50(2)	0.49(2)	0.48(2)	0.47(2)	0.47(2)
9024	15	24	0.52(2)	0.52(2)	0.51(2)	0.51(2)	0.51(2)	0.50(2)
9025	18	27	0.53(2)	0.51(2)	0.51(2)	0.51(2)	0.53(2)	0.55(2)
9025	9	18	0.59(2)	0.55(2)	0.53(2)	0.52(2)	0.53(2)	0.53(2)
9026	28	29	0.49(2)	0.48(2)	0.47(2)	0.47(2)	0.47(2)	0.47(2)
9026	22	28	0.51(2)	0.50(2)	0.48(2)	0.48(2)	0.49(2)	0.49(2)
9026	29	32	0.47(2)	0.46(2)	0.44(2)	0.43(2)	0.43(2)	0.44(2)
9027	22	30	0.51(2)	0.46(2)	0.42(2)	0.42(2)	0.45(2)	0.48(2)
9028	22	34	0.50(2)	0.42(2)	0.38(2)	0.37(2)	0.41(2)	0.46(2)

VERIFICHE STATO LIMITE ULTIMO

Verifica delle travi

Scenario di calcolo : Set_NT_SLV_SLD_A2_STR/GEO

Simbologia:

L[cm] :Lunghezza teorica elemento (distanza tra i nodi)

Ln[cm] :Lunghezza netta elemento (tiene conto dei conci rigidi)

Terreno :Nome della stratigrafia per travi Winkler

L2,L3[cm] :Lunghezze libere di inflessione

Sez. R :Sezione Rettangolare

By[cm] :Larghezza (asse locale y)

Bz[cm] :Larghezza (asse locale z)

Sez. T : Sezione a T (rovescia e non)

Ba[cm] :Larghezza base inferiore

Ha[cm] :Altezza inferiore

Bs[cm] :Larghezza superiore

Hs[cm] :Altezza superiore

Sez. L : Sezione ad L (rovescia e non)

Ba[cm] :Larghezza base inferiore

Ha[cm] :Altezza inferiore

Bs[cm] :Larghezza superiore

Hs[cm] :Altezza superiore

Sez. C : Sezione circolare

R[cm] :Raggio

Criterio : Criterio di verifica adottato

X[cm] : Punto di verifica

ILN : Inizio luce netta

CAMP : rappresenta il punto di massimo momento sia superiore che inferiore ad esclusione degli estremi

FLN :Fine luce netta

M-[kg*m]⁽¹⁾ : Momento negativo massimo di calcolo

N-[kg] : Sforzo normale corrispondente ad M-

M+[kg*m]⁽¹⁾ : Momento positivo massimo di calcolo

N+[kg] : Sforzo normale corrispondente ad M+

ΔM-[kg*m] : Incremento di M- per la traslazione del diagramma del momento a causa del taglio

ΔM+[kg*m] : Incremento di M+ per la traslazione del diagramma del momento a causa del taglio

Afs[cmq] : Area di ferro superiore

Afi[cmq] : Area di ferro inferiore

εc^- : Deformazione nel cls per effetto di $M^-:N^-$ (⁴)
 εc^+ : Deformazione nel cls per effetto di $M^+:N^+$ (⁴)
 εf^- : Deformazione nell'acciaio per effetto di $M^-:N^-$ (⁴)
 εf^+ : Deformazione nell'acciaio per effetto di $M^+:N^+$ (⁴)
 C^- : Combinazione di carico generatore di $M^-:N^-$
 C^+ : Combinazione di carico generatore di $M^+:N^+$

$x-[cm]$ (⁵) : profondità asse neutro per la combinazione C^-
 $d-[cm]$ (⁶) : altezza utile della sezione per la combinazione C^-
 $x+[cm]$ (⁵) : profondità asse neutro per la combinazione C^+
 $d+[cm]$ (⁶) : altezza utile della sezione per la combinazione C^+
 $M_r-[kg*m]$: Momento resistente superiore
 $M_r+[kg*m]$: Momento resistente inferiore
 $Stato-(^7)$: Stato della sezione per la combinazione C^-
 $Stato+(^7)$: Stato della sezione per la combinazione C^+

Comb: Combinazione di Carico individuata dal codice [C] se Comb è non sismica, ovvero [(C_x+C_y) C_m S_c] se Comb è sismica.

- C individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- C_x individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- C_y individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- C_m individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni sisma in

Spostamento masse impalcato);

- S_c individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):

- 1) $S_c = + SismaZ*f_z + SismaX*f_x + SismaY*f_y$
- 2) $S_c = + SismaZ*f_z + SismaX*f_x - SismaY*f_y$
- 3) $S_c = + SismaZ*f_z - SismaX*f_x + SismaY*f_y$
- 4) $S_c = + SismaZ*f_z - SismaX*f_x - SismaY*f_y$.
- 1) $S_c = - SismaZ*f_z + SismaX*f_x + SismaY*f_y$
- 2) $S_c = - SismaZ*f_z + SismaX*f_x - SismaY*f_y$
- 3) $S_c = - SismaZ*f_z - SismaX*f_x + SismaY*f_y$
- 4) $S_c = - SismaZ*f_z - SismaX*f_x - SismaY*f_y$.

- Quando non è richiesto il contributo del sisma in direzione Z le ultime quattro sono assenti

Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).

Sez : Sezione di verifica [Sinistra/Destra]

$Td[kg](^2)$: Taglio di verifica

$VR_{dns}[kg]$: Resistenza a taglio in assenza di armature

$VR_{cd}[kg]$: Resistenza taglio-compressione calcestruzzo

$VR_{sd}[kg]$: Resistenza taglio-trazione acciaio

$VR_d[kg]$: Resistenza a taglio = $\min(VR_{cd}, VR_{sd})$

$VR_{d,f}[kg]$: Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006)

$M_t[kg*m]$: Momento torcente

$Tpl[kg]$: Taglio dovuto ai momenti resistenti alle estremità della trave

$M_r[kg*m]$: Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto

$Dx[cm]$: Distanza dall'estremo da armare con staffe

Staffe[cmq] : Area delle staffe

$\cot(\theta)$: cotangente teta secondo il punto 4.1.2.1.3 delle Norme Tecniche

$F.Parete[cmq](^3)$: Area armatura longitudinale di parete

Simbologia verifica travi collegamento:

Comb : Combinazione più gravosa

$N_{sd}[kg]$: Azione verticale negli elementi collegati, nella combinazione specificata

α : Coefficiente in funzione della classe di terreno (NTC 7.2.5.1)

a/g : Punto di aggancio dello spettro di accelerazione ($a/g=S_a(0)$)

N : Sforzo normale di verifica $N=\alpha*N_{sd}*a/g$

$A_f[cmq]$: Area di ferro complessiva nella sezione

$NR_d C[kg]$: Resistenza a compressione della sezione

NRd T[kg] : Resistenza a trazione della sezione

Fatt.Ampl.Sisma = fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)

Cs : Coefficiente di sicurezza definito dal rapporto F_r/F_d (F_r =resistenza, F_d =azione)

Css : Coefficiente di sicurezza sismico definito rapporto $(F_r-F_v)/F_dE$ (F_r =resistenza, F_v =azione per carichi verticali, F_dE =azione sismica)

Note Verifica travi:

(¹): il valore del momento di verifica è dato da $M + \Delta M$

(²): T_d è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di T_{pl} ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di struttura

(³): armatura necessaria per la sola verifica a torsione

(⁴): le deformazioni sono stampate a meno del fattore 10^{-3}

(⁵) : distanza tra la fibra di cls compressa piu' lontana e l'asse neutro in direzione ortogonale all'asse neutro

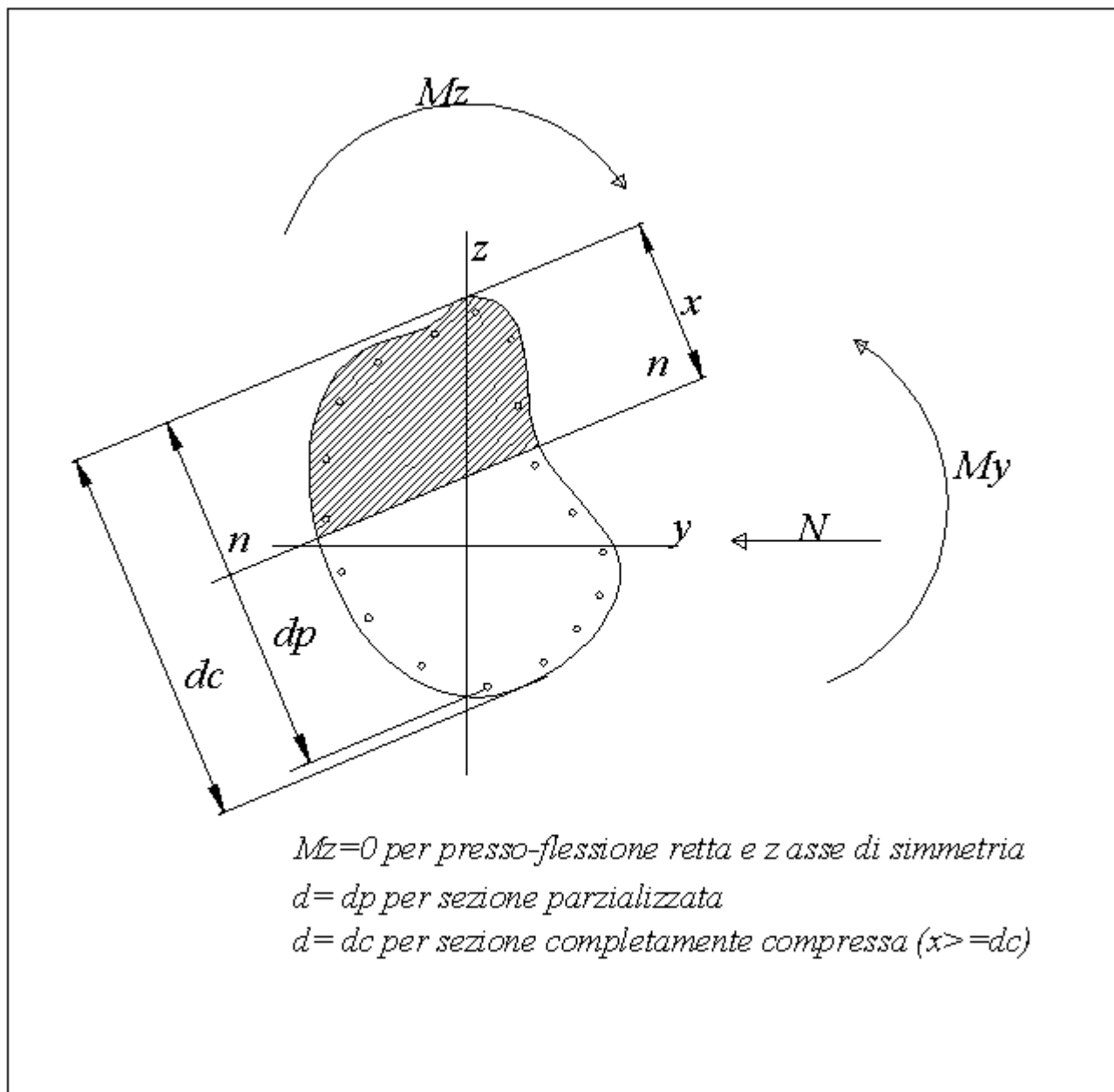
(⁶) : distanza tra le fibre sollecitate piu' lontane dall'asse neutro:

nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso piu lontane da n-n

nel caso di sezione completamente compressa le due fibre sono le due di cls compresso piu lontane da n-n

(⁷) : Indica lo stato della sezione se: completamente compressa (Compr.),completamente tesa (Tesa), parzializzata (Parz.)

Schema geometrico verifica della sezione



Trave di Fond. : 9001 [33 , 30] Pilastrate [33 , 30]

Sez. T: $Ba=100.0$ cm $Ha=40.0$ cm $Bs=40.0$ cm $Hs=50.0$ cm $L=402.4$ cm $Ln=404.7$ cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10118	4317	--	--	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	3.9
40.5	9388	3593	697	692	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	4.0
CAMP	8314	6668	1026	2986	12.57	14.83	39929	45945	(3+4)-V-3		4.3
364.2	--	9795	--	3414	12.57	14.83	39929	45945	1	2	3.5
FLN	--	13369	--	--	12.57	14.83	39929	45945	1	2	3.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
40.5	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.
CAMP	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-V-3	2	Parz.	Parz.
364.2	--	--	--	23.1	85.9	0.269	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.1	85.9	0.269	39929	45945	1	2	--	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-V-3 Cen=(5+6)-V-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3064	--	75231	76031	75231	0	45945	90.0	10.05	25
Cen	6658	--	75231	47519	47519	--	--	--	6.28	7.1
Des	9576	--	75231	76031	75231	0	39929	90.0	10.05	7.9

Trave di Fond. : 9002 [5 , 14] Pilastrate [5 , 14]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=520.6 cm Ln=535.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3967	1902	647	--	12.57	14.83	39929	45945	(3+4)-VI-4	(3+4)-VI-1	8.7
53.5	4863	102	254	1300	12.57	14.83	39929	45945	(3+4)-VI-4	(3+4)-VI-1	7.8
CAMP	5697	3095	--	2277	12.57	14.83	39929	45945	2	(3+4)-VI-4	7.0
481.9	526	6249	963	2659	12.57	14.83	39929	45945	(3+4)-VI-1	(3+4)-VI-4	5.2
FLN	-1277	9932	1302	--	12.57	14.83	39929	45945	(3+4)-VI-1	(3+4)-VI-4	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VI-4	(3+4)-VI-1	Parz.	Parz.
53.5	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VI-4	(3+4)-VI-1	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VI-4	Parz.	Parz.
481.9	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VI-1	(3+4)-VI-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VI-1	(3+4)-VI-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4663	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	5870	--	75231	47519	47519	--	--	--	6.28	8.1
Des	8789	--	75231	76031	75231	0	39929	90.0	10.05	8.6

Trave di Fond. : 9002 [14 , 23] Pilastrate [14 , 23]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=516.3 cm Ln=503.9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-435	11925	1149	--	12.57	14.83	39929	45945	(3+4)-VI-4	(3+4)-VI-1	3.9
50.4	1062	8542	766	2595	12.57	14.83	39929	45945	(3+4)-VI-4	(3+4)-VI-1	4.1
CAMP	2742	5658	--	2212	12.57	14.83	39929	45945	(3+4)-VI-4	(3+4)-VI-1	5.8
453.5	2374	3104	22	1906	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	9.2
FLN	1885	5588	375	--	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.268	39929	45945	(3+4)-VI-4	(3+4)-VI-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
50.4	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VI-4	(3+4)-VI-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VI-4	(3+4)-VI-1	Parz.	Parz.
453.5	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.
FLN	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=(5+6)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8646	--	75231	76031	75231	0	45945	90.0	10.05	8.7
Cen	5381	--	75231	47566	47566	--	--	--	6.29	8.8
Des	5379	--	75231	76031	75231	0	39929	90.0	10.05	14

Trave di Fond. : 9003 [1 , 10] Pilastrate [1 , 10]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=520.4 cm Ln=535.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5942	4510	--	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	6.7
53.6	6789	2200	--	1667	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	5.9
CAMP	7026	4512	--	2598	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-IV-2	5.7
482.0	7027	8112	--	2949	12.57	14.83	39929	45945	(3+4)-IV-3	(3+4)-IV-2	4.2
FLN	6684	12207	247	--	12.57	14.83	39929	45945	(3+4)-IV-3	(3+4)-VIII-2	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
53.6	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
CAMP	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-IV-2	Parz.	Parz.
482.0	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-IV-3	(3+4)-IV-2	Parz.	Parz.
FLN	14.9	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-IV-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-I-3 Cen=(5+6)-VIII-2 Des=(5+6)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5754	--	75231	76031	75231	0	45945	90.0	10.05	13
Cen	6458	--	75231	47519	47519	--	--	--	6.28	7.4
Des	8293	--	75231	76031	75231	0	39929	90.0	10.05	9.1

Trave di Fond. : 9003 [10 , 19] Pilastrate [10 , 19]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=515.1 cm Ln=500.3 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3923	13066	405	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	3.5
50.0	4448	9166	104	3013	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	3.8
CAMP	5249	5742	--	2646	12.57	14.83	39929	45945	(3+4)-IV-3	(3+4)-VIII-1	5.5
450.3	4978	3364	203	1626	12.57	14.83	39929	45945	(3+4)-IV-3	(3+4)-IV-2	7.7
FLN	4141	5567	647	--	12.57	14.83	39929	45945	(3+4)-IV-3	(3+4)-VIII-4	8.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
50.0	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-IV-3	(3+4)-VIII-1	Parz.	Parz.
450.3	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-IV-3	(3+4)-IV-2	Parz.	Parz.
FLN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-IV-3	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-VIII-3 Cen=(5+6)-VIII-3 Des=(5+6)-VII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8536	--	75231	76031	75231	0	45945	90.0	10.05	8.8
Cen	6544	--	75231	47519	47519	--	--	--	6.28	7.3
Des	5461	--	75231	76031	75231	0	39929	90.0	10.05	14

Trave di Fond. : 9004 [19 , 20] Pilastrate [19 , 20]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=549.6 cm Ln=549.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7735	6652	543	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	4.8
55.0	8250	3997	316	1868	12.57	14.83	39929	45945	(3+4)-V-4	(3+4)-VII-1	4.7
CAMP	8700	1093	--	2187	12.57	14.83	39929	45945	(3+4)-V-4	(3+4)-VII-4	4.6
494.6	1202	4203	707	2561	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.8
FLN	-224	7844	1003	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	5.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
55.0	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-4	(3+4)-VII-1	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-V-4	(3+4)-VII-4	Parz.	Parz.
494.6	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-VIII-1 Cen=(5+6)-V-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6517	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	5546	--	75231	47519	47519	--	--	--	6.28	8.6
Des	7806	--	75231	76031	75231	0	39929	90.0	10.05	9.6

Trave di Fond. : 9004 [20 , 21] Pilastrate [20 , 21]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=585.7 cm Ln=555.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2754	8024	553	--	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	5.7
55.6	3548	5079	182	2050	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	6.4
CAMP	3810	5286	--	2324	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-VII-3	6.0
500.0	-238	8625	901	2729	12.57	14.83	39929	45945	(3+4)-VII-2	(3+4)-VII-3	4.0
FLN	--	12548	--	--	12.57	14.83	39929	45945	1	(3+4)-VII-3	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
55.6	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-VII-3	Parz.	Parz.
500.0	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-2	(3+4)-VII-3	Parz.	Parz.
FLN	--	--	--	23.1	85.9	0.269	39929	45945	1	(3+4)-VII-3	--	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6253	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	5691	--	75231	48197	48197	--	--	--	6.37	8.5
Des	8870	--	75231	76031	75231	0	39929	90.0	10.05	8.5

Trave di Fond. : 9004 [21 , 22] Pilastrate [21 , 22]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.0 cm Ln=560.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	475	10219	1028	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	4.5
56.0	1964	6619	660	2485	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	5.0
CAMP	3751	3620	--	2070	12.57	14.83	39929	45945	2	(3+4)-VII-1	8.1
504.0	2099	4239	489	2082	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	7.3
FLN	897	7254	830	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
56.0	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VII-1	Parz.	Parz.
504.0	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VII-1 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7857	--	75231	76031	75231	0	45945	90.0	10.05	9.6
Cen	4829	--	75231	47519	47519	--	--	--	6.28	9.8
Des	6486	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9004 [22 , 23] Pilastrate [22 , 23]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=617.8 cm Ln=647.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8212	--	--	12.57	14.83	39929	45945	1	(3+4)-VII-1	5.6
64.8	124	4626	929	2140	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	6.8
CAMP	4532	2244	--	1758	12.57	14.83	39929	45945	2	(3+4)-VII-4	8.8
582.8	1886	5188	746	2181	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.2
FLN	-8	8842	1131	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	5.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	(3+4)-VII-1	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
64.8	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VII-4	Parz.	Parz.
582.8	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7714	--	75231	76031	75231	0	45945	90.0	10.05	9.8
Cen	4556	--	75231	47519	47519	--	--	--	6.28	10
Des	7539	--	75231	76031	75231	0	39929	90.0	10.05	10.0

Trave di Fond. : 9004 [23 , 24] Pilastrate [23 , 24]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=486.7 cm Ln=486.7 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	87	8994	808	--	12.57	14.83	39929	45945	(3+4)-VII-3	(3+4)-VII-2	5.1
48.7	1105	6149	468	2260	12.57	14.83	39929	45945	(3+4)-VII-3	(3+4)-VII-2	5.5
CAMP	2096	3755	--	1901	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-2	8.1
438.0	1548	4676	383	1906	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	7.0
FLN	642	7075	720	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-3	(3+4)-VII-2	Parz.	Parz.
48.7	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-3	(3+4)-VII-2	Parz.	Parz.
CAMP	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-2	Parz.	Parz.
438.0	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-VII-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7142	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4496	--	75231	47519	47519	--	--	--	6.28	11
Des	5888	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9004 [24 , 25] Pilastrate [24 , 25]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=615.7 cm Ln=615.7 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-279	11295	1105	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	4.1
61.6	1480	7100	728	2633	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	4.7
CAMP	4384	3647	--	2168	12.57	14.83	39929	45945	2	(3+4)-VII-1	7.9
554.1	3083	4040	491	2007	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	7.6
FLN	1711	7237	861	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
61.6	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VII-1	Parz.	Parz.
554.1	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2 \cos = (5+6) - VII-1 \tan = 2$

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8645	--	75231	76031	75231	0	45945	90.0	10.05	8.7
Cen	5053	--	75231	47519	47519	--	--	--	6.28	9.4
Des	6538	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9004 [25 , 26] Pilastrate [25 , 26]

Sez. T: $Ba = 100.0 \text{ cm}$ $Ha = 40.0 \text{ cm}$ $Bs = 40.0 \text{ cm}$ $Hs = 50.0 \text{ cm}$ $L = 536.9 \text{ cm}$ $Ln = 536.9 \text{ cm}$ Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-454	9530	873	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	4.8
53.7	759	6400	511	2254	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	5.3
CAMP	2260	4089	--	1904	12.57	14.83	39929	45945	(3+4)-VII-2	(3+4)-VII-3	7.7
483.2	1600	6734	392	2272	12.57	14.83	39929	45945	(3+4)-VII-2	(3+4)-VII-3	5.1
FLN	624	9889	703	--	12.57	14.83	39929	45945	(3+4)-VII-2	(3+4)-VII-3	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
53.7	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-2	(3+4)-VII-3	Parz.	Parz.
483.2	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-2	(3+4)-VII-3	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-2	(3+4)-VII-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2 \cos = (5+6) - V-3 \tan = 2$

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7258	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4468	--	75231	48664	48664	--	--	--	6.43	11
Des	6487	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9004 [26 , 27] Pilastrate [26 , 27]

Sez. T: $Ba = 100.0 \text{ cm}$ $Ha = 40.0 \text{ cm}$ $Bs = 40.0 \text{ cm}$ $Hs = 50.0 \text{ cm}$ $L = 663.8 \text{ cm}$ $Ln = 663.8 \text{ cm}$ Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	10006	--	--	12.57	14.83	39929	45945	1	(3+4)-V-1	4.6
66.4	385	5073	1144	2873	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-1	5.8
CAMP	9399	900	--	2485	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-VII-1	4.2
597.4	8411	2936	386	2462	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-3	4.5
FLN	6167	7163	1194	--	12.57	14.83	39929	45945	(3+4)-V-1	(3+4)-VII-3	5.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	(3+4)-V-1	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
66.4	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-V-3	(3+4)-V-1	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-I-1	(3+4)-VII-1	Parz.	Parz.
597.4	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-3	Parz.	Parz.
FLN	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-V-1	(3+4)-VII-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2$ $\cos = (5+6)$ -I-1 $\tan = (5+6)$ -II-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9083	--	75231	76031	75231	0	45945	90.0	10.05	8.3
Cen	5812	--	75231	47519	47519	--	--	--	6.28	8.2
Des	7036	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9005 [2 , 11] Pilastrate [2 , 11]

Sez. T: $B_a = 100.0$ cm $H_a = 40.0$ cm $B_s = 40.0$ cm $H_s = 50.0$ cm $L = 519.6$ cm $L_n = 534.4$ cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6018	3505	335	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	6.3
53.4	6481	1450	--	1486	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	6.2
CAMP	6385	4763	70	2623	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-2	6.2
481.0	4061	8389	367	2995	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	4.0
FLN	3113	12530	686	--	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
53.4	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
CAMP	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-2	Parz.	Parz.
481.0	14.8	85.9	0.173	23.1	85.9	0.268	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2$ $\cos = (5+6)$ -VIII-2 $\tan = (5+6)$ -VIII-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4378	--	75231	76031	75231	0	45945	90.0	10.05	17
Cen	6301	--	75231	47519	47519	--	--	--	6.28	7.5
Des	8225	--	75231	76031	75231	0	39929	90.0	10.05	9.1

Trave di Fond. : 9005 [11 , 20] Pilastrate [11 , 20]

Sez. T: $B_a = 100.0$ cm $H_a = 40.0$ cm $B_s = 40.0$ cm $H_s = 50.0$ cm $L = 515.2$ cm $L_n = 500.1$ cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2381	13428	526	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	3.4
50.0	3061	10204	173	2492	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	3.6
CAMP	3285	7482	--	2104	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	4.8
450.1	--	6162	--	2347	12.57	14.83	39929	45945	1	2	5.4
FLN	--	9199	--	--	12.57	14.83	39929	45945	1	2	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
50.0	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
450.1	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2 \cos = (5+6)$ -VIII-3 $\tan = 2$

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7145	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4970	--	75231	47519	47519	--	--	--	6.28	9.6
Des	6706	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9006 [33 , 38] Pilastrate [33 , 38]

Sez. T: $B_a = 100.0 \text{ cm}$ $H_a = 40.0 \text{ cm}$ $B_s = 40.0 \text{ cm}$ $H_s = 50.0 \text{ cm}$ $L = 533.2 \text{ cm}$ $L_n = 544.2 \text{ cm}$ Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	9275	--	--	12.57	14.83	39929	45945	1	2	5.0
54.4	--	5191	--	2901	12.57	14.83	39929	45945	1	2	5.7
CAMP	6882	1800	--	2408	12.57	14.83	39929	45945	(3+4)-VIII-3	2	5.8
489.8	4338	2080	1496	1051	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-4	6.8
FLN	3554	3560	1277	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	8.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
54.4	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-3	2	Parz.	Parz.
489.8	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-3	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin = 2.500, \cot(\theta) \cos = 2.500, \cot(\theta) \tan = 2.500$

Comb $\sin = 2 \cos = 2 \tan = (5+6)$ -V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8254	--	75231	76031	75231	0	45945	90.0	10.05	9.1
Cen	5598	--	75231	47519	47519	--	--	--	6.28	8.5
Des	5621	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9007 [23 , 28] Pilastrate [23 , 28]

Sez. T: $B_a = 100.0 \text{ cm}$ $H_a = 40.0 \text{ cm}$ $B_s = 40.0 \text{ cm}$ $H_s = 50.0 \text{ cm}$ $L = 199.6 \text{ cm}$ $L_n = 202.4 \text{ cm}$ Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	3541	--	749	12.57	14.83	39929	45945	1	2	11
20.2	--	3882	--	952	12.57	14.83	39929	45945	1	2	9.5
CAMP	--	9206	--	2315	12.57	14.83	39929	45945	1	2	4.0
182.2	--	10372	--	1263	12.57	14.83	39929	45945	1	2	3.9
FLN	--	11635	--	--	12.57	14.83	39929	45945	1	2	3.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
20.2	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.
CAMP	--	--	--	23.1	85.9	0.268	39929	45945	1	2	--	Parz.
182.2	--	--	--	23.1	85.9	0.268	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.1	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6475	--	75231	77454	75231	0	45945	202.4	10.24	12
Des							39929			

Trave di Fond. : 9007 [28 , 35] Pilastrate [28 , 35]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=961.2 cm Ln=939.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	7585	--	--	12.57	14.83	39929	45945	1	2	6.1
93.9	657	2895	878	1824	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-VI-3	9.7
CAMP	9302	-414	--	1362	12.57	14.83	39929	45945	2	(3+4)-VI-3	4.3
845.1	6845	--	727	--	12.57	14.83	39929	45945	2	1	5.3
FLN	3520	--	1369	--	12.57	14.83	39929	45945	2	1	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
93.9	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-VI-3	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.8	85.9	0.266	39929	45945	2	(3+4)-VI-3	Parz.	Parz.
845.1	14.9	85.9	0.173	--	--	--	39929	45945	2	1	Parz.	--
FLN	14.8	85.9	0.173	--	--	--	39929	45945	2	1	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7261	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	5287	--	75231	47519	47519	--	--	--	6.28	9.0
Des	4796	--	75231	76031	75231	0	39929	90.0	10.05	16

Trave di Fond. : 9008 [35 , 36] Pilastrate [35 , 36]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=682.2 cm Ln=621.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3453	8388	536	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	5.5
62.1	4314	4605	181	2355	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	6.6
CAMP	7703	3876	45	2015	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	5.2
559.0	7776	7113	--	2389	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	4.8
FLN	7362	10952	258	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	4.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
62.1	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
559.0	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-VII-1 Cen=(5+6)-VII-3 Des=(5+6)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6821	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4784	--	75231	48171	48171	--	--	--	6.37	10
Des	7039	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9008 [36 , 37] Pilastrate [36 , 37]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=236.1 cm Ln=287.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	59	2873	1064	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-VI-2	16
28.8	853	2632	854	241	12.57	14.83	39929	45945	(3+4)-VI-3	(3+4)-VI-2	16
CAMP	2925	4425	--	944	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	8.6
259.0	2408	5113	417	746	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	7.8
FLN	1820	5859	713	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	7.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-VI-2	Parz.	Parz.
28.8	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-VI-3	(3+4)-VI-2	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
259.0	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-VIII-1 Cen=(5+6)-VIII-1 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4220	--	75231	76031	75231	0	45945	90.0	10.05	18
Cen	1908	--	75231	49404	49404	--	--	--	6.53	26
Des	3732	--	75231	76031	75231	0	39929	90.0	10.05	20

Trave di Fond. : 9009 [7 , 16] Pilastrate [7 , 16]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=520.6 cm Ln=535.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5236	3068	501	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	7.0
53.5	5929	1033	71	1469	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	6.7
CAMP	6028	4691	--	2650	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-2	6.3
481.9	2317	8361	691	3045	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	4.0
FLN	881	12579	1037	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
53.5	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-II-2	(3+4)-II-2	Parz.	Parz.
481.9	14.8	85.9	0.173	23.1	85.9	0.268	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-II-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4722	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	6344	--	75231	47519	47519	--	--	--	6.28	7.5
Des	9086	--	75231	76031	75231	0	39929	90.0	10.05	8.3

Trave di Fond. : 9009 [16 , 25] Pilastrate [16 , 25]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=515.3 cm Ln=500.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1260	13317	857	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.4
50.0	2369	9908	485	2635	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.7
CAMP	3205	7017	--	2235	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	5.0
450.1	-243	3833	363	1918	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	8.0
FLN	--	6315	--	--	12.57	14.83	39929	45945	1	(3+4)-II-4	7.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
50.0	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
450.1	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.
FLN	--	--	--	22.9	85.9	0.267	39929	45945	1	(3+4)-II-4	--	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-II-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8156	--	75231	76031	75231	0	45945	90.0	10.05	9.2
Cen	5297	--	75231	47519	47519	--	--	--	6.28	9.0
Des	5850	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9010 [10 , 11] Pilastrate [10 , 11]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.1 cm Ln=560.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4612	1856	728	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	7.5
56.0	5667	218	349	1131	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	6.6
CAMP	6183	942	--	2508	12.57	14.83	39929	45945	(3+4)-I-4	2	6.5
504.1	--	4576	--	3076	12.57	14.83	39929	45945	1	2	6.0
FLN	--	9033	--	--	12.57	14.83	39929	45945	1	2	5.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
56.0	14.8	85.9	0.173	22.8	85.9	0.266	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-I-4	2	Parz.	Parz.
504.1	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4464	--	75231	76031	75231	0	45945	90.0	10.05	17
Cen	5775	--	75231	47792	47792	--	--	--	6.32	8.3
Des	8712	--	75231	76031	75231	0	39929	90.0	10.05	8.6

Trave di Fond. : 9010 [11 , 12] Pilastrate [11 , 12]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.0 cm Ln=560.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8663	--	--	12.57	14.83	39929	45945	1	2	5.3
56.0	--	4651	--	2769	12.57	14.83	39929	45945	1	2	6.2
CAMP	2809	2233	--	1684	12.57	14.83	39929	45945	2	(3+4)-V-1	12
504.0	-719	3346	998	2589	12.57	14.83	39929	45945	(3+4)-V-1	2	7.7
FLN	--	7096	--	--	12.57	14.83	39929	45945	1	2	6.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
56.0	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-V-1	Parz.	Parz.
504.0	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-V-1	2	Parz.	Parz.
FLN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8116	--	75231	76031	75231	0	45945	90.0	10.05	9.3
Cen	4840	--	75231	47791	47791	--	--	--	6.32	9.9
Des	7512	--	75231	76031	75231	0	39929	90.0	10.05	10

Trave di Fond. : 9010 [12 , 13] Pilastrate [12 , 13]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.0 cm Ln=560.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	7089	--	--	12.57	14.83	39929	45945	1	2	6.5
56.0	-751	3176	1082	2701	12.57	14.83	39929	45945	(3+4)-I-3	2	7.8
CAMP	3491	1426	--	1634	12.57	14.83	39929	45945	2	(3+4)-I-4	11
504.0	-1144	3852	1164	2828	12.57	14.83	39929	45945	(3+4)-I-1	2	6.9
FLN	--	7949	--	--	12.57	14.83	39929	45945	1	2	5.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
56.0	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-I-3	2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-I-4	Parz.	Parz.
504.0	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-I-1	2	Parz.	Parz.
FLN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7992	--	75231	76031	75231	0	45945	90.0	10.05	9.4
Cen	4857	--	75231	47817	47817	--	--	--	6.32	9.8
Des	8147	--	75231	76031	75231	0	39929	90.0	10.05	9.2

Trave di Fond. : 9010 [13 , 14] Pilastrate [13 , 14]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.0 cm Ln=560.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8097	--	--	12.57	14.83	39929	45945	1	2	5.7
56.0	--	3979	--	2843	12.57	14.83	39929	45945	1	2	6.7
CAMP	3446	1381	--	1640	12.57	14.83	39929	45945	2	(3+4)-VII-2	12
504.0	-348	2866	1019	2579	12.57	14.83	39929	45945	(3+4)-VII-2	2	8.4
FLN	--	6603	--	--	12.57	14.83	39929	45945	1	2	7.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
56.0	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-VII-2	Parz.	Parz.
504.0	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-2	2	Parz.	Parz.
FLN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8374	--	75231	76031	75231	0	45945	90.0	10.05	9.0
Cen	4876	--	75231	47838	47838	--	--	--	6.33	9.8
Des	7458	--	75231	76031	75231	0	39929	90.0	10.05	10

Trave di Fond. : 9010 [14 , 15] Pilastrate [14 , 15]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=561.5 cm Ln=561.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	5426	--	--	12.57	14.83	39929	45945	1	2	8.5
56.2	-71	1927	949	2409	12.57	14.83	39929	45945	(3+4)-VII-3	2	11
CAMP	3425	1400	--	2299	12.57	14.83	39929	45945	2	2	12
505.4	--	4739	--	2914	12.57	14.83	39929	45945	1	2	6.0
FLN	--	8971	--	--	12.57	14.83	39929	45945	1	2	5.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.
56.2	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-3	2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	2	Parz.	Parz.
505.4	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7205	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	5160	--	75231	47628	47628	--	--	--	6.30	9.2
Des	8339	--	75231	76031	75231	0	39929	90.0	10.05	9.0

Trave di Fond. : 9010 [15 , 16] Pilastrate [15 , 16]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=628.5 cm Ln=628.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8253	--	--	12.57	14.83	39929	45945	1	2	5.6
62.9	-751	3463	1216	2946	12.57	14.83	39929	45945	(3+4)-V-4	2	7.2
CAMP	4972	936	--	1657	12.57	14.83	39929	45945	2	(3+4)-V-1	8.0
565.7	-432	2878	1145	2854	12.57	14.83	39929	45945	(3+4)-V-1	2	8.0
FLN	--	7518	--	--	12.57	14.83	39929	45945	1	2	6.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
62.9	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-V-4	2	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-V-1	Parz.	Parz.
565.7	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-V-1	2	Parz.	Parz.
FLN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8702	--	75231	76031	75231	0	45945	90.0	10.05	8.6
Cen	4988	--	75231	47519	47519	--	--	--	6.28	9.5
Des	8285	--	75231	76031	75231	0	39929	90.0	10.05	9.1

Trave di Fond. : 9010 [16 , 17] Pilastrate [16 , 17]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=551.9 cm Ln=551.9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8358	--	--	12.57	14.83	39929	45945	1	2	5.5
55.2	--	4624	--	2615	12.57	14.83	39929	45945	1	2	6.3
CAMP	1551	2712	--	2171	12.57	14.83	39929	45945	2	2	9.4
496.7	--	5813	--	2756	12.57	14.83	39929	45945	1	2	5.4
FLN	--	9748	--	--	12.57	14.83	39929	45945	1	2	4.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
55.2	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	2	2	Parz.	Parz.
496.7	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
FLN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7752	--	75231	76031	75231	0	45945	90.0	10.05	9.7
Cen	4857	--	75231	47519	47519	--	--	--	6.28	9.8
Des	7882	--	75231	76031	75231	0	39929	90.0	10.05	9.5

Trave di Fond. : 9010 [17 , 18] Pilastrate [17 , 18]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=663.8 cm Ln=663.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	9957	--	--	12.57	14.83	39929	45945	1	2	4.6
66.4	--	4188	--	3359	12.57	14.83	39929	45945	1	2	6.1
CAMP	9714	-452	--	2702	12.57	14.83	39929	45945	2	2	4.1
597.4	7384	--	951	--	12.57	14.83	39929	45945	2	1	4.8
FLN	6362	294	794	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
66.4	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	2	2	Parz.	Parz.
597.4	14.9	85.9	0.173	--	--	--	39929	45945	2	1	Parz.	--
FLN	14.9	85.9	0.173	22.8	85.9	0.266	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9761	--	75231	76031	75231	0	45945	90.0	10.05	7.7
Cen	6197	--	75231	47519	47519	--	--	--	6.28	7.7
Des	4903	--	75231	76031	75231	0	39929	90.0	10.05	15

Trave di Fond. : 9011 [3 , 12] Pilastrate [3 , 12]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=520.6 cm Ln=535.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5202	3040	535	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	7.0
53.5	5943	1001	125	1472	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	6.6
CAMP	6115	3866	--	2572	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-2	6.5
481.9	2766	7428	605	2987	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	4.4
FLN	1474	11565	933	--	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	4.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
53.5	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-2	Parz.	Parz.
481.9	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
FLN	14.8	85.9	0.172	23.1	85.9	0.268	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-VIII-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4773	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	6121	--	75231	47519	47519	--	--	--	6.28	7.8
Des	8740	--	75231	76031	75231	0	39929	90.0	10.05	8.6

Trave di Fond. : 9011 [12 , 21] Pilastrate [12 , 21]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=530.3 cm Ln=500.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1840	13054	530	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	3.5
50.0	2526	9418	123	2811	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	3.8
CAMP	2777	6319	--	2439	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	5.2
450.1	2650	9474	48	2793	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	3.7
FLN	2045	13087	468	--	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	3.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
50.0	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
450.1	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
FLN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-VIII-3 Cen=(5+6)-VIII-2 Des=(5+6)-VIII-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7909	--	75231	76031	75231	0	45945	90.0	10.05	9.5
Cen	5841	--	75231	47519	47519	--	--	--	6.28	8.1
Des	7672	--	75231	76031	75231	0	39929	90.0	10.05	9.8

Trave di Fond. : 9011 [21 , 30] Pilastrate [21 , 30]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.1 cm Ln=587.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3075	12815	851	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	3.6
58.7	4368	8533	491	2818	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	4.0
CAMP	5356	4928	--	2372	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	6.3
528.7	3692	3064	243	2056	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	9.0
FLN	2822	6189	572	--	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	7.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
58.7	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
528.7	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
FLN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VIII-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8139	--	75231	76031	75231	0	45945	90.0	10.05	9.2
Cen	5569	--	75231	47804	47804	--	--	--	6.32	8.6
Des	5998	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9012 [1 , 2] Pilastrate [1 , 2]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=545.1 cm Ln=545.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7387	8160	606	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	5.0
54.5	8241	5655	137	1776	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	4.8
CAMP	8435	3558	--	1487	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	4.7
490.6	476	4421	664	2565	12.57	14.83	39929	45945	(3+4)-III-2	(3+4)-I-4	6.6
FLN	-477	8038	774	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
54.5	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
490.6	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-III-2	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-IV-2 Cen=(5+6)-I-4 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6392	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	5492	--	75231	47519	47519	--	--	--	6.28	8.7
Des	7236	--	75231	76031	75231	0	39929	90.0	10.05	10

Trave di Fond. : 9012 [2 , 3] Pilastrate [2 , 3]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=560.0 cm Ln=560.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3355	9876	473	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	4.7
56.0	4041	6441	160	2371	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	5.2
CAMP	4273	3572	--	1980	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	8.3
504.0	2801	5845	358	2278	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.7
FLN	1800	9145	691	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
56.0	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
504.0	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-III-2 Cen=(5+6)-I-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6934	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4691	--	75231	47527	47527	--	--	--	6.28	10
Des	6490	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9012 [3 , 4] Pilastrate [3 , 4]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=552.0 cm Ln=552.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	241	10161	817	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	4.5
55.2	1408	6783	464	2366	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	5.0
CAMP	2684	3970	--	1969	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-1	7.7
496.8	2086	6432	367	2231	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.3
FLN	1106	9619	686	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
55.2	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-I-1	(3+4)-I-1	Parz.	Parz.
496.8	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-III-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7262	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4667	--	75231	47519	47519	--	--	--	6.28	10
Des	6470	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9012 [4 , 5] Pilastrate [4 , 5]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=568.0 cm Ln=568.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2104	8361	748	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	5.5
56.8	3204	5137	389	2194	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	6.3
CAMP	4055	2896	--	1977	12.57	14.83	39929	45945	2	(3+4)-I-4	9.4
511.2	2943	5801	402	2360	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.6
FLN	1880	9269	724	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
56.8	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-I-4	Parz.	Parz.
511.2	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-I-4 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6835	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4646	--	75231	47519	47519	--	--	--	6.28	10
Des	6749	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9012 [5 , 6] Pilastrate [5 , 6]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=561.5 cm Ln=561.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	27	9972	917	--	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	4.6
56.2	1359	6692	533	2258	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-1	5.1
CAMP	2399	4114	--	2014	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-I-4	7.5
505.4	1260	7039	456	2399	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.9
FLN	134	10524	776	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
56.2	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-I-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-I-4	Parz.	Parz.
505.4	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-I-4 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7267	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4729	--	75231	47519	47519	--	--	--	6.28	10
Des	7020	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9012 [6 , 7] Pilastrate [6 , 7]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=628.5 cm Ln=628.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1335	8906	966	--	12.57	14.83	39929	45945	(3+4)-III-3	(3+4)-I-2	5.2
62.9	3117	5101	618	2262	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-III-2	6.2
CAMP	5122	2531	--	2103	12.57	14.83	39929	45945	2	(3+4)-I-4	7.8
565.7	3331	5951	404	2573	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	5.4
FLN	2168	10134	716	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-III-3	(3+4)-I-2	Parz.	Parz.
62.9	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-III-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-I-4	Parz.	Parz.
565.7	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-I-4 Des=(5+6)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7502	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4884	--	75231	47519	47519	--	--	--	6.28	9.7
Des	7335	--	75231	76031	75231	0	39929	90.0	10.05	10

Trave di Fond. : 9012 [7 , 8] Pilastrate [7 , 8]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=536.9 cm Ln=536.9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	10215	--	--	12.57	14.83	39929	45945	1	(3+4)-I-2	4.5
53.7	154	7051	623	2227	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-III-2	5.0
CAMP	1595	4915	--	2066	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	6.6
483.2	1248	7784	250	2454	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.5
FLN	526	11193	520	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	(3+4)-I-2	--	Parz.
53.7	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-4	(3+4)-III-2	Parz.	Parz.
CAMP	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
483.2	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-I-4 Des=(5+6)-I-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7302	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4867	--	75231	48664	48664	--	--	--	6.43	10.0
Des	6872	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9012 [8 , 9] Pilastrate [8 , 9]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=663.8 cm Ln=663.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	799	8138	1166	--	12.57	14.83	39929	45945	(3+4)-III-3	(3+4)-I-2	5.6
66.4	3034	3572	864	2589	12.57	14.83	39929	45945	(3+4)-I-4	(3+4)-III-2	7.5
CAMP	10727	210	--	2094	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-1	3.7
597.4	10354	3130	217	2269	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	3.8
FLN	9165	7026	693	--	12.57	14.83	39929	45945	(3+4)-I-1	(3+4)-I-4	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-III-3	(3+4)-I-2	Parz.	Parz.
66.4	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-I-4	(3+4)-III-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-I-1	(3+4)-I-1	Parz.	Parz.
597.4	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.
FLN	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-I-1	(3+4)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VII-2 Des=(5+6)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8513	--	75231	76031	75231	0	45945	90.0	10.05	8.8
Cen	5356	--	75231	47519	47519	--	--	--	6.28	8.9
Des	7595	--	75231	76031	75231	0	39929	90.0	10.05	9.9

Trave di Fond. : 9013 [34 , 38] Pilastrate [34 , 38]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=430.4 cm Ln=430.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8677	--	--	12.57	14.83	39929	45945	1	2	5.3
43.0	--	5828	--	2558	12.57	14.83	39929	45945	1	2	5.5
CAMP	6637	3448	--	2138	12.57	14.83	39929	45945	(3+4)-VI-3	2	6.0
387.4	6586	5483	9	1180	12.57	14.83	39929	45945	(3+4)-VI-3	(3+4)-VI-2	6.1
FLN	6030	6797	499	--	12.57	14.83	39929	45945	(3+4)-VI-3	(3+4)-VI-2	6.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
43.0	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-3	2	Parz.	Parz.
387.4	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VI-3	(3+4)-VI-2	Parz.	Parz.
FLN	14.9	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VI-3	(3+4)-VI-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VI-3 Des=(5+6)-VII-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7354	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4910	--	75231	48127	48127	--	--	--	6.36	9.8
Des	3986	--	75231	76031	75231	0	39929	90.0	10.05	19

Trave di Fond. : 9014 [31 , 35] Pilastrate [31 , 35]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=802.5 cm Ln=786.7 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8958	--	--	12.57	14.83	39929	45945	1	2	5.1
78.7	-948	3798	1074	2535	12.57	14.83	39929	45945	(3+4)-V-2	2	7.3
CAMP	7904	808	--	1539	12.57	14.83	39929	45945	2	(3+4)-V-3	5.1
708.0	5127	--	925	--	12.57	14.83	39929	45945	2	1	6.6
FLN	2957	493	819	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	11

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
78.7	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-V-2	2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-V-3	Parz.	Parz.
708.0	14.8	85.9	0.173	--	--	--	39929	45945	2	1	Parz.	--
FLN	14.8	85.9	0.173	22.8	85.9	0.266	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7285	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4553	--	75231	47548	47548	--	--	--	6.29	10
Des	5262	--	75231	76031	75231	0	39929	90.0	10.05	14

Trave di Fond. : 9014 [29 , 31] Pilastrate [29 , 31]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=388.6 cm Ln=355.9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4121	6313	--	--	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-VI-3	7.3
35.6	4122	4823	--	1490	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-VI-3	7.3
CAMP	3920	3531	202	1421	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-VI-3	9.3
320.3	706	1990	--	1424	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	13
FLN	610	3415	--	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	13

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-VI-3	Parz.	Parz.
35.6	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-VI-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-VI-3	Parz.	Parz.
320.3	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-VI-3 Cen=(5+6)-VI-2 Des=(5+6)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4578	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	3010	--	75231	50296	50296	--	--	--	6.65	17
Des	4285	--	75231	76031	75231	0	39929	90.0	10.05	18

Trave di Fond. : 9015 [30 , 34] Pilastrate [30 , 34]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=376.4 cm Ln=370.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-959	7322	1744	--	12.57	14.83	39929	45945	(3+4)-VII-3	(3+4)-VII-1	6.3
37.1	677	4679	945	2643	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-VII-1	6.3
CAMP	5272	3325	488	1941	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VII-2	6.9
333.5	5746	--	312	--	12.57	14.83	39929	45945	(3+4)-VIII-1	1	6.6
FLN	6059	--	--	--	12.57	14.83	39929	45945	(3+4)-VIII-1	1	6.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-3	(3+4)-VII-1	Parz.	Parz.
37.1	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-VII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VII-2	Parz.	Parz.
333.5	14.8	85.9	0.173	--	--	--	39929	45945	(3+4)-VIII-1	1	Parz.	--
FLN	14.8	85.9	0.173	--	--	--	39929	45945	(3+4)-VIII-1	1	Parz.	--

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=2 Des=(5+6)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7192	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4521	--	75231	47519	47519	--	--	--	6.28	11
Des	2041	--	75231	76031	75231	0	39929	90.0	10.05	37

Trave di Fond. : 9015 [34 , 35] Pilastrate [34 , 35]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=351.9 cm Ln=380.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4507	3906	--	--	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	8.9
38.1	4330	2361	177	1545	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	8.9
CAMP	3976	3134	357	1786	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-VII-4	9.2
342.8	3539	4890	78	1971	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.7
FLN	3247	6861	293	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.
38.1	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-VII-4	Parz.	Parz.
342.8	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-VII-2 Cen=(5+6)-VII-4 Des=(5+6)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4443	--	75231	76031	75231	0	45945	90.0	10.05	17
Cen	3851	--	75231	47519	47519	--	--	--	6.28	12
Des	5502	--	75231	76031	75231	0	39929	90.0	10.05	14

Trave di Fond. : 9016 [4 , 13] Pilastrate [4 , 13]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=518.9 cm Ln=533.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4590	2301	610	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.7
53.3	5431	401	218	1377	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.1
CAMP	6117	3021	--	2390	12.57	14.83	39929	45945	2	(3+4)-VIII-4	6.5
480.1	1863	6319	782	2800	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	5.0
FLN	314	10183	1123	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	4.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
53.3	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VIII-4	Parz.	Parz.
480.1	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4730	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	5731	--	75231	47519	47519	--	--	--	6.28	8.3
Des	8774	--	75231	76031	75231	0	39929	90.0	10.05	8.6

Trave di Fond. : 9016 [13 , 22] Pilastrate [13 , 22]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=530.3 cm Ln=500.1 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1160	11914	383	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	3.9
50.0	1655	9050	--	2214	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	4.1
CAMP	1616	8936	30	2671	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-4	4.0
450.1	--	12392	--	3021	12.57	14.83	39929	45945	1	(3+4)-VIII-4	3.0
FLN	--	16301	--	--	12.57	14.83	39929	45945	1	(3+4)-VIII-4	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.268	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
50.0	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	23.1	85.9	0.268	39929	45945	(3+4)-VIII-4	(3+4)-VIII-4	Parz.	Parz.
450.1	--	--	--	23.1	85.9	0.269	39929	45945	1	(3+4)-VIII-4	--	Parz.
FLN	--	--	--	23.2	85.9	0.270	39929	45945	1	(3+4)-VIII-4	--	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VIII-4 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6442	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	6443	--	75231	47519	47519	--	--	--	6.28	7.4
Des	8589	--	75231	76031	75231	0	39929	90.0	10.05	8.8

Trave di Fond. : 9016 [22 , 35] Pilastrate [22 , 35]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=1014.1 cm Ln=1012.2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-602	6673	1156	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	6.9
101.2	2424	2161	674	1723	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	12
CAMP	8710	-1032	--	1219	12.57	14.83	39929	45945	2	(3+4)-VIII-1	4.6
911.0	6146	-473	306	1259	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	6.2
FLN	4134	2825	769	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	8.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
101.2	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.8	85.9	0.266	39929	45945	2	(3+4)-VIII-1	Parz.	Parz.
911.0	14.9	85.9	0.173	22.8	85.9	0.266	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6884	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4633	--	75231	47987	47987	--	--	--	6.34	10
Des	5061	--	75231	76031	75231	0	39929	90.0	10.05	15

Trave di Fond. : 9017 [25 , 32] Pilastrate [25 , 32]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=653.5 cm Ln=683.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	7882	--	--	12.57	14.83	39929	45945	1	(3+4)-II-3	5.8
68.4	349	3958	749	2219	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-II-3	7.4
CAMP	5950	3107	--	1624	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.7
615.4	5166	5979	359	1969	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	5.8
FLN	3991	9462	664	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	4.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	(3+4)-II-3	--	Parz.
68.4	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
615.4	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7463	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4252	--	75231	47727	47727	--	--	--	6.31	11
Des	5723	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9018 [28 , 31] Pilastrate [28 , 31]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=519.0 cm Ln=488.9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5455	4095	--	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.3
48.9	5538	1861	--	1766	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.2
CAMP	5150	3338	305	1911	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-4	7.3
440.0	4406	5756	152	2136	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	5.8
FLN	3943	8458	366	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	5.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
48.9	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-4	Parz.	Parz.
440.0	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-VIII-1 Cen=(5+6)-VIII-4 Des=(5+6)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5132	--	75231	76031	75231	0	45945	90.0	10.05	15
Cen	4650	--	75231	47519	47519	--	--	--	6.28	10
Des	5813	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9019 [31 , 36] Pilastrate [31 , 36]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=392.2 cm Ln=375.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2703	3420	249	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-II-1	13
37.6	2949	1404	101	2016	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-II-1	13
CAMP	7470	997	363	1086	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	5.1
338.0	7830	2048	105	1182	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	5.0
FLN	7935	3230	--	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-4	(3+4)-II-1	Parz.	Parz.
37.6	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-4	(3+4)-II-1	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
338.0	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-II-1 Cen=(5+6)-II-1 Des=(5+6)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5838	--	75231	76031	75231	0	45945	90.0	10.05	13
Cen	4137	--	75231	47519	47519	--	--	--	6.28	11
Des	3330	--	75231	76031	75231	0	39929	90.0	10.05	23

Trave di Fond. : 9020 [20 , 33] Pilastrate [20 , 33]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=846.0 cm Ln=827.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8968	--	--	12.57	14.83	39929	45945	1	(3+4)-VIII-1	5.1
82.7	894	4052	849	2297	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.2
CAMP	6752	1009	--	1704	12.57	14.83	39929	45945	2	(3+4)-IV-4	5.9
744.7	2142	4763	664	2096	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	6.7
FLN	-555	9250	1260	--	12.57	14.83	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	(3+4)-VIII-1	--	Parz.
82.7	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-IV-4	Parz.	Parz.
744.7	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VIII-1	(3+4)-VIII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8461	--	75231	76031	75231	0	45945	90.0	10.05	8.9
Cen	4212	--	75231	48078	48078	--	--	--	6.36	11
Des	7450	--	75231	76031	75231	0	39929	90.0	10.05	10

Trave di Fond. : 9021 [32 , 37] Pilastrate [32 , 37]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=620.9 cm Ln=587.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2401	7964	498	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	5.8
58.8	2786	4503	721	2277	12.57	14.83	39929	45945	(3+4)-V-2	(3+4)-II-3	6.8
CAMP	6020	1621	--	1905	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-VI-3	6.6
528.8	4702	4184	628	1641	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	7.5
FLN	3047	6679	1089	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
58.8	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-V-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-VI-3	Parz.	Parz.
528.8	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-II-1 Cen=(5+6)-II-3 Des=(5+6)-VII-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6587	--	75231	76031	75231	0	45945	90.0	10.05	11
Cen	4690	--	75231	47519	47519	--	--	--	6.28	10
Des	6451	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9022 [8 , 17] Pilastrate [8 , 17]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=521.3 cm Ln=535.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6298	3692	--	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	6.3
53.6	6567	1643	--	1479	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	6.1
CAMP	6266	6469	217	2859	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-2	4.9
482.0	3194	10430	453	3239	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	3.4
FLN	2129	14918	768	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
53.6	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-2	Parz.	Parz.
482.0	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=(5+6)-II-3 Cen=(5+6)-II-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4245	--	75231	76031	75231	0	45945	90.0	10.05	18
Cen	6898	--	75231	47519	47519	--	--	--	6.28	6.9
Des	8913	--	75231	76031	75231	0	39929	90.0	10.05	8.4

Trave di Fond. : 9022 [17 , 26] Pilastrate [17 , 26]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=516.0 cm Ln=500.3 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1596	14167	818	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.2
50.0	2654	10075	473	3161	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.5
CAMP	5576	6464	283	2790	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-3	5.0
450.3	5942	2016	--	1527	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.7
FLN	5803	3993	--	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
50.0	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-3	(3+4)-II-3	Parz.	Parz.
450.3	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-II-3 Des=(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9094	--	75231	76031	75231	0	45945	90.0	10.05	8.3
Cen	6766	--	75231	47519	47519	--	--	--	6.28	7.0
Des	4237	--	75231	76031	75231	0	39929	90.0	10.05	18

Trave di Fond. : 9023 [31 , 32] Pilastrate [31 , 32]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=693.0 cm Ln=662.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	10198	--	--	12.57	14.83	39929	45945	1	2	4.5
66.2	--	5855	--	2536	12.57	14.83	39929	45945	1	2	5.5
CAMP	3794	2987	--	1686	12.57	14.83	39929	45945	2	(3+4)-VIII-1	9.8
595.8	1860	883	593	1034	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	16
FLN	208	2653	964	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	17

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.
66.2	--	--	--	23.0	85.9	0.268	39929	45945	1	2	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VIII-1	Parz.	Parz.
595.8	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7492	--	75231	76031	75231	0	45945	90.0	10.05	10
Cen	4630	--	75231	48259	48259	--	--	--	6.38	10
Des	4454	--	75231	76031	75231	0	39929	90.0	10.05	17

Trave di Fond. : 9024 [6 , 15] Pilastrate [6 , 15]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=520.6 cm Ln=535.4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4597	2426	541	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	7.8
53.5	5347	530	149	1369	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	7.3
CAMP	5702	3706	--	2404	12.57	14.83	39929	45945	2	(3+4)-II-4	7.0
481.9	1175	7035	863	2790	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	4.7
FLN	-497	10900	1207	--	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	4.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
53.5	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-II-4	Parz.	Parz.
481.9	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4606	--	75231	76031	75231	0	45945	90.0	10.05	16
Cen	5931	--	75231	47519	47519	--	--	--	6.28	8.0
Des	8898	--	75231	76031	75231	0	39929	90.0	10.05	8.5

Trave di Fond. : 9024 [15 , 24] Pilastrate [15 , 24]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=508.3 cm Ln=493.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	600	12679	1003	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.6
49.3	1881	9379	630	2586	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	3.8
CAMP	3064	6569	--	2201	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	5.2
444.1	769	3387	161	2009	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	8.5
FLN	169	5952	470	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	7.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	23.1	85.9	0.269	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
49.3	14.8	85.9	0.172	23.1	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
444.1	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-II-3 Des=(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8345	--	75231	76031	75231	0	45945	90.0	10.05	9.0
Cen	5235	--	75231	48352	48352	--	--	--	6.39	9.2
Des	5643	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9024 [24 , 29] Pilastrate [24 , 29]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=347.6 cm Ln=372.5 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	5435	--	--	12.57	14.83	39929	45945	1	2	8.5
37.3	--	3510	--	1925	12.57	14.83	39929	45945	1	2	8.5
CAMP	4809	4564	388	1428	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	7.7
335.3	5190	5932	198	1582	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.1
FLN	5388	7514	--	--	12.57	14.83	39929	45945	(3+4)-II-3	(3+4)-II-2	6.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.
37.3	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
335.3	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-II-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-II-3 Des=(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5785	--	75231	76031	75231	0	45945	90.0	10.05	13
Cen	3812	--	75231	49755	49755	--	--	--	6.58	13
Des	4527	--	75231	76031	75231	0	39929	90.0	10.05	17

Trave di Fond. : 9025 [9 , 18] Pilastrate [9 , 18]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=521.3 cm Ln=550.6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5114	5920	830	--	12.57	14.83	39929	45945	(3+4)-VI-2	(3+4)-II-1	6.7
55.1	6494	2757	207	2005	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-VI-3	6.0
CAMP	6789	6429	--	3043	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-4	4.9
495.5	5813	10763	269	3447	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	3.2
FLN	4965	15673	595	--	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-4	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-2	(3+4)-II-1	Parz.	Parz.
55.1	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-2	(3+4)-VI-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-4	Parz.	Parz.
495.5	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.
FLN	14.8	85.9	0.173	23.1	85.9	0.269	39929	45945	(3+4)-II-1	(3+4)-II-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-II-2 Des=(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6486	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	7417	--	75231	47519	47519	--	--	--	6.28	6.4
Des	9478	--	75231	76031	75231	0	39929	90.0	10.05	7.9

Trave di Fond. : 9025 [18 , 27] Pilastrate [18 , 27]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=516.0 cm Ln=485.2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6186	9901	--	--	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	4.6
48.5	6439	5945	--	3152	12.57	14.83	39929	45945	(3+4)-II-2	(3+4)-II-3	5.1
CAMP	7192	2597	--	2668	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-3	5.6
436.6	5352	2963	1466	1716	12.57	14.83	39929	45945	(3+4)-II-1	(3+4)-II-2	5.9
FLN	5389	5117	876	--	12.57	14.83	39929	45945	(3+4)-VI-3	(3+4)-II-2	6.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
48.5	14.9	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-II-2	(3+4)-II-3	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-II-3	Parz.	Parz.
436.6	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VI-3	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=(5+6)-II-1 Cen=(5+6)-II-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8905	--	75231	76031	75231	0	45945	90.0	10.05	8.4
Cen	6509	--	75231	47519	47519	--	--	--	6.28	7.3
Des	5647	--	75231	76031	75231	0	39929	90.0	10.05	13

Trave di Fond. : 9026 [22 , 28] Pilastrate [22 , 28]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=528.9 cm Ln=561.3 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2354	5450	705	--	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	8.4
56.1	3378	2899	369	1756	12.57	14.83	39929	45945	(3+4)-VII-4	(3+4)-VII-1	9.9
CAMP	4252	2536	--	1885	12.57	14.83	39929	45945	2	(3+4)-VII-4	9.4
505.2	1453	5273	617	2233	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	6.1
FLN	145	8516	901	--	12.57	14.83	39929	45945	(3+4)-VII-1	(3+4)-VII-4	5.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.
56.1	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VII-4	(3+4)-VII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-VII-4	Parz.	Parz.
505.2	14.8	85.9	0.172	23.0	85.9	0.267	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-VII-1	(3+4)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=(5+6)-VII-4 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5596	--	75231	76031	75231	0	45945	90.0	10.05	13
Cen	4431	--	75231	47680	47680	--	--	--	6.30	11
Des	6964	--	75231	76031	75231	0	39929	90.0	10.05	11

Trave di Fond. : 9026 [28 , 29] Pilastrate [28 , 29]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=565.9 cm Ln=541.8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	4974	--	--	12.57	14.83	39929	45945	1	(3+4)-VIII-1	9.2
54.2	293	2875	741	1497	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	11
CAMP	2415	1398	--	1294	12.57	14.83	39929	45945	2	(3+4)-VII-4	17
487.6	-727	3133	843	2115	12.57	14.83	39929	45945	(3+4)-VII-1	2	8.8
FLN	--	6097	--	--	12.57	14.83	39929	45945	1	2	7.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	22.9	85.9	0.267	39929	45945	1	(3+4)-VIII-1	--	Parz.
54.2	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
CAMP	14.8	85.9	0.172	22.9	85.9	0.266	39929	45945	2	(3+4)-VII-4	Parz.	Parz.
487.6	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VII-1	2	Parz.	Parz.
FLN	--	--	--	22.9	85.9	0.267	39929	45945	1	2	--	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6136	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	3712	--	75231	47519	47519	--	--	--	6.28	13
Des	6061	--	75231	76031	75231	0	39929	90.0	10.05	12

Trave di Fond. : 9026 [29 , 32] Pilastrate [29 , 32]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=489.6 cm Ln=475.0 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	7611	--	--	12.57	14.83	39929	45945	1	2	6.0
47.5	--	4350	--	2653	12.57	14.83	39929	45945	1	2	6.6
CAMP	6171	1581	271	2253	12.57	14.83	39929	45945	(3+4)-II-1	2	6.2
427.5	6504	--	43	--	12.57	14.83	39929	45945	(3+4)-II-1	1	6.1
FLN	6557	--	--	--	12.57	14.83	39929	45945	(3+4)-II-1	1	6.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.
47.5	--	--	--	23.0	85.9	0.267	39929	45945	1	2	--	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-II-1	2	Parz.	Parz.
427.5	14.9	85.9	0.173	--	--	--	39929	45945	(3+4)-II-1	1	Parz.	--
FLN	14.9	85.9	0.173	--	--	--	39929	45945	(3+4)-II-1	1	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=(5+6)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7559	--	75231	76031	75231	0	45945	90.0	10.05	10.0
Cen	5338	--	75231	47519	47519	--	--	--	6.28	8.9
Des	2029	--	75231	76031	75231	0	39929	90.0	10.05	37

Trave di Fond. : 9027 [22 , 30] Pilastrate [22 , 30]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=734.5 cm Ln=767.2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1103	4471	1126	--	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	10
76.7	3337	1133	703	1682	12.57	14.83	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	9.9
CAMP	7469	1741	--	1828	12.57	14.83	39929	45945	2	(3+4)-V-2	5.3
690.5	2040	5368	846	2283	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	6.0
FLN	-386	9899	1222	--	12.57	14.83	39929	45945	(3+4)-V-3	(3+4)-V-2	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
76.7	14.8	85.9	0.173	22.9	85.9	0.266	39929	45945	(3+4)-VIII-2	(3+4)-VIII-3	Parz.	Parz.
CAMP	14.9	85.9	0.173	22.9	85.9	0.267	39929	45945	2	(3+4)-V-2	Parz.	Parz.
690.5	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.
FLN	14.8	85.9	0.172	23.0	85.9	0.268	39929	45945	(3+4)-V-3	(3+4)-V-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6470	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	4616	--	75231	47832	47832	--	--	--	6.32	10
Des	7930	--	75231	76031	75231	0	39929	90.0	10.05	9.5

Trave di Fond. : 9028 [22 , 34] Pilastrate [22 , 34]

Sez. T: Ba=100.0 cm Ha=40.0 cm Bs=40.0 cm Hs=50.0 cm L=843.7 cm Ln=877.2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1702	5863	1027	--	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	7.8
87.7	4033	1923	578	1736	12.57	14.83	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	8.7
CAMP	7867	1343	--	1649	12.57	14.83	39929	45945	2	(3+4)-VIII-2	5.1
789.5	4829	5084	391	2102	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	6.4
FLN	3178	9854	728	--	12.57	14.83	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	4.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.8	85.9	0.172	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.
87.7	14.8	85.9	0.173	22.9	85.9	0.267	39929	45945	(3+4)-VIII-4	(3+4)-VIII-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	14.9	85.9	0.173	22.9	85.9	0.266	39929	45945	2	(3+4)-VIII-2	Parz.	Parz.
789.5	14.8	85.9	0.173	23.0	85.9	0.267	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.
FLN	14.8	85.9	0.173	23.0	85.9	0.268	39929	45945	(3+4)-VIII-3	(3+4)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500

Comb Sin=2 Cen=(5+6)-VIII-2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6495	--	75231	76031	75231	0	45945	90.0	10.05	12
Cen	3721	--	75231	47967	47967	--	--	--	6.34	13
Des	6464	--	75231	76031	75231	0	39929	90.0	10.05	12

Normativa di riferimento

- Legge nr. 1086 del 05/11/1971.

Norme per la disciplina delle opere in conglomerato cementizio, normale e precompresso ed a struttura metallica.

- Legge nr. 64 del 02/02/1974.

Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. LL.PP. del 11/03/1988.

Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione.

- D.M. LL.PP. del 14/02/1992.

Norme tecniche per l'esecuzione delle opere in cemento armato normale e precompresso e per le strutture metalliche.

- D.M. 9 Gennaio 1996

Norme Tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato normale e precompresso e per le strutture metalliche

- D.M. 16 Gennaio 1996

Norme Tecniche relative ai 'Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi'

- D.M. 16 Gennaio 1996

Norme Tecniche per le costruzioni in zone sismiche

- Circolare Ministero LL.PP. 15 Ottobre 1996 N. 252 AA.GG./S.T.C.

Istruzioni per l'applicazione delle Norme Tecniche di cui al D.M. 9 Gennaio 1996

- Circolare Ministero LL.PP. 10 Aprile 1997 N. 65/AA.GG.

Istruzioni per l'applicazione delle Norme Tecniche per le costruzioni in zone sismiche di cui al D.M. 16 Gennaio 1996.

- Norme Tecniche per le costruzioni D.M.14/01/2008.

Istruzioni per l'applicazione delle Norme Tecniche per le costruzioni in zone sismiche di cui al D.M. 14 Gennaio 2008

Modello per il calcolo del carico limite

Il terreno di fondazione è considerato costituito da due strati uno superiore ed uno inferiore al piano di posa della fondazione. La presenza della falda è presa in considerazione in base alla sua profondità dal piano campagna. Per la verifica a carico limite si adotta l'approccio 2 con una unica combinazione di carico A1+M1+R3, in cui i coefficienti parziali di sicurezza per le resistenze sono unitari ed il coefficiente di sicurezza globale è 2.3 per il carico limite verticale e 1.1 per il coefficiente di sicurezza a carico orizzontale. L'effetto del sisma è portato in conto considerando che la forza applicata a causa del sisma non è né centrata né verticale cioè comporta l'applicazione di fattori correttivi per l'inclinazione e una riduzione delle dimensioni della fondazione in funzione dell'eccentricità. Di seguito si riporta il calcolo per le combinazioni più gravose; in calce è riportato un riepilogo per tutte le combinazioni.

Carico limite

Il calcolo del carico limite è valutato secondo la formula di Terzaghi-Meyerof

$$Q_{lim} = q \cdot N_q \cdot \zeta_q \cdot \xi_q \cdot \alpha_q \cdot \beta_q \cdot \psi_q + c \cdot N_c \cdot \zeta_c \cdot \xi_c \cdot \alpha_c \cdot \beta_c \cdot \psi_c + \gamma \cdot N_\gamma \cdot \frac{B}{2} \cdot \zeta_\gamma \cdot \xi_\gamma \cdot \alpha_\gamma \cdot \beta_\gamma \cdot \psi_\gamma$$

dove :

N_q, N_c, N_γ = Coefficienti di Terzaghi - Meyerof per la striscia indefinita

$\zeta_q, \zeta_c, \zeta_\gamma$ = coefficienti correttivi di forma funzione del rapporto B/L

ξ_q, ξ_c, ξ_γ = coefficienti correttivi di inclinazione del carico dipendente da H/V

$\alpha_q, \alpha_c, \alpha_\gamma$ = coefficienti correttivi di inclinazione del piano di posa

$\beta_q, \beta_c, \beta_\gamma$ = coefficienti correttivi di inclinazione del piano campagna

$\psi_q, \psi_c, \psi_\gamma$ = coefficienti correttivi di punzonamento dipendenti da un indice di rigidezza del terreno, in particolare detto Ir l'indice di rigidezza del terreno (secondo la teoria di Vesic dipendente dal modulo tangenziale $G=0.5 E/(1+\nu)$ del terreno,

dalla coesione c , dalla tensione effettiva alla profondità $B/2$ sotto il piano di posa, dall'angolo di attrito del terreno di fondazione) ed I_{rcrit} l'indice di rigidezza critico (dipendente dall'angolo di attrito del terreno e dal rapporto B/L) risulta che i coefficienti di punzonamento sono uguali alla unità quando $I_r \geq I_{rcrit}$, mentre sono minori dell'unità quando $I_r < I_{rcrit}$.

Oltre a queste correzioni un'altra deriva dalla eccentricità del carico riducendo le dimensioni della fondazione in modo che il carico risulti centrato rispetto alla fondazione ridotta, dette e_b ed e_l le eccentricità del carico nella direzione di B ed L il carico limite si calcola per una fondazione di dimensioni ridotte $B' = B - 2e_b$ e $L' = L - 2e_l$

Altra correzione deriva dalla presenza della falda inserendo i pesi del terreno immerso nel primo e terzo termine, in particolare, detta H_f la profondità della falda e D la profondità del piano di posa, si ha:

per $H_f < D$ si valuta la pressione effettiva sul piano di posa considerando che parte del terreno superiore è immerso, mentre nel terzo termine si userà il peso immerso

per $H_f > D$ ed $H_f < D + B$ il peso del terreno del terzo termine si interpola tra i valori immerso e secco secondo la formula:

$$\gamma = \gamma' + (\gamma - \gamma') * D/B$$

per $H_f > D + B$ la falda è trascurata.

I coefficienti di Terzaghi - Meyerhof per la striscia ed i coefficienti correttivi sono dati dalle relazioni:

$$N_q = \frac{1 + \sin(\phi)}{1 - \sin(\phi)} e^{\pi \tan(\phi)}$$

$$N_c = (N_q - 1) \cot(\phi)$$

Il coefficiente N_γ non è suscettibile di una espressione in forma analitica chiusa, ed è stato calcolato per via numerica da diversi Autori. I valori del coefficiente sono riportati nella seguente tabella in funzione dell'angolo ϕ :

ϕ°	0	1	2	3	4	5	6	7	8
N_γ	0	0.07	0.15	0.24	0.34	0.45	0.57	0.71	0.86
ϕ°	9	10	11	12	13	14	15	16	17
N_γ	1.03	1.22	1.44	1.69	1.97	2.29	2.65	3.06	3.53
ϕ°	18	19	20	21	22	23	24	25	26
N_γ	4.07	4.68	5.39	6.2	7.13	8.2	9.44	10.88	12.54
ϕ°	27	28	29	30	31	32	33	34	35
N_γ	14.47	16.72	19.34	22.4	25.99	30.22	35.19	41.06	48.03
ϕ°	36	37	38	39	40	41	42	43	44
N_γ	56.31	66.19	78.03	92.25	109.41	130.22	155.55	186.54	224.64
ϕ°	45	46	47	48	49	50			
N_γ	271.76	330.75	403.67	496.01	613.16	762.89			

$$\zeta_q = 1 + \frac{B}{L} \tan(\phi)$$

$$\zeta_c = 1 + \frac{B}{L} \frac{N_q}{N_c}$$

$$\zeta_r = 1 - 0.4 \frac{B}{L}$$

$$m = \frac{2 + \frac{B}{L}}{1 + \frac{B}{L}}$$

$$\xi_q = \left[1 - \frac{H \tan(\phi)}{V \tan(\phi) + BLc} \right]^m$$

$$\xi_c = \xi_q - \frac{1 - \xi_q}{N_c \cdot \tan(\phi)}$$

$$\xi_r = \left[1 - \frac{H \tan(\phi)}{V \tan(\phi) + BL_c} \right]^{m+1}$$

$$\psi_q = \exp \left(0.6 \frac{B}{L} - 4.4 \right) \tan(\phi) + \frac{3.07 \sin(\phi) \log_{10}(2I_r)}{1 + \sin(\phi)}$$

$$\psi_c = \psi_q - \frac{1 - \psi_q}{N_q \tan(\phi)} \text{ se } \phi \neq 0; \quad \psi_c = 0.32 + 0.12 \frac{B}{L} + 0.61 \log_{10}(I_r) \text{ se } \phi = 0$$

$$\psi_r = \psi_q$$

$$\alpha_q = \alpha_r = (1 - \varepsilon \tan(\phi))^2$$

$$\alpha_c = \alpha_q - \frac{1 - \alpha_q}{N_c \tan(\phi)}$$

$$\beta_q = (1 - \tan(\phi))^2 \cos(\phi)$$

$$\beta_c = \beta_q - \frac{q - \beta_q}{N_c \tan(\phi)}$$

$$\beta_c = \beta_q - \frac{q - \beta_q}{N_c \tan(\phi)}$$

$$\varepsilon < \pi/4; \quad \omega < \pi/4; \quad \omega < \phi$$

$$zq = zc = 1$$

$$zg = (1 - kh / \tan(\phi))^{0.45}$$

$$kh = \beta \frac{\alpha_{\max}}{g} \cdot (\text{vedi } NT - 7.11.3)$$

Per la fondazione composta si adotta una fondazione rettangolare equivalente ottenuta mediando le basi dei tratti pesati rispetto alla loro lunghezza; il numero di tratti che si prendono in considerazione sono quelli che si ottengono considerando la parte di fondazione sulla quale le tensioni del terreno non sono nulle considerando le sole condizioni di equilibrio (metodo del trapezio). La fondazione equivalente e poi ridotta in base alle eccentricità della risultante dei carichi verticali.

Simbologia carico limite fondazione composta:

B	Base del tratto
L	Lunghezza del tratto
Xq	Distanza inizio carico distribuito dall'estremo sinistro del tratto
Lq	Lunghezza del carico distribuito
Eq	Eccentricità del carico distribuito rispetto all'asse del tratto
Qv1	Primo valore del carico distribuito normale
Qv2	Secondo valore del carico distribuito normale
Qh1	Primo valore del carico distribuito tangenziale
Qh2	Secondo valore del carico distribuito tangenziale
	Distanza forza dall'estremo sinistro della fondazione.
XF	Nota: la posizione è comprensiva di eventuali momenti di trasporto, quindi sono possibili valori negativi e valori superiori alla lunghezza della fondazione

EF	Eccentricità forza dall'asse del tratto
Fv	Componente normale della forza
Fh	Componente tangenziale della forza
D	Profondità del piano di posa
ε	Inclinazione del piano di posa
ω	Inclinazione del piano campagna
ϕ	Angolo di attrito del terreno di fondazione
c	Coesione del terreno di fondazione
G	Modulo tangenziale del terreno di fondazione
γ_1	Peso specifico terreno superiore
γ	Peso specifico terreno di fondazione
γ_{1Sat}	Peso specifico terreno saturo superiore
γ_{Sat}	Peso specifico terreno saturo di fondazione
Hf	Profondità della falda
W0	Peso specifico acqua

Modello terreno per il calcolo dei cedimenti per terreno incoerente:

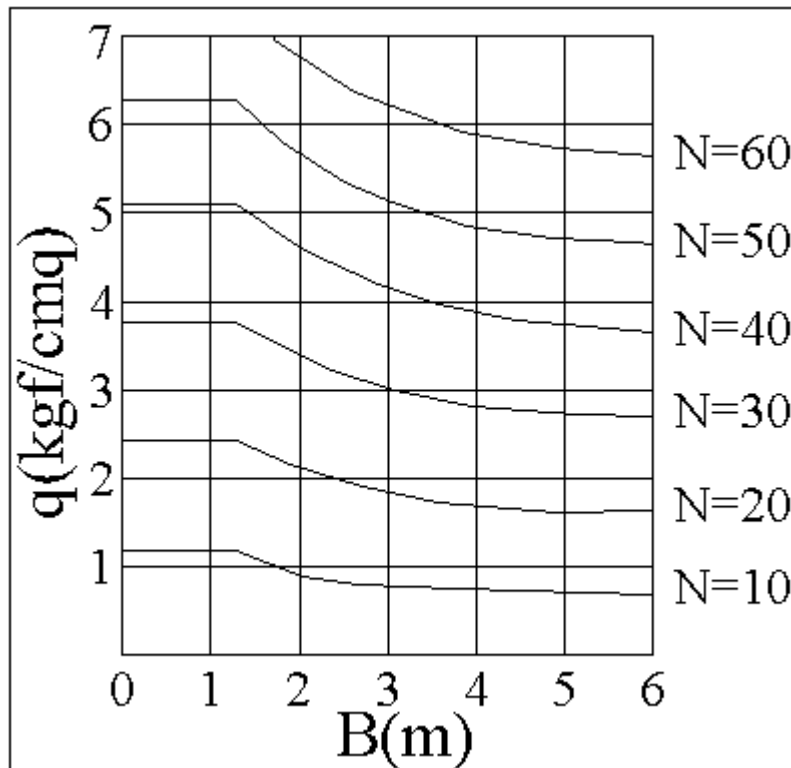
Il terreno è modellato come sequenza di strati di tipo incoerente (terreni ad elevata permeabilità). Per i terreni incoerenti non è possibile prelevare campioni intatti; per la valutazione dei parametri meccanici occorre riferirsi a prove in sito quali CPT ed SPT e quindi far uso di correlazioni empiriche per la loro valutazione. Per tali terreni, quindi, i metodi per la valutazione dei cedimenti sono empirici o semiempirici.

Simbologia terreno incoerente:

Metodo di Terzaghi e Peck

H	Spessore dello strato
Df	Profondità della fondazione rispetto allo scavo del cassone della struttura
γ	Peso specifico del terreno dello strato
γ_{Sat}	Peso specifico del terreno saturo dello strato
N_{SPT}	Numero di colpi Standard Penetration Test
Sfine	Indica se la frazione fina è rilevante, per cui il numero di colpi deve essere corretto se la strato si trova sotto falda, il suo valore è significativo solo se lo strato è sotto falda

Il cedimento viene calcolato con il metodo di Terzaghi e Peck, in base a prove SPT. Gli A.A. propongono un abaco in funzione di B, base della fondazione ed N, numero di colpi, in cui forniscono il carico q che provoca un cedimento di 2.5 cm, assumendo che tale valore fosse un cedimento accettabile. Il metodo nasce come metodo di verifica, in seguito il metodo è stato usato per il calcolo dei cedimenti istituendo una proporzionalità diretta tra q e w secondo la relazione $w(\text{cm}) = 2.5 * q/q_{\text{abaco}}$.



Il valore di N da introdurre è quello compreso tra le profondità D e D+B esso va corretto in presenza di sabbie fini e/o limose sotto falda per tener conto del fittizio aumento di resistenza per l'insorgere di sovrappressioni neutre che si hanno durante l'infissione dello strumento di prova.

La correzione da apportare è data da: $N' = 15 + 0.5 \cdot (N - 15)$ solo se $N > 15$

Il valore del carico che si legge sull'abaco va corretto in base alla profondità della falda e della profondità del piano di posa.

Per $H_f = D$ q_{abaco} va dimezzato.

Per $H_f \geq D+B$ q_{abaco} è intero.

Per $D < H_f < D+B$ si interpola linearmente.

Al valore così calcolato si applica un coefficiente di profondità dato dalla relazione $C_D = (1 - 0.25 \cdot D/B)$ per $0 < D < B$, $C_D = 1$ per $D > B$.

Travata 9010-2

La fondazione è composta da elementi rettangolari:

Profondità della falda $H_f=3.50[m]$

Peso specifico acqua $W_0=1.00[t/mc]$

Geometria fondazione e carichi applicati

Tratto	B[m]	L[m]
1	1.20	5.60
2	1.20	5.60
3	1.20	5.60
4	1.20	5.60
5	1.20	5.62
6	1.20	6.29
7	1.20	5.52
8	1.20	6.64

Carico	Xq [m]	Lq [m]	Eq [m]	Qv ₁ [kg/m]	Qv ₂ [kg/m]	Qh ₁ [kg/m]	Qh ₂ [kg/m]
1	0.00	5.60	0.00	3159.44	3620.56	-0.00	0.00
2	0.00	5.60	0.00	3158.57	3621.43	-0.00	0.00
3	0.00	5.60	0.00	3157.09	3622.91	-0.00	0.00
4	0.00	5.60	0.00	3155.85	3624.15	-0.00	0.00
5	0.00	5.62	0.00	3156.81	3623.19	-0.00	0.00
6	0.00	6.29	0.00	3187.49	3592.51	-0.00	0.00
7	0.00	5.52	0.00	3154.41	3625.59	-0.00	0.00
8	0.00	6.64	0.00	3195.05	3584.95	-0.00	0.00

Forza	XF [m]	EF [m]	Fv [kg]	Fh [kg]
1	1.36	0.00	6453	-0
2	5.74	0.00	14420	0
3	11.25	0.00	15743	0
4	16.83	0.00	15943	0
5	22.43	0.00	15279	0
6	28.19	0.00	15971	-0
7	34.21	0.00	16128	0
8	39.94	0.00	14883	-0
9	44.89	0.00	6681	0

D	1.20 [m]
ε	0.00 [°]
ω	0.00 [°]
ϕ	24.00 [°]
c	0.00 [kg/cm ²]
G	30.57 [kg/cm ²]
γ_1	1500.00 [t/mc]
γ	1500.00 [t/mc]
γ_{1Sat}	1500.00 [t/mc]
γ_{Sat}	1500.00 [t/mc]
Hf	3.50 [m]
W0	1.00 [t/mc]

Carico limite

La fondazione data è equivalente ad una fondazione rettangolare di dimensioni $B=1.20 [m]$ ed $L=46.21 [m]$

N_q	N_c	N_γ
9.603	19.324	9.440
α_q	α_c	α_γ
1.000	1.000	1.000
β_q	β_c	β_γ
1.000	1.000	1.000
ξ_q	ξ_c	ξ_γ
1.000	1.000	1.000
ψ_q	ψ_c	ψ_γ
0.109	-0.099	0.109
ζ_q	ζ_c	ζ_γ
1.012	1.013	0.990
z_q	z_c	z_g
1.000	1.000	1.000
N'_q	N'_c	N'_γ
1.063	-1.935	1.022

Indice di rigidezza critico $Ir_{crit} = 79.076$

Indice di rigidezza $Ir = 0.254$

$V = 279033$ [kg]

$H = 0$ [kg]

$eb = 0.00$ [m]

$el = 0.13$ [m]

$Q_{lim} = 1.063 \cdot 180.00 [\text{kg/cmq}] + 1.022 \cdot 1500.00 [\text{t/mc}] \cdot 1.20 [\text{m}] / 2 = 283.30 [\text{kg/cmq}]$

$Q_d = 123.17$ [kg/cmq]

$\eta_{vd} = 2.300$

$H_{lim} = 124234$ [kg]

$H_d = 112940$ [kg]

$\eta_{hd} = 1.100$

$V = 279033$ [kg] $\leq V_d = 68294934$ [kg]

$H = 0$ [kg] $\leq H_d = 112940$ [kg]

VERIFICATO
VERIFICATO

Tensioni indotte sul terreno:

Le tensioni sono riferite ai vertici dei tratti della fondazione posti in un riferimento XY con X coincidente con l'asse dei tratti ed origine nel primo tratto. I tratti sono considerati consecutivamente uno dopo l'altro in direzione X

X[m]	Y[m]	σ [kg/cmq]
0.00	0.60	0.51
5.60	0.60	0.51
11.20	0.60	0.50
16.80	0.60	0.50
22.40	0.60	0.50
28.02	0.60	0.50
34.31	0.60	0.50
39.83	0.60	0.49
46.47	0.60	0.49
0.00	-0.60	0.51
5.60	-0.60	0.51
11.20	-0.60	0.50
16.80	-0.60	0.50
22.40	-0.60	0.50
28.02	-0.60	0.50

X[m]	Y[m]	σ [kg/cmq]
34.31	-0.60	0.50
39.83	-0.60	0.49
46.47	-0.60	0.49

N°	H[m]	γ [t/mc]	γ_{Sat} [t/mc]	N _{SPT}	Sfine
1	2.00	1500.00	1500.00	5	No
2	12.00	1500.00	1500.00	10	No

Profondità fondazione **Df = 1.20 [m]**
 Carico Totale **q_{tot}=0.50[kg/cmq]**
 Valore medio di NSPT **NSPTmed= 6.667**
 Valore di q(2.5 cm) **q_{2.5}=0.771667[kg/cmq]**
 Valore di q(2.5 cm) ridotto **q_{2.5rid}=0.5787[kg/cmq]**
 CD **CD=0.750**
 CW **Cw=1.000**
 Cedimento **W=22[mm]**

Travata 9014-(3+4)-III-3

La fondazione è composta da elementi rettangolari:

Profondità della falda $H_f=3.50[m]$

Peso specifico acqua $W_0=1.00[t/mc]$

Geometria fondazione e carichi applicati

Tratto	B[m]	L[m]
1	1.20	8.02
2	1.20	3.89

Carico	Xq [m]	Lq [m]	Eq [m]	Qv1 [kg/m]	Qv2 [kg/m]	Qh1 [kg/m]	Qh2 [kg/m]
1	0.00	8.02	0.00	2200.47	2586.77	-0.00	0.00
2	0.00	3.89	0.00	2027.33	2478.50	-0.00	0.00

Forza	XF [m]	EF [m]	Fv [kg]	Fh [kg]
1	1.74	0.00	4952	1252
2	7.38	0.00	7115	157
3	10.91	0.00	2784	866

D	1.20 [m]
ε	0.00 [°]
ω	0.00 [°]
ϕ	24.00 [°]
c	0.00 [kg/cm ^q]
G	30.57 [kg/cm ^q]
γ_1	1500.00 [t/mc]
γ	1500.00 [t/mc]
γ_{1Sat}	1500.00 [t/mc]
γ_{Sat}	1500.00 [t/mc]
Hf	3.50 [m]
W0	1.00 [t/mc]

Carico limite

La fondazione data è equivalente ad una fondazione rettangolare di dimensioni B=1.20 [m] ed L=11.75 [m]

N_q	N_c	N_γ
9.603	19.324	9.440
α_q	α_c	α_γ
1.000	1.000	1.000
β_q	β_c	β_γ
1.000	1.000	1.000
ξ_q	ξ_c	ξ_γ
0.901	0.890	0.853
ψ_q	ψ_c	ψ_γ
0.112	-0.096	0.112
ζ_q	ζ_c	ζ_γ
1.045	1.051	0.959
zq	zc	zg
1.000	1.000	0.959
N'_q	N'_c	N'_γ
1.010	-1.736	0.827

Coefficiente sismico K_h (effetto cinematico) = 0.040

Indice di rigidezza critico $I_{r_{crit}} = 75.010$

Indice di rigidezza $I_r = 0.254$

$V = 42812$ [kg]

$H = 2274$ [kg]

$e_b = 0.00$ [m]

$e_l = 0.08$ [m]

$Q_{lim} = 1.010 \cdot 180.00 [\text{kg/cm}^2] + 0.827 \cdot 1500.00 [\text{t/mc}] \cdot 1.20 [\text{m}] / 2 = 256.29 [\text{kg/cm}^2]$

$Q_d = 111.43$ [kg/cm²]

$\eta_{vd} = 2.300$

$H_{lim} = 19061$ [kg]

$H_d = 17328$ [kg]

$\eta_{hd} = 1.100$

$V = 42812$ [kg] $\leq V_d = 15706537$ [kg]

$H = 2274$ [kg] $\leq H_d = 17328$ [kg]

VERIFICATO

VERIFICATO

Tensioni indotte sul terreno:

Le tensioni sono riferite ai vertici dei tratti della fondazione posti in un riferimento XY con X coincidente con l'asse dei tratti ed origine nel primo tratto. I tratti sono considerati consecutivamente uno dopo l'altro in direzione X

X[m]	Y[m]	σ [kg/cm ²]
0.00	0.60	0.29
8.02	0.60	0.30
11.91	0.60	0.31
0.00	-0.60	0.29
8.02	-0.60	0.30
11.91	-0.60	0.31

N°	H[m]	γ [t/mc]	γ_{Sat} [t/mc]	N _{SPT}	Sfine
1	2.00	1500.00	1500.00	5	No
2	12.00	1500.00	1500.00	10	No

Profondità fondazione

Df = 1.20 [m]

Carico Totale

q_{tot} = 0.30 [kg/cm²]

Valore medio di NSPT

NSPT_{med} = 6.667

Valore di q(2.5 cm)

q_{2.5} = 0.771667 [kg/cm²]

Valore di q(2.5 cm) ridotto

q_{2.5rid} = 0.5787 [kg/cm²]

CD

CD = 0.750

CW

Cw = 1.000

Cedimento

W = 13 [mm]

Travata 9025-2

La fondazione è composta da elementi rettangolari:

Profondità della falda $H_f=3.50$ [m]

Peso specifico acqua $W_0=1.00$ [t/mc]

Geometria fondazione e carichi applicati

Tratto	B[m]	L[m]
1	1.20	5.21
2	1.20	5.16

Carico	X _q [m]	L _q [m]	E _q [m]	Q _{v1} [kg/m]	Q _{v2} [kg/m]	Q _{h1} [kg/m]	Q _{h2} [kg/m]
1	0.00	5.21	0.00	2683.81	4477.76	0.00	-0.00
2	0.00	5.16	0.00	2815.63	3559.36	0.00	-0.00

Forza	XF [m]	EF [m]	Fv [kg]	Fh [kg]
1	1.19	0.00	8119	0
2	5.38	0.00	12508	0
3	9.09	0.00	6887	-0

D	1.20 [m]
ε	0.00 [°]
ω	0.00 [°]
ϕ	24.00 [°]
c	0.00 [kg/cm ²]
G	30.57 [kg/cm ²]
γ_1	1500.00 [t/mc]
γ	1500.00 [t/mc]
γ_{1Sat}	1500.00 [t/mc]
γ_{Sat}	1500.00 [t/mc]
H _f	3.50 [m]
W ₀	1.00 [t/mc]

Carico limite

La fondazione data è equivalente ad una fondazione rettangolare di dimensioni B=1.20 [m] ed L=10.29 [m]

N _q	N _c	N _{γ}
9.603	19.324	9.440
α_q	α_c	α_γ
1.000	1.000	1.000
β_q	β_c	β_γ
1.000	1.000	1.000
ξ_q	ξ_c	ξ_γ
1.000	1.000	1.000
ψ_q	ψ_c	ψ_γ
0.112	-0.096	0.112
ζ_q	ζ_c	ζ_γ
1.052	1.058	0.953
z _q	z _c	z _g
1.000	1.000	1.000
N' _q	N' _c	N' _{γ}
1.132	-1.954	1.009

Indice di rigidezza critico $I_{r_{crit}} = 74.260$

Indice di rigidezza $I_r = 0.254$

$V = 62618$ [kg]

$H = 0$ [kg]

$e_b = 0.00$ [m]

$e_l = 0.04$ [m]

$Q_{lim} = 1.132 \cdot 180.00 [\text{kg/cm}^2] + 1.009 \cdot 1500.00 [\text{t/mc}] \cdot 1.20 [\text{m}] / 2 = 294.61 [\text{kg/cm}^2]$

$Q_d = 128.09$ [kg/cm²]

$\eta_{vd} = 2.300$

$H_{lim} = 27879$ [kg]

$H_d = 25345$ [kg]

$\eta_{hd} = 1.100$

$V = 62618$ [kg] $\leq V_d = 15812564$ [kg]

$H = 0$ [kg] $\leq H_d = 25345$ [kg]

VERIFICATO
VERIFICATO

Tensioni indotte sul terreno:

Le tensioni sono riferite ai vertici dei tratti della fondazione posti in un riferimento XY con X coincidente con l'asse dei tratti ed origine nel primo tratto. I tratti sono considerati consecutivamente uno dopo l'altro in direzione X

X[m]	Y[m]	σ [kg/cm ²]
0.00	0.60	0.52
5.21	0.60	0.50
10.37	0.60	0.49
0.00	-0.60	0.52
5.21	-0.60	0.50
10.37	-0.60	0.49

N°	H[m]	γ [t/mc]	γ_{sat} [t/mc]	N _{SPT}	Sfine
1	2.00	1500.00	1500.00	5	No
2	12.00	1500.00	1500.00	10	No

Profondità fondazione

Df = 1.20 [m]

Carico Totale

q_{tot} = 0.50 [kg/cm²]

Valore medio di NSPT

NSPT_{med} = 6.667

Valore di q(2.5 cm)

q_{2.5} = 0.771667 [kg/cm²]

Valore di q(2.5 cm) ridotto

q_{2.5rid} = 0.5787 [kg/cm²]

CD

CD = 0.750

CW

Cw = 1.000

Cedimento

W = 22 [mm]

Riepilogo risultati del calcolo

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cm ²]	q _e [kg/cm ²]	w [mm]
9001	2	22967	6653264	>100	0	9296	>100	138.55	0.48	21
	(3+4)-I-1	15319	5938699	>100	630	6200	10.83	126.12	0.32	14
	(3+4)-I-2	15075	5770738	>100	767	6102	8.76	123.71	0.31	13
	(3+4)-I-3	17000	5807805	>100	866	6881	8.74	123.54	0.35	15
	(3+4)-I-4	16756	5969022	>100	690	6782	10.82	126.00	0.35	15
	(3+4)-II-1	16191	6546744	>100	40	6553	>100	136.28	0.34	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-II-2	15380	6076699	>100	462	6225	14.81	129.09	0.32	14
	(3+4)-II-3	16695	6106660	>100	503	6758	14.77	128.96	0.35	15
	(3+4)-II-4	15884	6523121	>100	39	6429	>100	136.35	0.33	14
	(3+4)-III-1	15295	5961366	>100	596	6191	11.42	126.71	0.32	14
	(3+4)-III-2	15099	5748722	>100	800	6111	8.40	123.13	0.31	14
	(3+4)-III-3	16976	5784377	>100	902	6871	8.38	122.96	0.35	15
	(3+4)-III-4	16780	5992765	>100	654	6792	11.42	126.59	0.35	15
	(3+4)-IV-1	16111	6464660	>100	156	6521	46.10	134.25	0.33	14
	(3+4)-IV-2	15460	6000471	>100	575	6257	11.97	127.13	0.32	14
	(3+4)-IV-3	16615	6026977	>100	620	6725	11.93	126.99	0.34	15
	(3+4)-IV-4	15964	6442230	>100	154	6461	46.24	134.33	0.33	14
	(3+4)-V-1	15259	5942137	>100	609	6176	11.15	126.48	0.32	14
	(3+4)-V-2	15016	5773611	>100	746	6078	8.96	124.06	0.31	13
	(3+4)-V-3	17059	5814823	>100	847	6905	8.97	123.92	0.35	15
	(3+4)-V-4	16816	5975689	>100	670	6806	11.17	126.38	0.35	15
	(3+4)-VI-1	16173	6545119	>100	46	6546	>100	136.17	0.34	14
	(3+4)-VI-2	15362	6077769	>100	456	6218	14.99	129.20	0.32	14
	(3+4)-VI-3	16713	6108586	>100	497	6765	14.96	129.07	0.35	15
	(3+4)-VI-4	15902	6521690	>100	45	6436	>100	136.24	0.33	14
	(3+4)-VII-1	15235	5964774	>100	576	6167	11.78	127.06	0.32	14
	(3+4)-VII-2	15040	5751628	>100	779	6087	8.59	123.48	0.31	13
	(3+4)-VII-3	17035	5791426	>100	883	6895	8.59	123.34	0.35	15
	(3+4)-VII-4	16840	5999399	>100	635	6816	11.81	126.97	0.35	15
	(3+4)-VIII-1	16093	6463000	>100	161	6514	44.38	134.14	0.33	14
	(3+4)-VIII-2	15442	6001569	>100	569	6250	12.09	127.23	0.32	14
	(3+4)-VIII-3	16633	6028936	>100	614	6732	12.05	127.10	0.34	15
	(3+4)-VIII-4	15982	6440779	>100	160	6469	44.55	134.22	0.33	14
	(5+6)-I-1	15319	5938699	>100	630	6200	10.83	126.12	0.32	14
	(5+6)-I-2	15075	5770738	>100	767	6102	8.76	123.71	0.31	13
	(5+6)-I-3	17000	5807805	>100	866	6881	8.74	123.54	0.35	15
	(5+6)-I-4	16756	5969022	>100	690	6782	10.82	126.00	0.35	15
	(5+6)-II-1	16191	6546744	>100	40	6553	>100	136.28	0.34	14
	(5+6)-II-2	15380	6076699	>100	462	6225	14.81	129.09	0.32	14
	(5+6)-II-3	16695	6106660	>100	503	6758	14.77	128.96	0.35	15
	(5+6)-II-4	15884	6523121	>100	39	6429	>100	136.35	0.33	14
	(5+6)-III-1	15295	5961366	>100	596	6191	11.42	126.71	0.32	14
	(5+6)-III-2	15099	5748722	>100	800	6111	8.40	123.13	0.31	14
	(5+6)-III-3	16976	5784377	>100	902	6871	8.38	122.96	0.35	15
	(5+6)-III-4	16780	5992765	>100	654	6792	11.42	126.59	0.35	15
	(5+6)-IV-1	16111	6464660	>100	156	6521	46.10	134.25	0.33	14
	(5+6)-IV-2	15460	6000471	>100	575	6257	11.97	127.13	0.32	14
	(5+6)-IV-3	16615	6026977	>100	620	6725	11.93	126.99	0.34	15
	(5+6)-IV-4	15964	6442230	>100	154	6461	46.24	134.33	0.33	14
	(5+6)-V-1	15259	5942137	>100	609	6176	11.15	126.48	0.32	14
	(5+6)-V-2	15016	5773611	>100	746	6078	8.96	124.06	0.31	13
	(5+6)-V-3	17059	5814823	>100	847	6905	8.97	123.92	0.35	15
	(5+6)-V-4	16816	5975689	>100	670	6806	11.17	126.38	0.35	15
	(5+6)-VI-1	16173	6545119	>100	46	6546	>100	136.17	0.34	14
	(5+6)-VI-2	15362	6077769	>100	456	6218	14.99	129.20	0.32	14
	(5+6)-VI-3	16713	6108586	>100	497	6765	14.96	129.07	0.35	15
	(5+6)-VI-4	15902	6521690	>100	45	6436	>100	136.24	0.33	14
	(5+6)-VII-1	15235	5964774	>100	576	6167	11.78	127.06	0.32	14
	(5+6)-VII-2	15040	5751628	>100	779	6087	8.59	123.48	0.31	13
	(5+6)-VII-3	17035	5791426	>100	883	6895	8.59	123.34	0.35	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-VII-4	16840	5999399	>100	635	6816	11.81	126.97	0.35	15
	(5+6)-VIII-1	16093	6463000	>100	161	6514	44.38	134.14	0.33	14
	(5+6)-VIII-2	15442	6001569	>100	569	6250	12.09	127.23	0.32	14
	(5+6)-VIII-3	16633	6028936	>100	614	6732	12.05	127.10	0.34	15
	(5+6)-VIII-4	15982	6440779	>100	160	6469	44.55	134.22	0.33	14
9002	2	61496	15798089	>100	0	24891	>100	128.10	0.49	21
	(3+4)-I-1	41728	15524872	>100	14	16890	>100	126.42	0.34	14
	(3+4)-I-2	42371	14689317	>100	1180	17150	15.98	118.87	0.34	15
	(3+4)-I-3	42454	14689287	>100	1185	17183	15.95	118.86	0.34	15
	(3+4)-I-4	43097	15707228	>100	14	17444	>100	126.34	0.35	15
	(3+4)-II-1	41232	14082427	>100	1721	16689	10.67	115.27	0.33	14
	(3+4)-II-2	43376	14030274	>100	2173	17556	8.89	112.97	0.35	15
	(3+4)-II-3	41450	13837233	>100	2082	16777	8.87	113.04	0.33	14
	(3+4)-II-4	43593	14280175	>100	1816	17645	10.69	115.19	0.35	15
	(3+4)-III-1	41739	15529434	>100	9	16894	>100	126.45	0.34	14
	(3+4)-III-2	42361	14685153	>100	1184	17146	15.93	118.85	0.34	15
	(3+4)-III-3	42464	14686361	>100	1190	17187	15.89	118.83	0.34	15
	(3+4)-III-4	43087	15710084	>100	9	17439	>100	126.37	0.35	15
	(3+4)-IV-1	41266	14072838	>100	1738	16703	10.57	115.16	0.33	14
	(3+4)-IV-2	43341	14022382	>100	2185	17543	8.83	112.89	0.35	15
	(3+4)-IV-3	41484	13827466	>100	2100	16791	8.80	112.93	0.33	14
	(3+4)-IV-4	43559	14272001	>100	1829	17631	10.60	115.10	0.35	15
	(3+4)-V-1	41890	15456304	>100	155	16955	>100	125.46	0.34	15
	(3+4)-V-2	42533	14864887	>100	1015	17215	18.66	119.93	0.34	15
	(3+4)-V-3	42292	14780625	>100	1009	17118	18.67	119.97	0.34	15
	(3+4)-V-4	42935	15546656	>100	159	17378	>100	125.42	0.35	15
	(3+4)-VI-1	41280	14056028	>100	1773	16708	10.36	114.94	0.33	14
	(3+4)-VI-2	43424	14056820	>100	2124	17576	9.10	113.29	0.35	15
	(3+4)-VI-3	41401	13863676	>100	2028	16757	9.09	113.36	0.33	14
	(3+4)-VI-4	43545	14253343	>100	1866	17625	10.39	114.87	0.35	15
	(3+4)-VII-1	41900	15453520	>100	160	16959	>100	125.43	0.34	15
	(3+4)-VII-2	42523	14860668	>100	1019	17211	18.58	119.90	0.34	15
	(3+4)-VII-3	42302	14777746	>100	1014	17122	18.58	119.94	0.34	15
	(3+4)-VII-4	42925	15542170	>100	163	17374	>100	125.40	0.34	15
	(3+4)-VIII-1	41315	14046391	>100	1791	16722	10.27	114.84	0.33	14
	(3+4)-VIII-2	43390	14048884	>100	2136	17562	9.04	113.20	0.35	15
	(3+4)-VIII-3	41435	13853955	>100	2046	16771	9.02	113.26	0.33	14
	(3+4)-VIII-4	43511	14245213	>100	1879	17611	10.31	114.79	0.35	15
	(5+6)-I-1	41728	15524872	>100	14	16890	>100	126.42	0.34	14
	(5+6)-I-2	42371	14689317	>100	1180	17150	15.98	118.87	0.34	15
	(5+6)-I-3	42454	14689287	>100	1185	17183	15.95	118.86	0.34	15
	(5+6)-I-4	43097	15707228	>100	14	17444	>100	126.34	0.35	15
	(5+6)-II-1	41232	14082427	>100	1721	16689	10.67	115.27	0.33	14
	(5+6)-II-2	43376	14030274	>100	2173	17556	8.89	112.97	0.35	15
	(5+6)-II-3	41450	13837233	>100	2082	16777	8.87	113.04	0.33	14
	(5+6)-II-4	43593	14280175	>100	1816	17645	10.69	115.19	0.35	15
	(5+6)-III-1	41739	15529434	>100	9	16894	>100	126.45	0.34	14
	(5+6)-III-2	42361	14685153	>100	1184	17146	15.93	118.85	0.34	15
	(5+6)-III-3	42464	14686361	>100	1190	17187	15.89	118.83	0.34	15
	(5+6)-III-4	43087	15710084	>100	9	17439	>100	126.37	0.35	15
	(5+6)-IV-1	41266	14072838	>100	1738	16703	10.57	115.16	0.33	14
	(5+6)-IV-2	43341	14022382	>100	2185	17543	8.83	112.89	0.35	15
	(5+6)-IV-3	41484	13827466	>100	2100	16791	8.80	112.93	0.33	14
	(5+6)-IV-4	43559	14272001	>100	1829	17631	10.60	115.10	0.35	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-V-1	41890	15456304	>100	155	16955	>100	125.46	0.34	15
	(5+6)-V-2	42533	14864887	>100	1015	17215	18.66	119.93	0.34	15
	(5+6)-V-3	42292	14780625	>100	1009	17118	18.67	119.97	0.34	15
	(5+6)-V-4	42935	15546656	>100	159	17378	>100	125.42	0.35	15
	(5+6)-VI-1	41280	14056028	>100	1773	16708	10.36	114.94	0.33	14
	(5+6)-VI-2	43424	14056820	>100	2124	17576	9.10	113.29	0.35	15
	(5+6)-VI-3	41401	13863676	>100	2028	16757	9.09	113.36	0.33	14
	(5+6)-VI-4	43545	14253343	>100	1866	17625	10.39	114.87	0.35	15
	(5+6)-VII-1	41900	15453520	>100	160	16959	>100	125.43	0.34	15
	(5+6)-VII-2	42523	14860668	>100	1019	17211	18.58	119.90	0.34	15
	(5+6)-VII-3	42302	14777746	>100	1014	17122	18.58	119.94	0.34	15
	(5+6)-VII-4	42925	15542170	>100	163	17374	>100	125.40	0.34	15
	(5+6)-VIII-1	41315	14046391	>100	1791	16722	10.27	114.84	0.33	14
	(5+6)-VIII-2	43390	14048884	>100	2136	17562	9.04	113.20	0.35	15
	(5+6)-VIII-3	41435	13853955	>100	2046	16771	9.02	113.26	0.33	14
	(5+6)-VIII-4	43511	14245213	>100	1879	17611	10.31	114.79	0.35	15
9003	2	59251	15729154	>100	0	23982	>100	128.13	0.48	21
	(3+4)-I-1	36843	15329779	>100	61	14912	>100	126.12	0.30	13
	(3+4)-I-2	36811	14598306	>100	1069	14899	15.33	118.58	0.30	13
	(3+4)-I-3	46251	14373910	>100	1346	18720	15.30	118.67	0.37	16
	(3+4)-I-4	46219	15635148	>100	76	18707	>100	125.98	0.37	16
	(3+4)-II-1	40173	13579463	>100	1652	16260	10.82	115.69	0.32	14
	(3+4)-II-2	40066	13533417	>100	2013	16217	8.86	113.18	0.32	14
	(3+4)-II-3	42995	13310310	>100	2166	17402	8.84	113.27	0.35	15
	(3+4)-II-4	42889	13887721	>100	1761	17359	10.84	115.55	0.35	15
	(3+4)-III-1	36815	15211617	>100	54	14901	>100	126.22	0.30	13
	(3+4)-III-2	36838	14476954	>100	1076	14910	15.24	118.59	0.30	13
	(3+4)-III-3	46224	14275489	>100	1353	18709	15.21	118.67	0.37	16
	(3+4)-III-4	46246	15565494	>100	68	18718	>100	126.07	0.37	16
	(3+4)-IV-1	40082	13214305	>100	1673	16223	10.67	115.72	0.32	14
	(3+4)-IV-2	40158	13181124	>100	2040	16254	8.77	113.22	0.32	14
	(3+4)-IV-3	42904	12975114	>100	2188	17366	8.73	113.28	0.35	15
	(3+4)-IV-4	42980	13549765	>100	1789	17396	10.70	115.57	0.35	15
	(3+4)-V-1	36751	15249758	>100	87	14875	>100	125.95	0.30	13
	(3+4)-V-2	36719	14781162	>100	921	14862	17.76	119.62	0.30	13
	(3+4)-V-3	46343	14547168	>100	1161	18757	17.77	119.73	0.37	16
	(3+4)-V-4	46311	15589811	>100	109	18744	>100	125.80	0.37	16
	(3+4)-VI-1	40145	13527593	>100	1700	16249	10.51	115.38	0.32	14
	(3+4)-VI-2	40039	13583369	>100	1965	16206	9.07	113.48	0.32	14
	(3+4)-VI-3	43023	13360738	>100	2115	17414	9.06	113.58	0.35	15
	(3+4)-VI-4	42916	13837724	>100	1813	17371	10.54	115.24	0.35	15
	(3+4)-VII-1	36723	15119821	>100	93	14864	>100	125.96	0.30	13
	(3+4)-VII-2	36746	14658298	>100	928	14873	17.64	119.63	0.30	13
	(3+4)-VII-3	46315	14448051	>100	1169	18746	17.64	119.73	0.37	16
	(3+4)-VII-4	46338	15485758	>100	117	18756	>100	125.79	0.37	16
	(3+4)-VIII-1	40054	13163198	>100	1721	16212	10.36	115.41	0.32	14
	(3+4)-VIII-2	40130	13229776	>100	1991	16243	8.97	113.52	0.32	14
	(3+4)-VIII-3	42932	13024817	>100	2137	17377	8.95	113.59	0.35	15
	(3+4)-VIII-4	43008	13500989	>100	1841	17407	10.40	115.27	0.35	15
	(5+6)-I-1	36843	15329779	>100	61	14912	>100	126.12	0.30	13
	(5+6)-I-2	36811	14598306	>100	1069	14899	15.33	118.58	0.30	13
	(5+6)-I-3	46251	14373910	>100	1346	18720	15.30	118.67	0.37	16
	(5+6)-I-4	46219	15635148	>100	76	18707	>100	125.98	0.37	16
	(5+6)-II-1	40173	13579463	>100	1652	16260	10.82	115.69	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-II-2	40066	13533417	>100	2013	16217	8.86	113.18	0.32	14
	(5+6)-II-3	42995	13310310	>100	2166	17402	8.84	113.27	0.35	15
	(5+6)-II-4	42889	13887721	>100	1761	17359	10.84	115.55	0.35	15
	(5+6)-III-1	36815	15211617	>100	54	14901	>100	126.22	0.30	13
	(5+6)-III-2	36838	14476954	>100	1076	14910	15.24	118.59	0.30	13
	(5+6)-III-3	46224	14275489	>100	1353	18709	15.21	118.67	0.37	16
	(5+6)-III-4	46246	15565494	>100	68	18718	>100	126.07	0.37	16
	(5+6)-IV-1	40082	13214305	>100	1673	16223	10.67	115.72	0.32	14
	(5+6)-IV-2	40158	13181124	>100	2040	16254	8.77	113.22	0.32	14
	(5+6)-IV-3	42904	12975114	>100	2188	17366	8.73	113.28	0.35	15
	(5+6)-IV-4	42980	13549765	>100	1789	17396	10.70	115.57	0.35	15
	(5+6)-V-1	36751	15249758	>100	87	14875	>100	125.95	0.30	13
	(5+6)-V-2	36719	14781162	>100	921	14862	17.76	119.62	0.30	13
	(5+6)-V-3	46343	14547168	>100	1161	18757	17.77	119.73	0.37	16
	(5+6)-V-4	46311	15589811	>100	109	18744	>100	125.80	0.37	16
	(5+6)-VI-1	40145	13527593	>100	1700	16249	10.51	115.38	0.32	14
	(5+6)-VI-2	40039	13583369	>100	1965	16206	9.07	113.48	0.32	14
	(5+6)-VI-3	43023	13360738	>100	2115	17414	9.06	113.58	0.35	15
	(5+6)-VI-4	42916	13837724	>100	1813	17371	10.54	115.24	0.35	15
	(5+6)-VII-1	36723	15119821	>100	93	14864	>100	125.96	0.30	13
	(5+6)-VII-2	36746	14658298	>100	928	14873	17.64	119.63	0.30	13
	(5+6)-VII-3	46315	14448051	>100	1169	18746	17.64	119.73	0.37	16
	(5+6)-VII-4	46338	15485758	>100	117	18756	>100	125.79	0.37	16
	(5+6)-VIII-1	40054	13163198	>100	1721	16212	10.36	115.41	0.32	14
	(5+6)-VIII-2	40130	13229776	>100	1991	16243	8.97	113.52	0.32	14
	(5+6)-VIII-3	42932	13024817	>100	2137	17377	8.95	113.59	0.35	15
	(5+6)-VIII-4	43008	13500989	>100	1841	17407	10.40	115.27	0.35	15
9004	2	268480	67804778	>100	0	108668	>100	123.18	0.48	21
	(3+4)-I-1	189234	59247939	>100	8909	76593	9.46	108.88	0.34	15
	(3+4)-I-2	185009	60393192	>100	7903	74883	10.42	110.01	0.33	14
	(3+4)-I-3	187552	59773853	>100	8028	75912	10.40	110.00	0.34	15
	(3+4)-I-4	183327	58585722	>100	8638	74202	9.45	108.88	0.33	14
	(3+4)-II-1	193575	63242028	>100	4012	78350	21.48	115.87	0.35	15
	(3+4)-II-2	179491	65397847	>100	1120	72650	71.34	119.83	0.32	14
	(3+4)-II-3	193070	66115724	>100	1208	78146	71.16	119.81	0.35	15
	(3+4)-II-4	178987	62490710	>100	3704	72445	21.52	115.90	0.32	14
	(3+4)-III-1	188833	59937878	>100	8437	76431	9.96	109.50	0.34	15
	(3+4)-III-2	185410	59692263	>100	8364	75045	9.87	109.39	0.33	14
	(3+4)-III-3	187151	59072721	>100	8464	75750	9.84	109.37	0.34	15
	(3+4)-III-4	183728	59290694	>100	8213	74365	9.96	109.51	0.33	14
	(3+4)-IV-1	192237	65144714	>100	2442	77809	35.05	118.04	0.35	15
	(3+4)-IV-2	180829	64823871	>100	2576	73191	31.25	117.62	0.33	14
	(3+4)-IV-3	191732	64192712	>100	2742	77604	31.13	117.61	0.35	15
	(3+4)-IV-4	180324	65006754	>100	2284	72987	35.15	118.05	0.33	14
	(3+4)-V-1	187387	59627970	>100	8994	75846	9.28	108.63	0.34	15
	(3+4)-V-2	183162	60794740	>100	7992	74135	10.20	109.75	0.33	14
	(3+4)-V-3	189399	60191864	>100	8260	76660	10.21	109.77	0.34	15
	(3+4)-V-4	185174	59018642	>100	8873	74950	9.29	108.66	0.33	14
	(3+4)-VI-1	193020	63361904	>100	4052	78126	21.21	115.79	0.35	15
	(3+4)-VI-2	178937	65174899	>100	1163	72425	68.48	119.76	0.32	14
	(3+4)-VI-3	193624	65910578	>100	1261	78370	68.37	119.74	0.35	15
	(3+4)-VI-4	179541	62633699	>100	3760	72670	21.26	115.82	0.32	14
	(3+4)-VII-1	186986	60324621	>100	8526	75683	9.76	109.24	0.34	15
	(3+4)-VII-2	183563	60086814	>100	8449	74298	9.67	109.14	0.33	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-VII-3	188998	59493745	>100	8699	76498	9.67	109.15	0.34	15
	(3+4)-VII-4	185575	59720482	>100	8444	75112	9.78	109.28	0.33	14
	(3+4)-VIII-1	191683	64938058	>100	2486	77584	34.33	117.97	0.35	15
	(3+4)-VIII-2	180275	64959275	>100	2615	72967	30.69	117.54	0.33	14
	(3+4)-VIII-3	192287	64322898	>100	2798	77829	30.59	117.54	0.35	15
	(3+4)-VIII-4	180878	65146077	>100	2337	73211	34.46	117.98	0.33	14
	(5+6)-I-1	189234	59247939	>100	8909	76593	9.46	108.88	0.34	15
	(5+6)-I-2	185009	60393192	>100	7903	74883	10.42	110.01	0.33	14
	(5+6)-I-3	187552	59773853	>100	8028	75912	10.40	110.00	0.34	15
	(5+6)-I-4	183327	58585722	>100	8638	74202	9.45	108.88	0.33	14
	(5+6)-II-1	193575	63242028	>100	4012	78350	21.48	115.87	0.35	15
	(5+6)-II-2	179491	65397847	>100	1120	72650	71.34	119.83	0.32	14
	(5+6)-II-3	193070	66115724	>100	1208	78146	71.16	119.81	0.35	15
	(5+6)-II-4	178987	62490710	>100	3704	72445	21.52	115.90	0.32	14
	(5+6)-III-1	188833	59937878	>100	8437	76431	9.96	109.50	0.34	15
	(5+6)-III-2	185410	59692263	>100	8364	75045	9.87	109.39	0.33	14
	(5+6)-III-3	187151	59072721	>100	8464	75750	9.84	109.37	0.34	15
	(5+6)-III-4	183728	59290694	>100	8213	74365	9.96	109.51	0.33	14
	(5+6)-IV-1	192237	65144714	>100	2442	77809	35.05	118.04	0.35	15
	(5+6)-IV-2	180829	64823871	>100	2576	73191	31.25	117.62	0.33	14
	(5+6)-IV-3	191732	64192712	>100	2742	77604	31.13	117.61	0.35	15
	(5+6)-IV-4	180324	65006754	>100	2284	72987	35.15	118.05	0.33	14
	(5+6)-V-1	187387	59627970	>100	8994	75846	9.28	108.63	0.34	15
	(5+6)-V-2	183162	60794740	>100	7992	74135	10.20	109.75	0.33	14
	(5+6)-V-3	189399	60191864	>100	8260	76660	10.21	109.77	0.34	15
	(5+6)-V-4	185174	59018642	>100	8873	74950	9.29	108.66	0.33	14
	(5+6)-VI-1	193020	63361904	>100	4052	78126	21.21	115.79	0.35	15
	(5+6)-VI-2	178937	65174899	>100	1163	72425	68.48	119.76	0.32	14
	(5+6)-VI-3	193624	65910578	>100	1261	78370	68.37	119.74	0.35	15
	(5+6)-VI-4	179541	62633699	>100	3760	72670	21.26	115.82	0.32	14
	(5+6)-VII-1	186986	60324621	>100	8526	75683	9.76	109.24	0.34	15
	(5+6)-VII-2	183563	60086814	>100	8449	74298	9.67	109.14	0.33	14
	(5+6)-VII-3	188998	59493745	>100	8699	76498	9.67	109.15	0.34	15
	(5+6)-VII-4	185575	59720482	>100	8444	75112	9.78	109.28	0.33	14
	(5+6)-VIII-1	191683	64938058	>100	2486	77584	34.33	117.97	0.35	15
	(5+6)-VIII-2	180275	64959275	>100	2615	72967	30.69	117.54	0.33	14
	(5+6)-VIII-3	192287	64322898	>100	2798	77829	30.59	117.54	0.35	15
	(5+6)-VIII-4	180878	65146077	>100	2337	73211	34.46	117.98	0.33	14
9005	2	60679	15634975	>100	0	24560	>100	128.17	0.49	21
	(3+4)-I-1	42393	15485559	>100	14	17159	>100	126.44	0.34	15
	(3+4)-I-2	42565	14721081	>100	1186	17228	15.98	118.86	0.34	15
	(3+4)-I-3	41221	14350081	>100	1151	16684	15.95	119.02	0.33	14
	(3+4)-I-4	41393	15427092	>100	14	16754	>100	126.46	0.33	14
	(3+4)-II-1	41783	13866461	>100	1744	16912	10.67	115.38	0.34	15
	(3+4)-II-2	42355	13965268	>100	2122	17143	8.89	113.01	0.34	15
	(3+4)-II-3	41431	13536957	>100	2081	16769	8.87	113.19	0.33	14
	(3+4)-II-4	42003	14296625	>100	1750	17001	10.69	115.18	0.34	15
	(3+4)-III-1	42335	15418656	>100	9	17135	>100	126.50	0.34	15
	(3+4)-III-2	42622	14730371	>100	1192	17252	15.93	118.83	0.34	15
	(3+4)-III-3	41164	14278160	>100	1154	16661	15.89	119.02	0.33	14
	(3+4)-III-4	41451	15502847	>100	9	16777	>100	126.46	0.33	14
	(3+4)-IV-1	41590	13636281	>100	1752	16834	10.57	115.39	0.33	14
	(3+4)-IV-2	42547	13748393	>100	2145	17221	8.83	113.03	0.34	15
	(3+4)-IV-3	41239	13309100	>100	2087	16692	8.80	113.20	0.33	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-IV-4	42196	14073106	>100	1772	17079	10.60	115.20	0.34	15
	(3+4)-V-1	42505	15381153	>100	157	17204	>100	125.50	0.34	15
	(3+4)-V-2	42677	14863025	>100	1018	17274	18.66	119.93	0.34	15
	(3+4)-V-3	41109	14470932	>100	980	16639	18.67	120.11	0.33	14
	(3+4)-V-4	41281	15302579	>100	153	16708	>100	125.53	0.33	14
	(3+4)-VI-1	41816	13830795	>100	1796	16925	10.36	115.05	0.34	15
	(3+4)-VI-2	42388	14000893	>100	2073	17157	9.10	113.32	0.34	15
	(3+4)-VI-3	41398	13572115	>100	2028	16756	9.09	113.51	0.33	14
	(3+4)-VI-4	41970	14260475	>100	1799	16987	10.39	114.87	0.34	15
	(3+4)-VII-1	42448	15307740	>100	162	17181	>100	125.50	0.34	15
	(3+4)-VII-2	42735	14854087	>100	1024	17297	18.58	119.90	0.34	15
	(3+4)-VII-3	41051	14398163	>100	984	16616	18.58	120.12	0.33	14
	(3+4)-VII-4	41338	15370741	>100	157	16732	>100	125.47	0.33	14
	(3+4)-VIII-1	41624	13601433	>100	1804	16847	10.27	115.06	0.34	14
	(3+4)-VIII-2	42581	13783552	>100	2096	17235	9.04	113.34	0.34	15
	(3+4)-VIII-3	41205	13343438	>100	2035	16678	9.02	113.52	0.33	14
	(3+4)-VIII-4	42162	14037430	>100	1821	17065	10.31	114.89	0.34	15
	(5+6)-I-1	42393	15485559	>100	14	17159	>100	126.44	0.34	15
	(5+6)-I-2	42565	14721081	>100	1186	17228	15.98	118.86	0.34	15
	(5+6)-I-3	41221	14350081	>100	1151	16684	15.95	119.02	0.33	14
	(5+6)-I-4	41393	15427092	>100	14	16754	>100	126.46	0.33	14
	(5+6)-II-1	41783	13866461	>100	1744	16912	10.67	115.38	0.34	15
	(5+6)-II-2	42355	13965268	>100	2122	17143	8.89	113.01	0.34	15
	(5+6)-II-3	41431	13536957	>100	2081	16769	8.87	113.19	0.33	14
	(5+6)-II-4	42003	14296625	>100	1750	17001	10.69	115.18	0.34	15
	(5+6)-III-1	42335	15418656	>100	9	17135	>100	126.50	0.34	15
	(5+6)-III-2	42622	14730371	>100	1192	17252	15.93	118.83	0.34	15
	(5+6)-III-3	41164	14278160	>100	1154	16661	15.89	119.02	0.33	14
	(5+6)-III-4	41451	15502847	>100	9	16777	>100	126.46	0.33	14
	(5+6)-IV-1	41590	13636281	>100	1752	16834	10.57	115.39	0.33	14
	(5+6)-IV-2	42547	13748393	>100	2145	17221	8.83	113.03	0.34	15
	(5+6)-IV-3	41239	13309100	>100	2087	16692	8.80	113.20	0.33	14
	(5+6)-IV-4	42196	14073106	>100	1772	17079	10.60	115.20	0.34	15
	(5+6)-V-1	42505	15381153	>100	157	17204	>100	125.50	0.34	15
	(5+6)-V-2	42677	14863025	>100	1018	17274	18.66	119.93	0.34	15
	(5+6)-V-3	41109	14470932	>100	980	16639	18.67	120.11	0.33	14
	(5+6)-V-4	41281	15302579	>100	153	16708	>100	125.53	0.33	14
	(5+6)-VI-1	41816	13830795	>100	1796	16925	10.36	115.05	0.34	15
	(5+6)-VI-2	42388	14000893	>100	2073	17157	9.10	113.32	0.34	15
	(5+6)-VI-3	41398	13572115	>100	2028	16756	9.09	113.51	0.33	14
	(5+6)-VI-4	41970	14260475	>100	1799	16987	10.39	114.87	0.34	15
	(5+6)-VII-1	42448	15307740	>100	162	17181	>100	125.50	0.34	15
	(5+6)-VII-2	42735	14854087	>100	1024	17297	18.58	119.90	0.34	15
	(5+6)-VII-3	41051	14398163	>100	984	16616	18.58	120.12	0.33	14
	(5+6)-VII-4	41338	15370741	>100	157	16732	>100	125.47	0.33	14
	(5+6)-VIII-1	41624	13601433	>100	1804	16847	10.27	115.06	0.34	14
	(5+6)-VIII-2	42581	13783552	>100	2096	17235	9.04	113.34	0.34	15
	(5+6)-VIII-3	41205	13343438	>100	2035	16678	9.02	113.52	0.33	14
	(5+6)-VIII-4	42162	14037430	>100	1821	17065	10.31	114.89	0.34	15
9006	2	31085	8469141	>100	0	12582	>100	134.39	0.49	21
	(3+4)-I-1	20144	7711401	>100	635	8153	14.12	124.42	0.31	14
	(3+4)-I-2	18474	8209413	>100	152	7477	54.04	130.55	0.29	12
	(3+4)-I-3	25335	8230224	>100	209	10254	53.93	130.51	0.40	17
	(3+4)-I-4	23665	7918025	>100	747	9579	14.11	124.02	0.37	16

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-II-1	23908	7448034	>100	1072	9677	9.93	120.97	0.37	16
	(3+4)-II-2	18343	7852504	>100	602	7424	13.57	123.77	0.29	12
	(3+4)-II-3	25466	7681586	>100	838	10307	13.53	124.07	0.40	17
	(3+4)-II-4	19901	7627955	>100	891	8055	9.95	120.64	0.31	13
	(3+4)-III-1	20166	7714135	>100	605	8162	14.85	124.88	0.32	14
	(3+4)-III-2	18452	8209029	>100	180	7468	45.52	130.08	0.29	12
	(3+4)-III-3	25357	8184205	>100	249	10264	45.41	130.12	0.40	17
	(3+4)-III-4	23643	7950844	>100	709	9570	14.84	124.43	0.37	16
	(3+4)-IV-1	23983	7469111	>100	952	9707	11.21	122.46	0.37	16
	(3+4)-IV-2	18268	7854760	>100	505	7394	16.10	125.31	0.29	12
	(3+4)-IV-3	25541	7706538	>100	709	10338	16.04	125.56	0.40	17
	(3+4)-IV-4	19826	7637666	>100	785	8024	11.25	122.16	0.31	13
	(3+4)-V-1	19895	7658810	>100	699	8052	12.67	123.44	0.31	13
	(3+4)-V-2	18225	8157310	>100	215	7377	37.71	129.55	0.28	12
	(3+4)-V-3	25584	8161776	>100	302	10355	37.73	129.55	0.40	17
	(3+4)-V-4	23914	7850122	>100	839	9679	12.69	123.10	0.37	16
	(3+4)-VI-1	23834	7432012	>100	1094	9647	9.70	120.69	0.37	16
	(3+4)-VI-2	18268	7866927	>100	580	7394	14.02	124.05	0.29	12
	(3+4)-VI-3	25540	7697850	>100	813	10338	13.99	124.36	0.40	17
	(3+4)-VI-4	19975	7613647	>100	915	8085	9.72	120.36	0.31	13
	(3+4)-VII-1	19917	7661380	>100	669	8061	13.25	123.90	0.31	13
	(3+4)-VII-2	18202	8157136	>100	243	7368	33.35	129.08	0.28	12
	(3+4)-VII-3	25606	8116267	>100	342	10364	33.35	129.16	0.40	17
	(3+4)-VII-4	23892	7895803	>100	801	9670	13.28	123.48	0.37	16
	(3+4)-VIII-1	23909	7452979	>100	975	9677	10.92	122.16	0.37	16
	(3+4)-VIII-2	18193	7868695	>100	484	7364	16.74	125.60	0.28	12
	(3+4)-VIII-3	25616	7722901	>100	684	10368	16.69	125.85	0.40	17
	(3+4)-VIII-4	19900	7623755	>100	809	8055	10.96	121.87	0.31	13
	(5+6)-I-1	20144	7711401	>100	635	8153	14.12	124.42	0.31	14
	(5+6)-I-2	18474	8209413	>100	152	7477	54.04	130.55	0.29	12
	(5+6)-I-3	25335	8230224	>100	209	10254	53.93	130.51	0.40	17
	(5+6)-I-4	23665	7918025	>100	747	9579	14.11	124.02	0.37	16
	(5+6)-II-1	23908	7448034	>100	1072	9677	9.93	120.97	0.37	16
	(5+6)-II-2	18343	7852504	>100	602	7424	13.57	123.77	0.29	12
	(5+6)-II-3	25466	7681586	>100	838	10307	13.53	124.07	0.40	17
	(5+6)-II-4	19901	7627955	>100	891	8055	9.95	120.64	0.31	13
	(5+6)-III-1	20166	7714135	>100	605	8162	14.85	124.88	0.32	14
	(5+6)-III-2	18452	8209029	>100	180	7468	45.52	130.08	0.29	12
	(5+6)-III-3	25357	8184205	>100	249	10264	45.41	130.12	0.40	17
	(5+6)-III-4	23643	7950844	>100	709	9570	14.84	124.43	0.37	16
	(5+6)-IV-1	23983	7469111	>100	952	9707	11.21	122.46	0.37	16
	(5+6)-IV-2	18268	7854760	>100	505	7394	16.10	125.31	0.29	12
	(5+6)-IV-3	25541	7706538	>100	709	10338	16.04	125.56	0.40	17
	(5+6)-IV-4	19826	7637666	>100	785	8024	11.25	122.16	0.31	13
	(5+6)-V-1	19895	7658810	>100	699	8052	12.67	123.44	0.31	13
	(5+6)-V-2	18225	8157310	>100	215	7377	37.71	129.55	0.28	12
	(5+6)-V-3	25584	8161776	>100	302	10355	37.73	129.55	0.40	17
	(5+6)-V-4	23914	7850122	>100	839	9679	12.69	123.10	0.37	16
	(5+6)-VI-1	23834	7432012	>100	1094	9647	9.70	120.69	0.37	16
	(5+6)-VI-2	18268	7866927	>100	580	7394	14.02	124.05	0.29	12
	(5+6)-VI-3	25540	7697850	>100	813	10338	13.99	124.36	0.40	17
	(5+6)-VI-4	19975	7613647	>100	915	8085	9.72	120.36	0.31	13
	(5+6)-VII-1	19917	7661380	>100	669	8061	13.25	123.90	0.31	13
	(5+6)-VII-2	18202	8157136	>100	243	7368	33.35	129.08	0.28	12

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-VII-3	25606	8116267	>100	342	10364	33.35	129.16	0.40	17
	(5+6)-VII-4	23892	7895803	>100	801	9670	13.28	123.48	0.37	16
	(5+6)-VIII-1	23909	7452979	>100	975	9677	10.92	122.16	0.37	16
	(5+6)-VIII-2	18193	7868695	>100	484	7364	16.74	125.60	0.28	12
	(5+6)-VIII-3	25616	7722901	>100	684	10368	16.69	125.85	0.40	17
	(5+6)-VIII-4	19900	7623755	>100	809	8055	10.96	121.87	0.31	13
9007	2	56504	17036420	>100	0	22870	>100	127.61	0.41	18
	(3+4)-I-1	39165	16064623	>100	1031	15852	16.92	118.73	0.28	12
	(3+4)-I-2	39008	15268853	>100	1826	15789	9.51	113.33	0.28	12
	(3+4)-I-3	40359	15169018	>100	1893	16335	9.49	113.35	0.29	13
	(3+4)-I-4	40202	15832856	>100	1059	16272	16.90	118.81	0.29	12
	(3+4)-II-1	39766	16191980	>100	925	16095	19.15	119.54	0.29	12
	(3+4)-II-2	39243	15198151	>100	1771	15884	9.86	113.82	0.28	12
	(3+4)-II-3	40124	15353240	>100	1815	16240	9.84	113.73	0.29	12
	(3+4)-II-4	39601	15925384	>100	919	16029	19.18	119.66	0.28	12
	(3+4)-III-1	39126	16123304	>100	974	15836	17.88	119.10	0.28	12
	(3+4)-III-2	39047	15212522	>100	1883	15804	9.23	112.97	0.28	12
	(3+4)-III-3	40320	15125568	>100	1949	16320	9.21	112.97	0.29	13
	(3+4)-III-4	40241	15877042	>100	1003	16288	17.87	119.20	0.29	12
	(3+4)-IV-1	39637	16042752	>100	1110	16043	15.89	118.26	0.28	12
	(3+4)-IV-2	39372	15012606	>100	1962	15936	8.94	112.61	0.28	12
	(3+4)-IV-3	39995	15207380	>100	2001	16188	8.90	112.47	0.29	12
	(3+4)-IV-4	39730	15734060	>100	1110	16081	15.94	118.40	0.29	12
	(3+4)-V-1	39112	16173419	>100	918	15831	18.97	119.49	0.28	12
	(3+4)-V-2	38955	15373099	>100	1714	15767	10.12	114.07	0.28	12
	(3+4)-V-3	40412	15266909	>100	1777	16357	10.13	114.11	0.29	13
	(3+4)-V-4	40255	15931969	>100	943	16293	19.00	119.59	0.29	12
	(3+4)-VI-1	39750	16161780	>100	959	16089	18.46	119.31	0.29	12
	(3+4)-VI-2	39227	15229114	>100	1737	15877	10.05	114.04	0.28	12
	(3+4)-VI-3	40140	15382855	>100	1781	16247	10.04	113.96	0.29	12
	(3+4)-VI-4	39617	15893344	>100	954	16035	18.50	119.43	0.28	12
	(3+4)-VII-1	39073	16232466	>100	862	15815	20.18	119.87	0.28	12
	(3+4)-VII-2	38994	15316415	>100	1770	15783	9.81	113.70	0.28	12
	(3+4)-VII-3	40373	15223398	>100	1833	16341	9.81	113.74	0.29	13
	(3+4)-VII-4	40294	15976212	>100	887	16309	20.23	119.98	0.29	12
	(3+4)-VIII-1	39621	16012610	>100	1145	16037	15.41	118.02	0.28	12
	(3+4)-VIII-2	39356	15043223	>100	1928	15929	9.09	112.83	0.28	12
	(3+4)-VIII-3	40011	15236933	>100	1966	16194	9.06	112.70	0.29	12
	(3+4)-VIII-4	39746	15702374	>100	1144	16087	15.47	118.18	0.29	12
	(5+6)-I-1	39165	16064623	>100	1031	15852	16.92	118.73	0.28	12
	(5+6)-I-2	39008	15268853	>100	1826	15789	9.51	113.33	0.28	12
	(5+6)-I-3	40359	15169018	>100	1893	16335	9.49	113.35	0.29	13
	(5+6)-I-4	40202	15832856	>100	1059	16272	16.90	118.81	0.29	12
	(5+6)-II-1	39766	16191980	>100	925	16095	19.15	119.54	0.29	12
	(5+6)-II-2	39243	15198151	>100	1771	15884	9.86	113.82	0.28	12
	(5+6)-II-3	40124	15353240	>100	1815	16240	9.84	113.73	0.29	12
	(5+6)-II-4	39601	15925384	>100	919	16029	19.18	119.66	0.28	12
	(5+6)-III-1	39126	16123304	>100	974	15836	17.88	119.10	0.28	12
	(5+6)-III-2	39047	15212522	>100	1883	15804	9.23	112.97	0.28	12
	(5+6)-III-3	40320	15125568	>100	1949	16320	9.21	112.97	0.29	13
	(5+6)-III-4	40241	15877042	>100	1003	16288	17.87	119.20	0.29	12
	(5+6)-IV-1	39637	16042752	>100	1110	16043	15.89	118.26	0.28	12
	(5+6)-IV-2	39372	15012606	>100	1962	15936	8.94	112.61	0.28	12
	(5+6)-IV-3	39995	15207380	>100	2001	16188	8.90	112.47	0.29	12

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-IV-4	39730	15734060	>100	1110	16081	15.94	118.40	0.29	12
	(5+6)-V-1	39112	16173419	>100	918	15831	18.97	119.49	0.28	12
	(5+6)-V-2	38955	15373099	>100	1714	15767	10.12	114.07	0.28	12
	(5+6)-V-3	40412	15266909	>100	1777	16357	10.13	114.11	0.29	13
	(5+6)-V-4	40255	15931969	>100	943	16293	19.00	119.59	0.29	12
	(5+6)-VI-1	39750	16161780	>100	959	16089	18.46	119.31	0.29	12
	(5+6)-VI-2	39227	15229114	>100	1737	15877	10.05	114.04	0.28	12
	(5+6)-VI-3	40140	15382855	>100	1781	16247	10.04	113.96	0.29	12
	(5+6)-VI-4	39617	15893344	>100	954	16035	18.50	119.43	0.28	12
	(5+6)-VII-1	39073	16232466	>100	862	15815	20.18	119.87	0.28	12
	(5+6)-VII-2	38994	15316415	>100	1770	15783	9.81	113.70	0.28	12
	(5+6)-VII-3	40373	15223398	>100	1833	16341	9.81	113.74	0.29	13
	(5+6)-VII-4	40294	15976212	>100	887	16309	20.23	119.98	0.29	12
	(5+6)-VIII-1	39621	16012610	>100	1145	16037	15.41	118.02	0.28	12
	(5+6)-VIII-2	39356	15043223	>100	1928	15929	9.09	112.83	0.28	12
	(5+6)-VIII-3	40011	15236933	>100	1966	16194	9.06	112.70	0.29	12
	(5+6)-VIII-4	39746	15702374	>100	1144	16087	15.47	118.18	0.29	12
9008	2	49713	14017347	>100	0	20122	>100	128.97	0.45	19
	(3+4)-I-1	36080	12216072	>100	1697	14604	9.47	114.85	0.33	14
	(3+4)-I-2	33914	12545863	>100	1410	13727	10.71	116.17	0.31	13
	(3+4)-I-3	36181	12657181	>100	1507	14644	10.69	116.07	0.33	14
	(3+4)-I-4	34015	12548480	>100	1601	13768	9.46	114.63	0.31	13
	(3+4)-II-1	38642	12821703	>100	865	15641	19.90	121.45	0.35	15
	(3+4)-II-2	31423	13757863	>100	133	12718	>100	126.16	0.29	12
	(3+4)-II-3	38673	13433351	>100	164	15653	>100	126.34	0.35	15
	(3+4)-II-4	31453	13114380	>100	703	12731	19.93	121.28	0.29	12
	(3+4)-III-1	35985	12281386	>100	1606	14565	9.97	115.48	0.33	14
	(3+4)-III-2	34010	12478873	>100	1495	13766	10.13	115.54	0.31	13
	(3+4)-III-3	36086	12587666	>100	1590	14606	10.10	115.44	0.33	14
	(3+4)-III-4	34110	12617621	>100	1523	13806	9.97	115.26	0.31	13
	(3+4)-IV-1	38325	13045910	>100	551	15512	30.97	123.62	0.35	15
	(3+4)-IV-2	31740	13519528	>100	388	12847	36.42	123.96	0.29	12
	(3+4)-IV-3	38355	13194996	>100	471	15524	36.28	124.14	0.35	15
	(3+4)-IV-4	31770	13351065	>100	455	12859	31.07	123.45	0.29	12
	(3+4)-V-1	36041	12195944	>100	1734	14588	9.25	114.56	0.33	14
	(3+4)-V-2	33875	12526253	>100	1445	13711	10.44	115.88	0.31	13
	(3+4)-V-3	36220	12619220	>100	1544	14660	10.44	115.82	0.33	14
	(3+4)-V-4	34054	12532142	>100	1636	13784	9.27	114.37	0.31	13
	(3+4)-VI-1	38631	12815651	>100	877	15636	19.62	121.36	0.35	15
	(3+4)-VI-2	31411	13744619	>100	143	12714	97.95	126.07	0.29	12
	(3+4)-VI-3	38684	13421348	>100	176	15658	97.78	126.26	0.35	15
	(3+4)-VI-4	31465	13109584	>100	712	12735	19.67	121.20	0.29	12
	(3+4)-VII-1	35946	12261328	>100	1643	14549	9.74	115.19	0.33	14
	(3+4)-VII-2	33971	12459183	>100	1530	13750	9.89	115.25	0.31	13
	(3+4)-VII-3	36125	12549911	>100	1627	14622	9.89	115.19	0.33	14
	(3+4)-VII-4	34149	12601145	>100	1558	13822	9.76	115.00	0.31	13
	(3+4)-VIII-1	38313	13039930	>100	563	15507	30.31	123.54	0.35	15
	(3+4)-VIII-2	31729	13506405	>100	398	12842	35.52	123.88	0.29	12
	(3+4)-VIII-3	38367	13183206	>100	482	15529	35.41	124.06	0.35	15
	(3+4)-VIII-4	31782	13346125	>100	465	12864	30.43	123.37	0.29	12
	(5+6)-I-1	36080	12216072	>100	1697	14604	9.47	114.85	0.33	14
	(5+6)-I-2	33914	12545863	>100	1410	13727	10.71	116.17	0.31	13
	(5+6)-I-3	36181	12657181	>100	1507	14644	10.69	116.07	0.33	14
	(5+6)-I-4	34015	12548480	>100	1601	13768	9.46	114.63	0.31	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-II-1	38642	12821703	>100	865	15641	19.90	121.45	0.35	15
	(5+6)-II-2	31423	13757863	>100	133	12718	>100	126.16	0.29	12
	(5+6)-II-3	38673	13433351	>100	164	15653	>100	126.34	0.35	15
	(5+6)-II-4	31453	13114380	>100	703	12731	19.93	121.28	0.29	12
	(5+6)-III-1	35985	12281386	>100	1606	14565	9.97	115.48	0.33	14
	(5+6)-III-2	34010	12478873	>100	1495	13766	10.13	115.54	0.31	13
	(5+6)-III-3	36086	12587666	>100	1590	14606	10.10	115.44	0.33	14
	(5+6)-III-4	34110	12617621	>100	1523	13806	9.97	115.26	0.31	13
	(5+6)-IV-1	38325	13045910	>100	551	15512	30.97	123.62	0.35	15
	(5+6)-IV-2	31740	13519528	>100	388	12847	36.42	123.96	0.29	12
	(5+6)-IV-3	38355	13194996	>100	471	15524	36.28	124.14	0.35	15
	(5+6)-IV-4	31770	13351065	>100	455	12859	31.07	123.45	0.29	12
	(5+6)-V-1	36041	12195944	>100	1734	14588	9.25	114.56	0.33	14
	(5+6)-V-2	33875	12526253	>100	1445	13711	10.44	115.88	0.31	13
	(5+6)-V-3	36220	12619220	>100	1544	14660	10.44	115.82	0.33	14
	(5+6)-V-4	34054	12532142	>100	1636	13784	9.27	114.37	0.31	13
	(5+6)-VI-1	38631	12815651	>100	877	15636	19.62	121.36	0.35	15
	(5+6)-VI-2	31411	13744619	>100	143	12714	97.95	126.07	0.29	12
	(5+6)-VI-3	38684	13421348	>100	176	15658	97.78	126.26	0.35	15
	(5+6)-VI-4	31465	13109584	>100	712	12735	19.67	121.20	0.29	12
	(5+6)-VII-1	35946	12261328	>100	1643	14549	9.74	115.19	0.33	14
	(5+6)-VII-2	33971	12459183	>100	1530	13750	9.89	115.25	0.31	13
	(5+6)-VII-3	36125	12549911	>100	1627	14622	9.89	115.19	0.33	14
	(5+6)-VII-4	34149	12601145	>100	1558	13822	9.76	115.00	0.31	13
	(5+6)-VIII-1	38313	13039930	>100	563	15507	30.31	123.54	0.35	15
	(5+6)-VIII-2	31729	13506405	>100	398	12842	35.52	123.88	0.29	12
	(5+6)-VIII-3	38367	13183206	>100	482	15529	35.41	124.06	0.35	15
	(5+6)-VIII-4	31782	13346125	>100	465	12864	30.43	123.37	0.29	12
9009	2	62083	15803746	>100	0	25128	>100	128.10	0.50	22
	(3+4)-I-1	42213	15501719	>100	14	17086	>100	126.43	0.34	15
	(3+4)-I-2	42562	14735798	>100	1186	17227	15.98	118.85	0.34	15
	(3+4)-I-3	43002	14559550	>100	1200	17405	15.95	118.92	0.35	15
	(3+4)-I-4	43351	15691928	>100	14	17547	>100	126.34	0.35	15
	(3+4)-II-1	42082	13861216	>100	1756	17033	10.67	115.38	0.34	15
	(3+4)-II-2	43245	13768405	>100	2167	17504	8.89	113.10	0.35	15
	(3+4)-II-3	42319	13590219	>100	2125	17129	8.87	113.16	0.34	15
	(3+4)-II-4	43482	14045066	>100	1812	17600	10.69	115.30	0.35	15
	(3+4)-III-1	42303	15561528	>100	9	17122	>100	126.43	0.34	15
	(3+4)-III-2	42472	14756143	>100	1187	17191	15.93	118.81	0.34	15
	(3+4)-III-3	43092	14607538	>100	1208	17442	15.89	118.86	0.35	15
	(3+4)-III-4	43261	15670133	>100	9	17510	>100	126.39	0.35	15
	(3+4)-IV-1	42383	14020156	>100	1785	17155	10.57	115.19	0.34	15
	(3+4)-IV-2	42945	13918805	>100	2165	17382	8.83	112.94	0.35	15
	(3+4)-IV-3	42619	13744723	>100	2157	17250	8.80	112.97	0.34	15
	(3+4)-IV-4	43182	14197610	>100	1813	17478	10.60	115.14	0.35	15
	(3+4)-V-1	42268	15399404	>100	157	17108	>100	125.49	0.34	15
	(3+4)-V-2	42617	14857228	>100	1017	17249	18.66	119.93	0.34	15
	(3+4)-V-3	42947	14681395	>100	1024	17383	18.67	120.01	0.35	15
	(3+4)-V-4	43296	15587781	>100	160	17524	>100	125.41	0.35	15
	(3+4)-VI-1	42099	13826045	>100	1808	17040	10.36	115.05	0.34	15
	(3+4)-VI-2	43262	13802926	>100	2116	17510	9.10	113.41	0.35	15
	(3+4)-VI-3	42302	13625160	>100	2073	17122	9.09	113.48	0.34	15
	(3+4)-VI-4	43466	14010096	>100	1863	17593	10.39	114.99	0.35	15
	(3+4)-VII-1	42358	15451345	>100	161	17145	>100	125.43	0.34	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-VII-2	42527	14900659	>100	1019	17213	18.58	119.88	0.34	15
	(3+4)-VII-3	43037	14729992	>100	1031	17419	18.58	119.96	0.35	15
	(3+4)-VII-4	43206	15535151	>100	164	17488	>100	125.40	0.35	15
	(3+4)-VIII-1	42399	13984372	>100	1838	17161	10.27	114.87	0.34	15
	(3+4)-VIII-2	42962	13953660	>100	2115	17389	9.04	113.25	0.35	15
	(3+4)-VIII-3	42603	13780267	>100	2104	17244	9.02	113.29	0.34	15
	(3+4)-VIII-4	43165	14162303	>100	1864	17471	10.31	114.82	0.35	15
	(5+6)-I-1	42213	15501719	>100	14	17086	>100	126.43	0.34	15
	(5+6)-I-2	42562	14735798	>100	1186	17227	15.98	118.85	0.34	15
	(5+6)-I-3	43002	14559550	>100	1200	17405	15.95	118.92	0.35	15
	(5+6)-I-4	43351	15691928	>100	14	17547	>100	126.34	0.35	15
	(5+6)-II-1	42082	13861216	>100	1756	17033	10.67	115.38	0.34	15
	(5+6)-II-2	43245	13768405	>100	2167	17504	8.89	113.10	0.35	15
	(5+6)-II-3	42319	13590219	>100	2125	17129	8.87	113.16	0.34	15
	(5+6)-II-4	43482	14045066	>100	1812	17600	10.69	115.30	0.35	15
	(5+6)-III-1	42303	15561528	>100	9	17122	>100	126.43	0.34	15
	(5+6)-III-2	42472	14756143	>100	1187	17191	15.93	118.81	0.34	15
	(5+6)-III-3	43092	14607538	>100	1208	17442	15.89	118.86	0.35	15
	(5+6)-III-4	43261	15670133	>100	9	17510	>100	126.39	0.35	15
	(5+6)-IV-1	42383	14020156	>100	1785	17155	10.57	115.19	0.34	15
	(5+6)-IV-2	42945	13918805	>100	2165	17382	8.83	112.94	0.35	15
	(5+6)-IV-3	42619	13744723	>100	2157	17250	8.80	112.97	0.34	15
	(5+6)-IV-4	43182	14197610	>100	1813	17478	10.60	115.14	0.35	15
	(5+6)-V-1	42268	15399404	>100	157	17108	>100	125.49	0.34	15
	(5+6)-V-2	42617	14857228	>100	1017	17249	18.66	119.93	0.34	15
	(5+6)-V-3	42947	14681395	>100	1024	17383	18.67	120.01	0.35	15
	(5+6)-V-4	43296	15587781	>100	160	17524	>100	125.41	0.35	15
	(5+6)-VI-1	42099	13826045	>100	1808	17040	10.36	115.05	0.34	15
	(5+6)-VI-2	43262	13802926	>100	2116	17510	9.10	113.41	0.35	15
	(5+6)-VI-3	42302	13625160	>100	2073	17122	9.09	113.48	0.34	15
	(5+6)-VI-4	43466	14010096	>100	1863	17593	10.39	114.99	0.35	15
	(5+6)-VII-1	42358	15451345	>100	161	17145	>100	125.43	0.34	15
	(5+6)-VII-2	42527	14900659	>100	1019	17213	18.58	119.88	0.34	15
	(5+6)-VII-3	43037	14729992	>100	1031	17419	18.58	119.96	0.35	15
	(5+6)-VII-4	43206	15535151	>100	164	17488	>100	125.40	0.35	15
	(5+6)-VIII-1	42399	13984372	>100	1838	17161	10.27	114.87	0.34	15
	(5+6)-VIII-2	42962	13953660	>100	2115	17389	9.04	113.25	0.35	15
	(5+6)-VIII-3	42603	13780267	>100	2104	17244	9.02	113.29	0.34	15
	(5+6)-VIII-4	43165	14162303	>100	1864	17471	10.31	114.82	0.35	15
9010	2	279033	68294934	>100	0	112940	>100	123.17	0.50	22
	(3+4)-I-1	191408	60490998	>100	9011	77473	9.46	108.85	0.34	15
	(3+4)-I-2	192441	61130294	>100	8220	77891	10.42	109.99	0.35	15
	(3+4)-I-3	191509	60843192	>100	8198	77514	10.40	109.97	0.34	15
	(3+4)-I-4	192542	60226733	>100	9073	77932	9.45	108.84	0.35	15
	(3+4)-II-1	190238	64270811	>100	3943	76999	21.48	115.85	0.34	15
	(3+4)-II-2	193682	66489508	>100	1208	78393	71.36	119.80	0.35	15
	(3+4)-II-3	190268	66375814	>100	1190	77012	71.18	119.80	0.34	15
	(3+4)-II-4	193712	64214185	>100	4009	78406	21.51	115.86	0.35	15
	(3+4)-III-1	191343	60877802	>100	8549	77447	9.96	109.47	0.34	15
	(3+4)-III-2	192506	60742972	>100	8684	77918	9.87	109.36	0.35	15
	(3+4)-III-3	191444	60532202	>100	8658	77488	9.84	109.34	0.34	15
	(3+4)-III-4	192607	60536769	>100	8610	77959	9.96	109.48	0.35	15
	(3+4)-IV-1	190021	65623351	>100	2414	76912	35.04	118.02	0.34	15
	(3+4)-IV-2	193899	65131473	>100	2762	78481	31.26	117.61	0.35	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cm ²]	qe [kg/cm ²]	w [mm]
	(3+4)-IV-3	190052	65294587	>100	2718	76924	31.14	117.59	0.34	15
	(3+4)-IV-4	193929	65284604	>100	2457	78493	35.15	118.04	0.35	15
	(3+4)-V-1	191416	60369220	>100	9188	77476	9.28	108.61	0.34	15
	(3+4)-V-2	192449	61008627	>100	8397	77894	10.20	109.75	0.35	15
	(3+4)-V-3	191501	60715002	>100	8351	77511	10.21	109.76	0.34	15
	(3+4)-V-4	192534	60100308	>100	9226	77929	9.29	108.64	0.35	15
	(3+4)-VI-1	190240	64234579	>100	3994	77000	21.21	115.77	0.34	15
	(3+4)-VI-2	193684	66453446	>100	1259	78394	68.50	119.73	0.35	15
	(3+4)-VI-3	190266	66332876	>100	1239	77011	68.38	119.73	0.34	15
	(3+4)-VI-4	193710	64173128	>100	4057	78405	21.26	115.79	0.35	15
	(3+4)-VII-1	191351	60755968	>100	8726	77450	9.76	109.23	0.34	15
	(3+4)-VII-2	192514	60621360	>100	8861	77921	9.67	109.12	0.35	15
	(3+4)-VII-3	191436	60404834	>100	8811	77484	9.67	109.13	0.34	15
	(3+4)-VII-4	192599	60409525	>100	8764	77955	9.78	109.27	0.35	15
	(3+4)-VIII-1	190024	65587096	>100	2464	76913	34.33	117.95	0.34	15
	(3+4)-VIII-2	193901	65095425	>100	2813	78482	30.69	117.54	0.35	15
	(3+4)-VIII-3	190049	65252516	>100	2766	76923	30.60	117.52	0.34	15
	(3+4)-VIII-4	193927	65242692	>100	2506	78493	34.46	117.97	0.35	15
	(5+6)-I-1	191408	60490998	>100	9011	77473	9.46	108.85	0.34	15
	(5+6)-I-2	192441	61130294	>100	8220	77891	10.42	109.99	0.35	15
	(5+6)-I-3	191509	60843192	>100	8198	77514	10.40	109.97	0.34	15
	(5+6)-I-4	192542	60226733	>100	9073	77932	9.45	108.84	0.35	15
	(5+6)-II-1	190238	64270811	>100	3943	76999	21.48	115.85	0.34	15
	(5+6)-II-2	193682	66489508	>100	1208	78393	71.36	119.80	0.35	15
	(5+6)-II-3	190268	66375814	>100	1190	77012	71.18	119.80	0.34	15
	(5+6)-II-4	193712	64214185	>100	4009	78406	21.51	115.86	0.35	15
	(5+6)-III-1	191343	60877802	>100	8549	77447	9.96	109.47	0.34	15
	(5+6)-III-2	192506	60742972	>100	8684	77918	9.87	109.36	0.35	15
	(5+6)-III-3	191444	60532202	>100	8658	77488	9.84	109.34	0.34	15
	(5+6)-III-4	192607	60536769	>100	8610	77959	9.96	109.48	0.35	15
	(5+6)-IV-1	190021	65623351	>100	2414	76912	35.04	118.02	0.34	15
	(5+6)-IV-2	193899	65131473	>100	2762	78481	31.26	117.61	0.35	15
	(5+6)-IV-3	190052	65294587	>100	2718	76924	31.14	117.59	0.34	15
	(5+6)-IV-4	193929	65284604	>100	2457	78493	35.15	118.04	0.35	15
	(5+6)-V-1	191416	60369220	>100	9188	77476	9.28	108.61	0.34	15
	(5+6)-V-2	192449	61008627	>100	8397	77894	10.20	109.75	0.35	15
	(5+6)-V-3	191501	60715002	>100	8351	77511	10.21	109.76	0.34	15
	(5+6)-V-4	192534	60100308	>100	9226	77929	9.29	108.64	0.35	15
	(5+6)-VI-1	190240	64234579	>100	3994	77000	21.21	115.77	0.34	15
	(5+6)-VI-2	193684	66453446	>100	1259	78394	68.50	119.73	0.35	15
	(5+6)-VI-3	190266	66332876	>100	1239	77011	68.38	119.73	0.34	15
	(5+6)-VI-4	193710	64173128	>100	4057	78405	21.26	115.79	0.35	15
	(5+6)-VII-1	191351	60755968	>100	8726	77450	9.76	109.23	0.34	15
	(5+6)-VII-2	192514	60621360	>100	8861	77921	9.67	109.12	0.35	15
	(5+6)-VII-3	191436	60404834	>100	8811	77484	9.67	109.13	0.34	15
	(5+6)-VII-4	192599	60409525	>100	8764	77955	9.78	109.27	0.35	15
	(5+6)-VIII-1	190024	65587096	>100	2464	76913	34.33	117.95	0.34	15
	(5+6)-VIII-2	193901	65095425	>100	2813	78482	30.69	117.54	0.35	15
	(5+6)-VIII-3	190049	65252516	>100	2766	76923	30.60	117.52	0.34	15
	(5+6)-VIII-4	193927	65242692	>100	2506	78493	34.46	117.97	0.35	15
9011	2	94723	23848216	>100	0	38339	>100	125.87	0.49	21
	(3+4)-I-1	65844	23587684	>100	21	26651	>100	124.14	0.34	15
	(3+4)-I-2	66240	22010066	>100	1845	26811	15.98	116.66	0.34	15
	(3+4)-I-3	64492	22201306	>100	1800	26103	15.95	116.61	0.33	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-I-4	64888	23467579	>100	21	26263	>100	124.16	0.34	14
	(3+4)-II-1	64909	21651973	>100	2709	26272	10.67	112.92	0.34	15
	(3+4)-II-2	66229	20750019	>100	3318	26806	8.89	110.83	0.34	15
	(3+4)-II-3	64503	21240239	>100	3240	26108	8.87	110.70	0.33	14
	(3+4)-II-4	65823	21172388	>100	2743	26642	10.69	113.03	0.34	15
	(3+4)-III-1	65764	23650518	>100	14	26618	>100	124.16	0.34	15
	(3+4)-III-2	66320	21952020	>100	1854	26843	15.93	116.65	0.34	15
	(3+4)-III-3	64412	22250287	>100	1805	26071	15.89	116.57	0.33	14
	(3+4)-III-4	64968	23415466	>100	14	26296	>100	124.20	0.34	15
	(3+4)-IV-1	64642	21797196	>100	2723	26164	10.57	112.78	0.33	14
	(3+4)-IV-2	66495	20568295	>100	3353	26914	8.83	110.78	0.34	15
	(3+4)-IV-3	64236	21354369	>100	3251	26000	8.80	110.57	0.33	14
	(3+4)-IV-4	66090	20985664	>100	2775	26750	10.60	112.98	0.34	15
	(3+4)-V-1	65661	23473190	>100	243	26577	>100	123.19	0.34	15
	(3+4)-V-2	66057	22271783	>100	1576	26737	18.66	117.72	0.34	15
	(3+4)-V-3	64675	22347342	>100	1543	26177	18.67	117.71	0.33	14
	(3+4)-V-4	65071	23227404	>100	241	26338	>100	123.24	0.34	15
	(3+4)-VI-1	64854	21608012	>100	2786	26250	10.36	112.59	0.34	14
	(3+4)-VI-2	66174	20824465	>100	3237	26784	9.10	111.14	0.34	15
	(3+4)-VI-3	64558	21283932	>100	3163	26130	9.09	111.02	0.33	14
	(3+4)-VI-4	65878	21096859	>100	2823	26664	10.39	112.72	0.34	15
	(3+4)-VII-1	65581	23524448	>100	250	26544	>100	123.15	0.34	15
	(3+4)-VII-2	66137	22212920	>100	1585	26769	18.58	117.70	0.34	15
	(3+4)-VII-3	64595	22396658	>100	1548	26145	18.58	117.67	0.33	14
	(3+4)-VII-4	65151	23164850	>100	248	26370	>100	123.22	0.34	15
	(3+4)-VIII-1	64587	21717132	>100	2800	26142	10.27	112.47	0.33	14
	(3+4)-VIII-2	66440	20641970	>100	3271	26892	9.04	111.09	0.34	15
	(3+4)-VIII-3	64291	21433746	>100	3175	26022	9.02	110.89	0.33	14
	(3+4)-VIII-4	66145	20910922	>100	2856	26772	10.31	112.67	0.34	15
	(5+6)-I-1	65844	23587684	>100	21	26651	>100	124.14	0.34	15
	(5+6)-I-2	66240	22010066	>100	1845	26811	15.98	116.66	0.34	15
	(5+6)-I-3	64492	22201306	>100	1800	26103	15.95	116.61	0.33	14
	(5+6)-I-4	64888	23467579	>100	21	26263	>100	124.16	0.34	14
	(5+6)-II-1	64909	21651973	>100	2709	26272	10.67	112.92	0.34	15
	(5+6)-II-2	66229	20750019	>100	3318	26806	8.89	110.83	0.34	15
	(5+6)-II-3	64503	21240239	>100	3240	26108	8.87	110.70	0.33	14
	(5+6)-II-4	65823	21172388	>100	2743	26642	10.69	113.03	0.34	15
	(5+6)-III-1	65764	23650518	>100	14	26618	>100	124.16	0.34	15
	(5+6)-III-2	66320	21952020	>100	1854	26843	15.93	116.65	0.34	15
	(5+6)-III-3	64412	22250287	>100	1805	26071	15.89	116.57	0.33	14
	(5+6)-III-4	64968	23415466	>100	14	26296	>100	124.20	0.34	15
	(5+6)-IV-1	64642	21797196	>100	2723	26164	10.57	112.78	0.33	14
	(5+6)-IV-2	66495	20568295	>100	3353	26914	8.83	110.78	0.34	15
	(5+6)-IV-3	64236	21354369	>100	3251	26000	8.80	110.57	0.33	14
	(5+6)-IV-4	66090	20985664	>100	2775	26750	10.60	112.98	0.34	15
	(5+6)-V-1	65661	23473190	>100	243	26577	>100	123.19	0.34	15
	(5+6)-V-2	66057	22271783	>100	1576	26737	18.66	117.72	0.34	15
	(5+6)-V-3	64675	22347342	>100	1543	26177	18.67	117.71	0.33	14
	(5+6)-V-4	65071	23227404	>100	241	26338	>100	123.24	0.34	15
	(5+6)-VI-1	64854	21608012	>100	2786	26250	10.36	112.59	0.34	14
	(5+6)-VI-2	66174	20824465	>100	3237	26784	9.10	111.14	0.34	15
	(5+6)-VI-3	64558	21283932	>100	3163	26130	9.09	111.02	0.33	14
	(5+6)-VI-4	65878	21096859	>100	2823	26664	10.39	112.72	0.34	15
	(5+6)-VII-1	65581	23524448	>100	250	26544	>100	123.15	0.34	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-VII-2	66137	22212920	>100	1585	26769	18.58	117.70	0.34	15
	(5+6)-VII-3	64595	22396658	>100	1548	26145	18.58	117.67	0.33	14
	(5+6)-VII-4	65151	23164850	>100	248	26370	>100	123.22	0.34	15
	(5+6)-VIII-1	64587	21717132	>100	2800	26142	10.27	112.47	0.33	14
	(5+6)-VIII-2	66440	20641970	>100	3271	26892	9.04	111.09	0.34	15
	(5+6)-VIII-3	64291	21433746	>100	3175	26022	9.02	110.89	0.33	14
	(5+6)-VIII-4	66145	20910922	>100	2856	26772	10.31	112.67	0.34	15
9012	2	263644	68238110	>100	0	106711	>100	123.17	0.48	21
	(3+4)-I-1	180663	59753452	>100	8505	73124	9.46	108.87	0.33	14
	(3+4)-I-2	190021	60053181	>100	8107	76912	10.44	110.03	0.34	15
	(3+4)-I-3	177898	59999333	>100	7606	72005	10.41	110.01	0.32	14
	(3+4)-I-4	187256	59785793	>100	8824	75792	9.45	108.86	0.34	15
	(3+4)-II-1	168779	63722463	>100	3511	68314	21.40	115.84	0.30	13
	(3+4)-II-2	199970	65538803	>100	1230	80939	72.40	119.85	0.36	16
	(3+4)-II-3	167949	65397325	>100	1035	67978	72.22	119.85	0.30	13
	(3+4)-II-4	199141	63777087	>100	4136	80603	21.44	115.85	0.36	16
	(3+4)-III-1	180772	59646465	>100	8077	73168	9.96	109.50	0.33	14
	(3+4)-III-2	189913	60139066	>100	8557	76868	9.88	109.39	0.34	15
	(3+4)-III-3	178007	60111604	>100	8041	72049	9.86	109.36	0.32	14
	(3+4)-III-4	187147	59696816	>100	8366	75749	9.96	109.50	0.34	15
	(3+4)-IV-1	169140	64108459	>100	2162	68460	34.84	118.04	0.31	13
	(3+4)-IV-2	199609	64548941	>100	2825	80792	31.46	117.65	0.36	16
	(3+4)-IV-3	168310	64401699	>100	2391	68124	31.33	117.64	0.30	13
	(3+4)-IV-4	198779	64323321	>100	2533	80457	34.94	118.04	0.36	15
	(3+4)-V-1	181276	59460844	>100	8702	73372	9.27	108.63	0.33	14
	(3+4)-V-2	190634	59768654	>100	8309	77160	10.21	109.79	0.34	15
	(3+4)-V-3	177286	59712964	>100	7724	71757	10.22	109.80	0.32	14
	(3+4)-V-4	186643	59511806	>100	8945	75544	9.29	108.65	0.34	15
	(3+4)-VI-1	168962	63738567	>100	3560	68388	21.13	115.76	0.30	13
	(3+4)-VI-2	200154	65451475	>100	1283	81013	69.43	119.78	0.36	16
	(3+4)-VI-3	167765	65299503	>100	1078	67904	69.32	119.78	0.30	13
	(3+4)-VI-4	198957	63786425	>100	4182	80528	21.18	115.78	0.36	16
	(3+4)-VII-1	181385	59355503	>100	8272	73416	9.76	109.27	0.33	14
	(3+4)-VII-2	190525	59853044	>100	8761	77116	9.68	109.15	0.34	15
	(3+4)-VII-3	177394	59827837	>100	8157	71801	9.68	109.15	0.32	14
	(3+4)-VII-4	186535	59420402	>100	8489	75501	9.78	109.29	0.34	15
	(3+4)-VIII-1	169324	64013919	>100	2209	68534	34.13	117.97	0.31	13
	(3+4)-VIII-2	199793	64557528	>100	2881	80867	30.88	117.57	0.36	16
	(3+4)-VIII-3	168127	64419474	>100	2432	68050	30.78	117.56	0.30	13
	(3+4)-VIII-4	198596	64236229	>100	2581	80382	34.26	117.97	0.36	15
	(5+6)-I-1	180663	59753452	>100	8505	73124	9.46	108.87	0.33	14
	(5+6)-I-2	190021	60053181	>100	8107	76912	10.44	110.03	0.34	15
	(5+6)-I-3	177898	59999333	>100	7606	72005	10.41	110.01	0.32	14
	(5+6)-I-4	187256	59785793	>100	8824	75792	9.45	108.86	0.34	15
	(5+6)-II-1	168779	63722463	>100	3511	68314	21.40	115.84	0.30	13
	(5+6)-II-2	199970	65538803	>100	1230	80939	72.40	119.85	0.36	16
	(5+6)-II-3	167949	65397325	>100	1035	67978	72.22	119.85	0.30	13
	(5+6)-II-4	199141	63777087	>100	4136	80603	21.44	115.85	0.36	16
	(5+6)-III-1	180772	59646465	>100	8077	73168	9.96	109.50	0.33	14
	(5+6)-III-2	189913	60139066	>100	8557	76868	9.88	109.39	0.34	15
	(5+6)-III-3	178007	60111604	>100	8041	72049	9.86	109.36	0.32	14
	(5+6)-III-4	187147	59696816	>100	8366	75749	9.96	109.50	0.34	15
	(5+6)-IV-1	169140	64108459	>100	2162	68460	34.84	118.04	0.31	13
	(5+6)-IV-2	199609	64548941	>100	2825	80792	31.46	117.65	0.36	16

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-IV-3	168310	64401699	>100	2391	68124	31.33	117.64	0.30	13
	(5+6)-IV-4	198779	64323321	>100	2533	80457	34.94	118.04	0.36	15
	(5+6)-V-1	181276	59460844	>100	8702	73372	9.27	108.63	0.33	14
	(5+6)-V-2	190634	59768654	>100	8309	77160	10.21	109.79	0.34	15
	(5+6)-V-3	177286	59712964	>100	7724	71757	10.22	109.80	0.32	14
	(5+6)-V-4	186643	59511806	>100	8945	75544	9.29	108.65	0.34	15
	(5+6)-VI-1	168962	63738567	>100	3560	68388	21.13	115.76	0.30	13
	(5+6)-VI-2	200154	65451475	>100	1283	81013	69.43	119.78	0.36	16
	(5+6)-VI-3	167765	65299503	>100	1078	67904	69.32	119.78	0.30	13
	(5+6)-VI-4	198957	63786425	>100	4182	80528	21.18	115.78	0.36	16
	(5+6)-VII-1	181385	59355503	>100	8272	73416	9.76	109.27	0.33	14
	(5+6)-VII-2	190525	59853044	>100	8761	77116	9.68	109.15	0.34	15
	(5+6)-VII-3	177394	59827837	>100	8157	71801	9.68	109.15	0.32	14
	(5+6)-VII-4	186535	59420402	>100	8489	75501	9.78	109.29	0.34	15
	(5+6)-VIII-1	169324	64013919	>100	2209	68534	34.13	117.97	0.31	13
	(5+6)-VIII-2	199793	64557528	>100	2881	80867	30.88	117.57	0.36	16
	(5+6)-VIII-3	168127	64419474	>100	2432	68050	30.78	117.56	0.30	13
	(5+6)-VIII-4	198596	64236229	>100	2581	80382	34.26	117.97	0.36	15
9013	2	25182	6946997	>100	0	10193	>100	137.70	0.49	21
	(3+4)-I-1	17575	6514596	>100	494	7114	15.83	128.30	0.34	15
	(3+4)-I-2	16664	6300957	>100	795	6745	9.33	122.93	0.32	14
	(3+4)-I-3	18747	6062833	>100	896	7588	9.31	123.64	0.36	16
	(3+4)-I-4	17836	6431896	>100	502	7219	15.82	128.54	0.35	15
	(3+4)-II-1	19048	6405114	>100	406	7710	20.88	130.75	0.37	16
	(3+4)-II-2	16011	6269985	>100	705	6481	10.11	124.14	0.31	13
	(3+4)-II-3	19399	6054334	>100	856	7852	10.09	124.79	0.38	16
	(3+4)-II-4	16363	6650679	>100	348	6623	20.91	130.03	0.32	14
	(3+4)-III-1	17700	6522227	>100	471	7164	16.72	128.75	0.34	15
	(3+4)-III-2	16539	6266601	>100	814	6694	9.05	122.57	0.32	14
	(3+4)-III-3	18871	6032812	>100	931	7638	9.03	123.27	0.37	16
	(3+4)-III-4	17711	6464819	>100	472	7169	16.72	128.91	0.34	15
	(3+4)-IV-1	19464	6302716	>100	514	7878	16.87	129.49	0.38	16
	(3+4)-IV-2	15595	6151299	>100	764	6312	9.08	122.98	0.30	13
	(3+4)-IV-3	19815	5957587	>100	975	8020	9.05	123.56	0.38	17
	(3+4)-IV-4	15947	6529256	>100	419	6455	16.93	128.82	0.31	13
	(3+4)-V-1	17520	6587661	>100	445	7091	17.51	128.93	0.34	15
	(3+4)-V-2	16608	6300423	>100	748	6722	9.89	123.74	0.32	14
	(3+4)-V-3	18802	6067580	>100	846	7610	9.89	124.48	0.36	16
	(3+4)-V-4	17891	6434316	>100	454	7241	17.54	129.39	0.35	15
	(3+4)-VI-1	19031	6403906	>100	422	7703	20.10	130.50	0.37	16
	(3+4)-VI-2	15995	6269158	>100	691	6474	10.30	124.39	0.31	13
	(3+4)-VI-3	19416	6055983	>100	841	7859	10.28	125.05	0.38	16
	(3+4)-VI-4	16379	6651208	>100	362	6630	20.14	129.78	0.32	14
	(3+4)-VII-1	17644	6595140	>100	422	7142	18.61	129.37	0.34	15
	(3+4)-VII-2	16484	6265687	>100	767	6672	9.57	123.39	0.32	14
	(3+4)-VII-3	18927	6037810	>100	881	7661	9.57	124.11	0.37	16
	(3+4)-VII-4	17766	6466940	>100	424	7191	18.65	129.77	0.34	15
	(3+4)-VIII-1	19447	6301252	>100	529	7871	16.36	129.24	0.38	16
	(3+4)-VIII-2	15579	6150054	>100	751	6306	9.23	123.23	0.30	13
	(3+4)-VIII-3	19832	5959468	>100	959	8027	9.20	123.81	0.38	17
	(3+4)-VIII-4	15964	6530202	>100	433	6461	16.42	128.57	0.31	13
	(5+6)-I-1	17575	6514596	>100	494	7114	15.83	128.30	0.34	15
	(5+6)-I-2	16664	6300957	>100	795	6745	9.33	122.93	0.32	14
	(5+6)-I-3	18747	6062833	>100	896	7588	9.31	123.64	0.36	16

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-I-4	17836	6431896	>100	502	7219	15.82	128.54	0.35	15
	(5+6)-II-1	19048	6405114	>100	406	7710	20.88	130.75	0.37	16
	(5+6)-II-2	16011	6269985	>100	705	6481	10.11	124.14	0.31	13
	(5+6)-II-3	19399	6054334	>100	856	7852	10.09	124.79	0.38	16
	(5+6)-II-4	16363	6650679	>100	348	6623	20.91	130.03	0.32	14
	(5+6)-III-1	17700	6522227	>100	471	7164	16.72	128.75	0.34	15
	(5+6)-III-2	16539	6266601	>100	814	6694	9.05	122.57	0.32	14
	(5+6)-III-3	18871	6032812	>100	931	7638	9.03	123.27	0.37	16
	(5+6)-III-4	17711	6464819	>100	472	7169	16.72	128.91	0.34	15
	(5+6)-IV-1	19464	6302716	>100	514	7878	16.87	129.49	0.38	16
	(5+6)-IV-2	15595	6151299	>100	764	6312	9.08	122.98	0.30	13
	(5+6)-IV-3	19815	5957587	>100	975	8020	9.05	123.56	0.38	17
	(5+6)-IV-4	15947	6529256	>100	419	6455	16.93	128.82	0.31	13
	(5+6)-V-1	17520	6587661	>100	445	7091	17.51	128.93	0.34	15
	(5+6)-V-2	16608	6300423	>100	748	6722	9.89	123.74	0.32	14
	(5+6)-V-3	18802	6067580	>100	846	7610	9.89	124.48	0.36	16
	(5+6)-V-4	17891	6434316	>100	454	7241	17.54	129.39	0.35	15
	(5+6)-VI-1	19031	6403906	>100	422	7703	20.10	130.50	0.37	16
	(5+6)-VI-2	15995	6269158	>100	691	6474	10.30	124.39	0.31	13
	(5+6)-VI-3	19416	6055983	>100	841	7859	10.28	125.05	0.38	16
	(5+6)-VI-4	16379	6651208	>100	362	6630	20.14	129.78	0.32	14
	(5+6)-VII-1	17644	6595140	>100	422	7142	18.61	129.37	0.34	15
	(5+6)-VII-2	16484	6265687	>100	767	6672	9.57	123.39	0.32	14
	(5+6)-VII-3	18927	6037810	>100	881	7661	9.57	124.11	0.37	16
	(5+6)-VII-4	17766	6466940	>100	424	7191	18.65	129.77	0.34	15
	(5+6)-VIII-1	19447	6301252	>100	529	7871	16.36	129.24	0.38	16
	(5+6)-VIII-2	15579	6150054	>100	751	6306	9.23	123.23	0.30	13
	(5+6)-VIII-3	19832	5959468	>100	959	8027	9.20	123.81	0.38	17
	(5+6)-VIII-4	15964	6530202	>100	433	6461	16.42	128.57	0.31	13
9014	2	60559	17885186	>100	0	24511	>100	127.31	0.42	18
	(3+4)-I-1	42742	16181034	>100	1756	17300	10.84	114.56	0.30	13
	(3+4)-I-2	42125	15782923	>100	2142	17050	8.75	112.02	0.29	13
	(3+4)-I-3	42789	15777842	>100	2181	17319	8.74	111.99	0.30	13
	(3+4)-I-4	42172	16100348	>100	1734	17069	10.83	114.58	0.30	13
	(3+4)-II-1	43479	17683380	>100	110	17598	>100	124.95	0.30	13
	(3+4)-II-2	41421	16489652	>100	1247	16765	14.79	117.51	0.29	13
	(3+4)-II-3	43493	16608231	>100	1312	17604	14.76	117.44	0.30	13
	(3+4)-II-4	41435	17527562	>100	105	16771	>100	125.00	0.29	13
	(3+4)-III-1	42764	16268223	>100	1666	17309	11.43	115.12	0.30	13
	(3+4)-III-2	42102	15697480	>100	2231	17041	8.40	111.47	0.29	13
	(3+4)-III-3	42812	15706537	>100	2274	17328	8.38	111.43	0.30	13
	(3+4)-III-4	42150	16172175	>100	1643	17060	11.42	115.15	0.29	13
	(3+4)-IV-1	43554	17431209	>100	422	17628	45.91	122.97	0.30	13
	(3+4)-IV-2	41346	16197457	>100	1539	16735	11.96	115.63	0.29	12
	(3+4)-IV-3	43568	16363751	>100	1628	17634	11.92	115.52	0.30	13
	(3+4)-IV-4	41361	17223000	>100	400	16741	46.05	123.05	0.29	13
	(3+4)-V-1	42639	16238563	>100	1702	17258	11.16	114.86	0.30	13
	(3+4)-V-2	42022	15839059	>100	2088	17008	8.96	112.32	0.29	13
	(3+4)-V-3	42892	15812401	>100	2130	17361	8.97	112.34	0.30	13
	(3+4)-V-4	42275	16134509	>100	1684	17111	11.18	114.92	0.30	13
	(3+4)-VI-1	43448	17673181	>100	126	17586	>100	124.84	0.30	13
	(3+4)-VI-2	41390	16507300	>100	1231	16753	14.97	117.60	0.29	13
	(3+4)-VI-3	43524	16618587	>100	1297	17616	14.95	117.55	0.30	13
	(3+4)-VI-4	41466	17508767	>100	120	16784	>100	124.90	0.29	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-VII-1	42662	16326095	>100	1611	17267	11.79	115.43	0.30	13
	(3+4)-VII-2	41999	15753280	>100	2176	16999	8.59	111.77	0.29	13
	(3+4)-VII-3	42915	15741149	>100	2224	17370	8.59	111.77	0.30	13
	(3+4)-VII-4	42253	16206279	>100	1592	17102	11.81	115.49	0.30	13
	(3+4)-VIII-1	43523	17420944	>100	438	17616	44.20	122.86	0.30	13
	(3+4)-VIII-2	41315	16214758	>100	1523	16723	12.08	115.72	0.29	12
	(3+4)-VIII-3	43599	16374166	>100	1612	17647	12.04	115.63	0.31	13
	(3+4)-VIII-4	41391	17204567	>100	415	16753	44.37	122.95	0.29	13
	(5+6)-I-1	42742	16181034	>100	1756	17300	10.84	114.56	0.30	13
	(5+6)-I-2	42125	15782923	>100	2142	17050	8.75	112.02	0.29	13
	(5+6)-I-3	42789	15777842	>100	2181	17319	8.74	111.99	0.30	13
	(5+6)-I-4	42172	16100348	>100	1734	17069	10.83	114.58	0.30	13
	(5+6)-II-1	43479	17683380	>100	110	17598	>100	124.95	0.30	13
	(5+6)-II-2	41421	16489652	>100	1247	16765	14.79	117.51	0.29	13
	(5+6)-II-3	43493	16608231	>100	1312	17604	14.76	117.44	0.30	13
	(5+6)-II-4	41435	17527562	>100	105	16771	>100	125.00	0.29	13
	(5+6)-III-1	42764	16268223	>100	1666	17309	11.43	115.12	0.30	13
	(5+6)-III-2	42102	15697480	>100	2231	17041	8.40	111.47	0.29	13
	(5+6)-III-3	42812	15706537	>100	2274	17328	8.38	111.43	0.30	13
	(5+6)-III-4	42150	16172175	>100	1643	17060	11.42	115.15	0.29	13
	(5+6)-IV-1	43554	17431209	>100	422	17628	45.91	122.97	0.30	13
	(5+6)-IV-2	41346	16197457	>100	1539	16735	11.96	115.63	0.29	12
	(5+6)-IV-3	43568	16363751	>100	1628	17634	11.92	115.52	0.30	13
	(5+6)-IV-4	41361	17223000	>100	400	16741	46.05	123.05	0.29	13
	(5+6)-V-1	42639	16238563	>100	1702	17258	11.16	114.86	0.30	13
	(5+6)-V-2	42022	15839059	>100	2088	17008	8.96	112.32	0.29	13
	(5+6)-V-3	42892	15812401	>100	2130	17361	8.97	112.34	0.30	13
	(5+6)-V-4	42275	16134509	>100	1684	17111	11.18	114.92	0.30	13
	(5+6)-VI-1	43448	17673181	>100	126	17586	>100	124.84	0.30	13
	(5+6)-VI-2	41390	16507300	>100	1231	16753	14.97	117.60	0.29	13
	(5+6)-VI-3	43524	16618587	>100	1297	17616	14.95	117.55	0.30	13
	(5+6)-VI-4	41466	17508767	>100	120	16784	>100	124.90	0.29	13
	(5+6)-VII-1	42662	16326095	>100	1611	17267	11.79	115.43	0.30	13
	(5+6)-VII-2	41999	15753280	>100	2176	16999	8.59	111.77	0.29	13
	(5+6)-VII-3	42915	15741149	>100	2224	17370	8.59	111.77	0.30	13
	(5+6)-VII-4	42253	16206279	>100	1592	17102	11.81	115.49	0.30	13
	(5+6)-VIII-1	43523	17420944	>100	438	17616	44.20	122.86	0.30	13
	(5+6)-VIII-2	41315	16214758	>100	1523	16723	12.08	115.72	0.29	12
	(5+6)-VIII-3	43599	16374166	>100	1612	17647	12.04	115.63	0.31	13
	(5+6)-VIII-4	41391	17204567	>100	415	16753	44.37	122.95	0.29	13
9015	2	40138	11392902	>100	0	16246	>100	130.80	0.46	20
	(3+4)-I-1	28470	10463390	>100	958	11523	13.23	120.04	0.33	14
	(3+4)-I-2	28581	10948976	>100	325	11568	39.16	126.09	0.33	14
	(3+4)-I-3	27612	10974514	>100	315	11176	39.08	126.06	0.32	14
	(3+4)-I-4	27724	10479550	>100	934	11221	13.22	120.02	0.32	14
	(3+4)-II-1	28039	10207236	>100	1232	11349	10.13	117.34	0.32	14
	(3+4)-II-2	28412	10478268	>100	862	11500	14.67	120.98	0.33	14
	(3+4)-II-3	27782	10501496	>100	845	11245	14.63	120.94	0.32	14
	(3+4)-II-4	28155	10183301	>100	1235	11396	10.15	117.38	0.32	14
	(3+4)-III-1	28478	10501748	>100	911	11527	13.91	120.48	0.33	14
	(3+4)-III-2	28573	10909665	>100	372	11565	34.19	125.64	0.33	14
	(3+4)-III-3	27621	10934913	>100	361	11180	34.10	125.61	0.32	14
	(3+4)-III-4	27716	10518254	>100	887	11218	13.90	120.46	0.32	14
	(3+4)-IV-1	28068	10333329	>100	1079	11361	11.58	118.79	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-IV-2	28383	10606691	>100	704	11488	17.94	122.46	0.32	14
	(3+4)-IV-3	27811	10629867	>100	693	11256	17.87	122.41	0.32	14
	(3+4)-IV-4	28126	10310021	>100	1078	11384	11.62	118.85	0.32	14
	(3+4)-V-1	28526	10381598	>100	1059	11546	11.99	119.12	0.33	14
	(3+4)-V-2	28638	10865924	>100	424	11591	30.07	125.15	0.33	14
	(3+4)-V-3	27556	10891736	>100	408	11154	30.09	125.13	0.32	14
	(3+4)-V-4	27668	10402993	>100	1025	11199	12.01	119.12	0.32	14
	(3+4)-VI-1	28056	10183903	>100	1262	11356	9.90	117.07	0.32	14
	(3+4)-VI-2	28429	10501293	>100	834	11507	15.17	121.25	0.33	14
	(3+4)-VI-3	27765	10525071	>100	816	11238	15.15	121.21	0.32	14
	(3+4)-VI-4	28138	10160796	>100	1263	11389	9.92	117.12	0.32	14
	(3+4)-VII-1	28534	10419813	>100	1012	11549	12.55	119.56	0.33	14
	(3+4)-VII-2	28629	10826755	>100	471	11588	27.05	124.70	0.33	14
	(3+4)-VII-3	27565	10852346	>100	454	11157	27.05	124.68	0.32	14
	(3+4)-VII-4	27660	10441504	>100	979	11195	12.58	119.56	0.32	14
	(3+4)-VIII-1	28085	10309864	>100	1109	11367	11.28	118.51	0.32	14
	(3+4)-VIII-2	28400	10629908	>100	676	11495	18.71	122.74	0.33	14
	(3+4)-VIII-3	27794	10653572	>100	664	11250	18.65	122.69	0.32	14
	(3+4)-VIII-4	28109	10287326	>100	1106	11377	11.32	118.58	0.32	14
	(5+6)-I-1	28470	10463390	>100	958	11523	13.23	120.04	0.33	14
	(5+6)-I-2	28581	10948976	>100	325	11568	39.16	126.09	0.33	14
	(5+6)-I-3	27612	10974514	>100	315	11176	39.08	126.06	0.32	14
	(5+6)-I-4	27724	10479550	>100	934	11221	13.22	120.02	0.32	14
	(5+6)-II-1	28039	10207236	>100	1232	11349	10.13	117.34	0.32	14
	(5+6)-II-2	28412	10478268	>100	862	11500	14.67	120.98	0.33	14
	(5+6)-II-3	27782	10501496	>100	845	11245	14.63	120.94	0.32	14
	(5+6)-II-4	28155	10183301	>100	1235	11396	10.15	117.38	0.32	14
	(5+6)-III-1	28478	10501748	>100	911	11527	13.91	120.48	0.33	14
	(5+6)-III-2	28573	10909665	>100	372	11565	34.19	125.64	0.33	14
	(5+6)-III-3	27621	10934913	>100	361	11180	34.10	125.61	0.32	14
	(5+6)-III-4	27716	10518254	>100	887	11218	13.90	120.46	0.32	14
	(5+6)-IV-1	28068	10333329	>100	1079	11361	11.58	118.79	0.32	14
	(5+6)-IV-2	28383	10606691	>100	704	11488	17.94	122.46	0.32	14
	(5+6)-IV-3	27811	10629867	>100	693	11256	17.87	122.41	0.32	14
	(5+6)-IV-4	28126	10310021	>100	1078	11384	11.62	118.85	0.32	14
	(5+6)-V-1	28526	10381598	>100	1059	11546	11.99	119.12	0.33	14
	(5+6)-V-2	28638	10865924	>100	424	11591	30.07	125.15	0.33	14
	(5+6)-V-3	27556	10891736	>100	408	11154	30.09	125.13	0.32	14
	(5+6)-V-4	27668	10402993	>100	1025	11199	12.01	119.12	0.32	14
	(5+6)-VI-1	28056	10183903	>100	1262	11356	9.90	117.07	0.32	14
	(5+6)-VI-2	28429	10501293	>100	834	11507	15.17	121.25	0.33	14
	(5+6)-VI-3	27765	10525071	>100	816	11238	15.15	121.21	0.32	14
	(5+6)-VI-4	28138	10160796	>100	1263	11389	9.92	117.12	0.32	14
	(5+6)-VII-1	28534	10419813	>100	1012	11549	12.55	119.56	0.33	14
	(5+6)-VII-2	28629	10826755	>100	471	11588	27.05	124.70	0.33	14
	(5+6)-VII-3	27565	10852346	>100	454	11157	27.05	124.68	0.32	14
	(5+6)-VII-4	27660	10441504	>100	979	11195	12.58	119.56	0.32	14
	(5+6)-VIII-1	28085	10309864	>100	1109	11367	11.28	118.51	0.32	14
	(5+6)-VIII-2	28400	10629908	>100	676	11495	18.71	122.74	0.33	14
	(5+6)-VIII-3	27794	10653572	>100	664	11250	18.65	122.69	0.32	14
	(5+6)-VIII-4	28109	10287326	>100	1106	11377	11.32	118.58	0.32	14
9016	2	110183	28908868	>100	0	44597	>100	125.13	0.45	19
	(3+4)-I-1	76394	28789299	>100	29	30921	>100	123.36	0.31	13
	(3+4)-I-2	76945	26904702	>100	2094	31144	16.36	116.06	0.31	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cm ²]	qe [kg/cm ²]	w [mm]
	(3+4)-I-3	76615	27079744	>100	2089	31010	16.33	116.02	0.31	13
	(3+4)-I-4	77166	28604132	>100	29	31233	>100	123.38	0.31	13
	(3+4)-II-1	75829	26366334	>100	3188	30692	10.59	112.08	0.31	13
	(3+4)-II-2	77665	25321085	>100	3883	31435	8.90	110.08	0.31	14
	(3+4)-II-3	75896	25870466	>100	3804	30719	8.88	109.97	0.31	13
	(3+4)-II-4	77731	25803903	>100	3263	31462	10.61	112.17	0.31	14
	(3+4)-III-1	76291	28806230	>100	34	30879	>100	123.33	0.31	13
	(3+4)-III-2	77049	26880876	>100	2102	31186	16.32	116.04	0.31	13
	(3+4)-III-3	76512	27095098	>100	2092	30968	16.28	116.00	0.31	13
	(3+4)-III-4	77270	28578547	>100	35	31275	>100	123.36	0.31	13
	(3+4)-IV-1	75483	26416495	>100	3193	30552	10.52	112.00	0.30	13
	(3+4)-IV-2	78011	25248321	>100	3916	31575	8.87	110.03	0.32	14
	(3+4)-IV-3	75550	25919102	>100	3808	30579	8.83	109.89	0.31	13
	(3+4)-IV-4	78077	25729507	>100	3293	31602	10.56	112.13	0.32	14
	(3+4)-V-1	76195	28558743	>100	337	30840	>100	122.23	0.31	13
	(3+4)-V-2	76746	27182934	>100	1781	31063	19.19	117.13	0.31	13
	(3+4)-V-3	76815	27305797	>100	1782	31091	19.20	117.12	0.31	13
	(3+4)-V-4	77365	28314987	>100	342	31314	>100	122.26	0.31	13
	(3+4)-VI-1	75770	26299155	>100	3278	30668	10.29	111.76	0.31	13
	(3+4)-VI-2	77605	25400167	>100	3788	31411	9.12	110.39	0.31	14
	(3+4)-VI-3	75955	25937228	>100	3714	30743	9.11	110.29	0.31	13
	(3+4)-VI-4	77791	25723881	>100	3358	31486	10.31	111.86	0.31	14
	(3+4)-VII-1	76091	28575529	>100	342	30798	99.03	122.21	0.31	13
	(3+4)-VII-2	76850	27158743	>100	1788	31105	19.13	117.12	0.31	13
	(3+4)-VII-3	76711	27321294	>100	1785	31049	19.13	117.10	0.31	13
	(3+4)-VII-4	77469	28289783	>100	348	31356	99.24	122.25	0.31	14
	(3+4)-VIII-1	75424	26349172	>100	3284	30528	10.23	111.68	0.30	13
	(3+4)-VIII-2	77951	25327065	>100	3820	31551	9.08	110.34	0.31	14
	(3+4)-VIII-3	75610	25986006	>100	3717	30603	9.06	110.21	0.31	13
	(3+4)-VIII-4	78137	25649826	>100	3389	31626	10.27	111.81	0.32	14
	(5+6)-I-1	76394	28789299	>100	29	30921	>100	123.36	0.31	13
	(5+6)-I-2	76945	26904702	>100	2094	31144	16.36	116.06	0.31	13
	(5+6)-I-3	76615	27079744	>100	2089	31010	16.33	116.02	0.31	13
	(5+6)-I-4	77166	28604132	>100	29	31233	>100	123.38	0.31	13
	(5+6)-II-1	75829	26366334	>100	3188	30692	10.59	112.08	0.31	13
	(5+6)-II-2	77665	25321085	>100	3883	31435	8.90	110.08	0.31	14
	(5+6)-II-3	75896	25870466	>100	3804	30719	8.88	109.97	0.31	13
	(5+6)-II-4	77731	25803903	>100	3263	31462	10.61	112.17	0.31	14
	(5+6)-III-1	76291	28806230	>100	34	30879	>100	123.33	0.31	13
	(5+6)-III-2	77049	26880876	>100	2102	31186	16.32	116.04	0.31	13
	(5+6)-III-3	76512	27095098	>100	2092	30968	16.28	116.00	0.31	13
	(5+6)-III-4	77270	28578547	>100	35	31275	>100	123.36	0.31	13
	(5+6)-IV-1	75483	26416495	>100	3193	30552	10.52	112.00	0.30	13
	(5+6)-IV-2	78011	25248321	>100	3916	31575	8.87	110.03	0.32	14
	(5+6)-IV-3	75550	25919102	>100	3808	30579	8.83	109.89	0.31	13
	(5+6)-IV-4	78077	25729507	>100	3293	31602	10.56	112.13	0.32	14
	(5+6)-V-1	76195	28558743	>100	337	30840	>100	122.23	0.31	13
	(5+6)-V-2	76746	27182934	>100	1781	31063	19.19	117.13	0.31	13
	(5+6)-V-3	76815	27305797	>100	1782	31091	19.20	117.12	0.31	13
	(5+6)-V-4	77365	28314987	>100	342	31314	>100	122.26	0.31	13
	(5+6)-VI-1	75770	26299155	>100	3278	30668	10.29	111.76	0.31	13
	(5+6)-VI-2	77605	25400167	>100	3788	31411	9.12	110.39	0.31	14
	(5+6)-VI-3	75955	25937228	>100	3714	30743	9.11	110.29	0.31	13
	(5+6)-VI-4	77791	25723881	>100	3358	31486	10.31	111.86	0.31	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cm ²]	qe [kg/cm ²]	w [mm]
	(5+6)-VII-1	76091	28575529	>100	342	30798	99.03	122.21	0.31	13
	(5+6)-VII-2	76850	27158743	>100	1788	31105	19.13	117.12	0.31	13
	(5+6)-VII-3	76711	27321294	>100	1785	31049	19.13	117.10	0.31	13
	(5+6)-VII-4	77469	28289783	>100	348	31356	99.24	122.25	0.31	14
	(5+6)-VIII-1	75424	26349172	>100	3284	30528	10.23	111.68	0.30	13
	(5+6)-VIII-2	77951	25327065	>100	3820	31551	9.08	110.34	0.31	14
	(5+6)-VIII-3	75610	25986006	>100	3717	30603	9.06	110.21	0.31	13
	(5+6)-VIII-4	78137	25649826	>100	3389	31626	10.27	111.81	0.32	14
9017	2	34778	10147187	>100	0	14077	>100	132.05	0.44	19
	(3+4)-I-1	25240	9719910	>100	515	10216	21.82	124.70	0.32	14
	(3+4)-I-2	25224	9275021	>100	1095	10209	10.26	118.52	0.32	14
	(3+4)-I-3	23567	9028472	>100	1025	9539	10.23	118.80	0.30	13
	(3+4)-I-4	23551	9534722	>100	481	9532	21.80	124.92	0.30	13
	(3+4)-II-1	24673	9427999	>100	712	9987	15.44	122.57	0.31	14
	(3+4)-II-2	24619	9153159	>100	1180	9965	9.29	117.37	0.31	14
	(3+4)-II-3	24171	8973718	>100	1161	9783	9.27	117.56	0.31	13
	(3+4)-II-4	24117	9484067	>100	695	9762	15.46	122.51	0.31	13
	(3+4)-III-1	25298	9765469	>100	488	10240	23.09	124.98	0.32	14
	(3+4)-III-2	25165	9231450	>100	1120	10186	10.00	118.25	0.32	14
	(3+4)-III-3	23625	9028365	>100	1055	9562	9.97	118.47	0.30	13
	(3+4)-III-4	23492	9534059	>100	453	9509	23.08	125.25	0.30	13
	(3+4)-IV-1	24868	9423154	>100	811	10065	13.65	121.47	0.32	14
	(3+4)-IV-2	24425	9007757	>100	1261	9886	8.62	116.49	0.31	13
	(3+4)-IV-3	24366	8969652	>100	1263	9862	8.59	116.48	0.31	13
	(3+4)-IV-4	23923	9331720	>100	778	9683	13.69	121.61	0.30	13
	(3+4)-V-1	25290	9805256	>100	434	10236	25.95	125.56	0.32	14
	(3+4)-V-2	25274	9357070	>100	1016	10230	11.08	119.35	0.32	14
	(3+4)-V-3	23516	9077705	>100	945	9518	11.08	119.70	0.30	13
	(3+4)-V-4	23500	9584639	>100	403	9512	25.99	125.83	0.30	13
	(3+4)-VI-1	24688	9412569	>100	737	9993	14.92	122.29	0.31	14
	(3+4)-VI-2	24634	9177569	>100	1157	9971	9.48	117.62	0.31	14
	(3+4)-VI-3	24156	8988731	>100	1136	9777	9.46	117.83	0.31	13
	(3+4)-VI-4	24102	9458849	>100	718	9755	14.96	122.26	0.31	13
	(3+4)-VII-1	25349	9851086	>100	406	10260	27.77	125.84	0.32	14
	(3+4)-VII-2	25216	9313237	>100	1042	10206	10.78	119.08	0.32	14
	(3+4)-VII-3	23575	9077866	>100	974	9542	10.78	119.37	0.30	13
	(3+4)-VII-4	23442	9583694	>100	375	9488	27.82	126.17	0.30	13
	(3+4)-VIII-1	24883	9407475	>100	837	10072	13.24	121.19	0.32	14
	(3+4)-VIII-2	24440	9031906	>100	1238	9892	8.79	116.73	0.31	13
	(3+4)-VIII-3	24351	8984916	>100	1238	9856	8.76	116.75	0.31	13
	(3+4)-VIII-4	23907	9306769	>100	801	9677	13.29	121.36	0.30	13
	(5+6)-I-1	25240	9719910	>100	515	10216	21.82	124.70	0.32	14
	(5+6)-I-2	25224	9275021	>100	1095	10209	10.26	118.52	0.32	14
	(5+6)-I-3	23567	9028472	>100	1025	9539	10.23	118.80	0.30	13
	(5+6)-I-4	23551	9534722	>100	481	9532	21.80	124.92	0.30	13
	(5+6)-II-1	24673	9427999	>100	712	9987	15.44	122.57	0.31	14
	(5+6)-II-2	24619	9153159	>100	1180	9965	9.29	117.37	0.31	14
	(5+6)-II-3	24171	8973718	>100	1161	9783	9.27	117.56	0.31	13
	(5+6)-II-4	24117	9484067	>100	695	9762	15.46	122.51	0.31	13
	(5+6)-III-1	25298	9765469	>100	488	10240	23.09	124.98	0.32	14
	(5+6)-III-2	25165	9231450	>100	1120	10186	10.00	118.25	0.32	14
	(5+6)-III-3	23625	9028365	>100	1055	9562	9.97	118.47	0.30	13
	(5+6)-III-4	23492	9534059	>100	453	9509	23.08	125.25	0.30	13
	(5+6)-IV-1	24868	9423154	>100	811	10065	13.65	121.47	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-IV-2	24425	9007757	>100	1261	9886	8.62	116.49	0.31	13
	(5+6)-IV-3	24366	8969652	>100	1263	9862	8.59	116.48	0.31	13
	(5+6)-IV-4	23923	9331720	>100	778	9683	13.69	121.61	0.30	13
	(5+6)-V-1	25290	9805256	>100	434	10236	25.95	125.56	0.32	14
	(5+6)-V-2	25274	9357070	>100	1016	10230	11.08	119.35	0.32	14
	(5+6)-V-3	23516	9077705	>100	945	9518	11.08	119.70	0.30	13
	(5+6)-V-4	23500	9584639	>100	403	9512	25.99	125.83	0.30	13
	(5+6)-VI-1	24688	9412569	>100	737	9993	14.92	122.29	0.31	14
	(5+6)-VI-2	24634	9177569	>100	1157	9971	9.48	117.62	0.31	14
	(5+6)-VI-3	24156	8988731	>100	1136	9777	9.46	117.83	0.31	13
	(5+6)-VI-4	24102	9458849	>100	718	9755	14.96	122.26	0.31	13
	(5+6)-VII-1	25349	9851086	>100	406	10260	27.77	125.84	0.32	14
	(5+6)-VII-2	25216	9313237	>100	1042	10206	10.78	119.08	0.32	14
	(5+6)-VII-3	23575	9077866	>100	974	9542	10.78	119.37	0.30	13
	(5+6)-VII-4	23442	9583694	>100	375	9488	27.82	126.17	0.30	13
	(5+6)-VIII-1	24883	9407475	>100	837	10072	13.24	121.19	0.32	14
	(5+6)-VIII-2	24440	9031906	>100	1238	9892	8.79	116.73	0.31	13
	(5+6)-VIII-3	24351	8984916	>100	1238	9856	8.76	116.75	0.31	13
	(5+6)-VIII-4	23907	9306769	>100	801	9677	13.29	121.36	0.30	13
9018	2	27384	8317154	>100	0	11084	>100	134.66	0.44	19
	(3+4)-I-1	18664	7822679	>100	457	7554	18.19	126.33	0.30	13
	(3+4)-I-2	18549	8208722	>100	23	7508	>100	132.70	0.30	13
	(3+4)-I-3	19585	8201159	>100	25	7927	>100	132.71	0.31	14
	(3+4)-I-4	19470	7800818	>100	477	7881	18.17	126.36	0.31	14
	(3+4)-II-1	19120	7463272	>100	888	7739	9.59	120.47	0.31	13
	(3+4)-II-2	18737	7555423	>100	738	7584	11.31	122.38	0.30	13
	(3+4)-II-3	19397	7572793	>100	766	7851	11.28	122.32	0.31	13
	(3+4)-II-4	19013	7437660	>100	881	7696	9.60	120.54	0.31	13
	(3+4)-III-1	18649	7840792	>100	435	7548	19.10	126.65	0.30	13
	(3+4)-III-2	18563	8230437	>100	2	7513	>100	133.02	0.30	13
	(3+4)-III-3	19571	8219879	>100	2	7921	>100	133.04	0.31	14
	(3+4)-III-4	19484	7821912	>100	454	7886	19.09	126.68	0.31	14
	(3+4)-IV-1	19073	7522237	>100	811	7720	10.46	121.50	0.31	13
	(3+4)-IV-2	18785	7624743	>100	666	7603	12.56	123.42	0.30	13
	(3+4)-IV-3	19349	7632353	>100	689	7832	12.51	123.36	0.31	13
	(3+4)-IV-4	19061	7506367	>100	809	7715	10.50	121.57	0.31	13
	(3+4)-V-1	18622	7757789	>100	529	7537	15.68	125.27	0.30	13
	(3+4)-V-2	18507	8185804	>100	49	7491	>100	132.32	0.30	13
	(3+4)-V-3	19627	8177430	>100	51	7944	>100	132.34	0.32	14
	(3+4)-V-4	19512	7736440	>100	553	7898	15.71	125.33	0.31	14
	(3+4)-VI-1	19108	7444131	>100	910	7734	9.35	120.16	0.31	13
	(3+4)-VI-2	18724	7574358	>100	716	7579	11.65	122.68	0.30	13
	(3+4)-VI-3	19409	7592066	>100	743	7856	11.63	122.63	0.31	13
	(3+4)-VI-4	19026	7418980	>100	904	7701	9.37	120.24	0.31	13
	(3+4)-VII-1	18607	7775833	>100	507	7531	16.35	125.59	0.30	13
	(3+4)-VII-2	18521	8167217	>100	70	7496	>100	131.99	0.30	13
	(3+4)-VII-3	19613	8155857	>100	74	7938	>100	132.01	0.31	14
	(3+4)-VII-4	19526	7757415	>100	530	7903	16.39	125.64	0.31	14
	(3+4)-VIII-1	19060	7503026	>100	833	7715	10.18	121.19	0.31	13
	(3+4)-VIII-2	18772	7643797	>100	644	7598	12.98	123.72	0.30	13
	(3+4)-VIII-3	19362	7651697	>100	666	7837	12.94	123.67	0.31	13
	(3+4)-VIII-4	19074	7487569	>100	831	7720	10.22	121.27	0.31	13
	(5+6)-I-1	18664	7822679	>100	457	7554	18.19	126.33	0.30	13
	(5+6)-I-2	18549	8208722	>100	23	7508	>100	132.70	0.30	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cm ²]	qe [kg/cm ²]	w [mm]
	(5+6)-I-3	19585	8201159	>100	25	7927	>100	132.71	0.31	14
	(5+6)-I-4	19470	7800818	>100	477	7881	18.17	126.36	0.31	14
	(5+6)-II-1	19120	7463272	>100	888	7739	9.59	120.47	0.31	13
	(5+6)-II-2	18737	7555423	>100	738	7584	11.31	122.38	0.30	13
	(5+6)-II-3	19397	7572793	>100	766	7851	11.28	122.32	0.31	13
	(5+6)-II-4	19013	7437660	>100	881	7696	9.60	120.54	0.31	13
	(5+6)-III-1	18649	7840792	>100	435	7548	19.10	126.65	0.30	13
	(5+6)-III-2	18563	8230437	>100	2	7513	>100	133.02	0.30	13
	(5+6)-III-3	19571	8219879	>100	2	7921	>100	133.04	0.31	14
	(5+6)-III-4	19484	7821912	>100	454	7886	19.09	126.68	0.31	14
	(5+6)-IV-1	19073	7522237	>100	811	7720	10.46	121.50	0.31	13
	(5+6)-IV-2	18785	7624743	>100	666	7603	12.56	123.42	0.30	13
	(5+6)-IV-3	19349	7632353	>100	689	7832	12.51	123.36	0.31	13
	(5+6)-IV-4	19061	7506367	>100	809	7715	10.50	121.57	0.31	13
	(5+6)-V-1	18622	7757789	>100	529	7537	15.68	125.27	0.30	13
	(5+6)-V-2	18507	8185804	>100	49	7491	>100	132.32	0.30	13
	(5+6)-V-3	19627	8177430	>100	51	7944	>100	132.34	0.32	14
	(5+6)-V-4	19512	7736440	>100	553	7898	15.71	125.33	0.31	14
	(5+6)-VI-1	19108	7444131	>100	910	7734	9.35	120.16	0.31	13
	(5+6)-VI-2	18724	7574358	>100	716	7579	11.65	122.68	0.30	13
	(5+6)-VI-3	19409	7592066	>100	743	7856	11.63	122.63	0.31	13
	(5+6)-VI-4	19026	7418980	>100	904	7701	9.37	120.24	0.31	13
	(5+6)-VII-1	18607	7775833	>100	507	7531	16.35	125.59	0.30	13
	(5+6)-VII-2	18521	8167217	>100	70	7496	>100	131.99	0.30	13
	(5+6)-VII-3	19613	8155857	>100	74	7938	>100	132.01	0.31	14
	(5+6)-VII-4	19526	7757415	>100	530	7903	16.39	125.64	0.31	14
	(5+6)-VIII-1	19060	7503026	>100	833	7715	10.18	121.19	0.31	13
	(5+6)-VIII-2	18772	7643797	>100	644	7598	12.98	123.72	0.30	13
	(5+6)-VIII-3	19362	7651697	>100	666	7837	12.94	123.67	0.31	13
	(5+6)-VIII-4	19074	7487569	>100	831	7720	10.22	121.27	0.31	13
9019	2	20711	6496760	>100	0	8383	>100	139.04	0.44	19
	(3+4)-I-1	14822	6323596	>100	68	5999	96.46	136.32	0.32	14
	(3+4)-I-2	14209	6027305	>100	449	5751	14.08	128.77	0.30	13
	(3+4)-I-3	14882	5987554	>100	472	6024	14.05	128.89	0.32	14
	(3+4)-I-4	14269	6381262	>100	66	5775	96.37	136.13	0.30	13
	(3+4)-II-1	15559	5834815	>100	617	6297	11.23	126.95	0.33	14
	(3+4)-II-2	13515	5782244	>100	682	5470	8.83	123.79	0.29	12
	(3+4)-II-3	15577	5703871	>100	788	6305	8.80	124.04	0.33	14
	(3+4)-II-4	13533	5914331	>100	536	5478	11.24	126.68	0.29	12
	(3+4)-III-1	14790	6330417	>100	63	5986	>100	136.40	0.31	14
	(3+4)-III-2	14242	6020616	>100	455	5765	13.94	128.69	0.30	13
	(3+4)-III-3	14849	5985858	>100	476	6010	13.90	128.79	0.32	14
	(3+4)-III-4	14302	6382666	>100	61	5789	>100	136.23	0.30	13
	(3+4)-IV-1	15449	5828503	>100	630	6253	10.92	126.62	0.33	14
	(3+4)-IV-2	13625	5778705	>100	702	5515	8.65	123.48	0.29	13
	(3+4)-IV-3	15467	5697442	>100	800	6260	8.61	123.72	0.33	14
	(3+4)-IV-4	13643	5910784	>100	555	5522	10.95	126.36	0.29	13
	(3+4)-V-1	14827	6371175	>100	10	6001	>100	137.43	0.32	14
	(3+4)-V-2	14214	6073355	>100	394	5753	16.05	129.83	0.30	13
	(3+4)-V-3	14878	6040320	>100	412	6022	16.06	129.95	0.32	14
	(3+4)-V-4	14265	6435901	>100	10	5774	>100	137.21	0.30	13
	(3+4)-VI-1	15560	5819329	>100	636	6298	10.90	126.63	0.33	14
	(3+4)-VI-2	13516	5797453	>100	666	5471	9.03	124.09	0.29	12
	(3+4)-VI-3	15575	5719227	>100	769	6304	9.02	124.36	0.33	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-VI-4	13532	5898900	>100	552	5477	10.92	126.37	0.29	12
	(3+4)-VII-1	14794	6378045	>100	5	5988	>100	137.51	0.31	14
	(3+4)-VII-2	14247	6066618	>100	400	5766	15.87	129.75	0.30	13
	(3+4)-VII-3	14845	6038650	>100	416	6009	15.87	129.85	0.32	14
	(3+4)-VII-4	14298	6437275	>100	5	5787	>100	137.31	0.30	13
	(3+4)-VIII-1	15450	5812996	>100	649	6254	10.61	126.31	0.33	14
	(3+4)-VIII-2	13626	5793897	>100	686	5515	8.84	123.78	0.29	13
	(3+4)-VIII-3	15466	5712819	>100	781	6260	8.82	124.03	0.33	14
	(3+4)-VIII-4	13641	5895370	>100	570	5521	10.65	126.06	0.29	13
	(5+6)-I-1	14822	6323596	>100	68	5999	96.46	136.32	0.32	14
	(5+6)-I-2	14209	6027305	>100	449	5751	14.08	128.77	0.30	13
	(5+6)-I-3	14882	5987554	>100	472	6024	14.05	128.89	0.32	14
	(5+6)-I-4	14269	6381262	>100	66	5775	96.37	136.13	0.30	13
	(5+6)-II-1	15559	5834815	>100	617	6297	11.23	126.95	0.33	14
	(5+6)-II-2	13515	5782244	>100	682	5470	8.83	123.79	0.29	12
	(5+6)-II-3	15577	5703871	>100	788	6305	8.80	124.04	0.33	14
	(5+6)-II-4	13533	5914331	>100	536	5478	11.24	126.68	0.29	12
	(5+6)-III-1	14790	6330417	>100	63	5986	>100	136.40	0.31	14
	(5+6)-III-2	14242	6020616	>100	455	5765	13.94	128.69	0.30	13
	(5+6)-III-3	14849	5985858	>100	476	6010	13.90	128.79	0.32	14
	(5+6)-III-4	14302	6382666	>100	61	5789	>100	136.23	0.30	13
	(5+6)-IV-1	15449	5828503	>100	630	6253	10.92	126.62	0.33	14
	(5+6)-IV-2	13625	5778705	>100	702	5515	8.65	123.48	0.29	13
	(5+6)-IV-3	15467	5697442	>100	800	6260	8.61	123.72	0.33	14
	(5+6)-IV-4	13643	5910784	>100	555	5522	10.95	126.36	0.29	13
	(5+6)-V-1	14827	6371175	>100	10	6001	>100	137.43	0.32	14
	(5+6)-V-2	14214	6073355	>100	394	5753	16.05	129.83	0.30	13
	(5+6)-V-3	14878	6040320	>100	412	6022	16.06	129.95	0.32	14
	(5+6)-V-4	14265	6435901	>100	10	5774	>100	137.21	0.30	13
	(5+6)-VI-1	15560	5819329	>100	636	6298	10.90	126.63	0.33	14
	(5+6)-VI-2	13516	5797453	>100	666	5471	9.03	124.09	0.29	12
	(5+6)-VI-3	15575	5719227	>100	769	6304	9.02	124.36	0.33	14
	(5+6)-VI-4	13532	5898900	>100	552	5477	10.92	126.37	0.29	12
	(5+6)-VII-1	14794	6378045	>100	5	5988	>100	137.51	0.31	14
	(5+6)-VII-2	14247	6066618	>100	400	5766	15.87	129.75	0.30	13
	(5+6)-VII-3	14845	6038650	>100	416	6009	15.87	129.85	0.32	14
	(5+6)-VII-4	14298	6437275	>100	5	5787	>100	137.31	0.30	13
	(5+6)-VIII-1	15450	5812996	>100	649	6254	10.61	126.31	0.33	14
	(5+6)-VIII-2	13626	5793897	>100	686	5515	8.84	123.78	0.29	13
	(5+6)-VIII-3	15466	5712819	>100	781	6260	8.82	124.03	0.33	14
	(5+6)-VIII-4	13641	5895370	>100	570	5521	10.65	126.06	0.29	13
9020	2	44405	13071830	>100	0	17973	>100	129.54	0.44	19
	(3+4)-I-1	29631	12203935	>100	451	11993	29.28	123.94	0.29	13
	(3+4)-I-2	28961	12235085	>100	354	11722	36.39	124.79	0.29	12
	(3+4)-I-3	33348	12349775	>100	409	13498	36.31	124.70	0.33	14
	(3+4)-I-4	32679	12299521	>100	497	13227	29.25	123.87	0.32	14
	(3+4)-II-1	31713	11655055	>100	1467	12836	9.63	115.46	0.31	13
	(3+4)-II-2	29481	11553869	>100	1335	11933	9.83	115.81	0.29	13
	(3+4)-II-3	32828	11628520	>100	1490	13287	9.81	115.72	0.32	14
	(3+4)-II-4	30597	11717195	>100	1413	12384	9.64	115.43	0.30	13
	(3+4)-III-1	29685	12191768	>100	431	12015	30.66	124.15	0.29	13
	(3+4)-III-2	28906	12285282	>100	334	11700	38.57	124.96	0.28	12
	(3+4)-III-3	33403	12396949	>100	387	13520	38.48	124.87	0.33	14
	(3+4)-III-4	32624	12289428	>100	474	13205	30.65	124.08	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-IV-1	31895	11625095	>100	1403	12910	10.12	116.12	0.31	14
	(3+4)-IV-2	29299	11712580	>100	1258	11859	10.37	116.35	0.29	12
	(3+4)-IV-3	33011	11776841	>100	1423	13361	10.33	116.25	0.33	14
	(3+4)-IV-4	30414	11684354	>100	1334	12310	10.15	116.11	0.30	13
	(3+4)-V-1	29520	12058604	>100	570	11948	23.05	122.85	0.29	13
	(3+4)-V-2	28850	12307150	>100	235	11677	54.54	125.93	0.28	12
	(3+4)-V-3	33459	12431221	>100	273	13543	54.57	125.84	0.33	14
	(3+4)-V-4	32790	12160092	>100	632	13272	23.08	122.79	0.32	14
	(3+4)-VI-1	31680	11613220	>100	1505	12822	9.37	115.14	0.31	13
	(3+4)-VI-2	29448	11575570	>100	1298	11919	10.10	116.13	0.29	13
	(3+4)-VI-3	32861	11652759	>100	1450	13301	10.09	116.05	0.32	14
	(3+4)-VI-4	30630	11675962	>100	1452	12398	9.40	115.12	0.30	13
	(3+4)-VII-1	29574	12046530	>100	551	11970	23.90	123.06	0.29	13
	(3+4)-VII-2	28796	12357736	>100	215	11655	59.61	126.10	0.28	12
	(3+4)-VII-3	33514	12478671	>100	250	13565	59.61	126.01	0.33	14
	(3+4)-VII-4	32735	12150173	>100	609	13250	23.95	123.00	0.32	14
	(3+4)-VIII-1	31862	11583341	>100	1441	12896	9.85	115.80	0.31	14
	(3+4)-VIII-2	29266	11734657	>100	1221	11845	10.67	116.67	0.29	12
	(3+4)-VIII-3	33044	11801354	>100	1383	13375	10.64	116.59	0.33	14
	(3+4)-VIII-4	30448	11643294	>100	1372	12324	9.88	115.80	0.30	13
	(5+6)-I-1	29631	12203935	>100	451	11993	29.28	123.94	0.29	13
	(5+6)-I-2	28961	12235085	>100	354	11722	36.39	124.79	0.29	12
	(5+6)-I-3	33348	12349775	>100	409	13498	36.31	124.70	0.33	14
	(5+6)-I-4	32679	12299521	>100	497	13227	29.25	123.87	0.32	14
	(5+6)-II-1	31713	11655055	>100	1467	12836	9.63	115.46	0.31	13
	(5+6)-II-2	29481	11553869	>100	1335	11933	9.83	115.81	0.29	13
	(5+6)-II-3	32828	11628520	>100	1490	13287	9.81	115.72	0.32	14
	(5+6)-II-4	30597	11717195	>100	1413	12384	9.64	115.43	0.30	13
	(5+6)-III-1	29685	12191768	>100	431	12015	30.66	124.15	0.29	13
	(5+6)-III-2	28906	12285282	>100	334	11700	38.57	124.96	0.28	12
	(5+6)-III-3	33403	12396949	>100	387	13520	38.48	124.87	0.33	14
	(5+6)-III-4	32624	12289428	>100	474	13205	30.65	124.08	0.32	14
	(5+6)-IV-1	31895	11625095	>100	1403	12910	10.12	116.12	0.31	14
	(5+6)-IV-2	29299	11712580	>100	1258	11859	10.37	116.35	0.29	12
	(5+6)-IV-3	33011	11776841	>100	1423	13361	10.33	116.25	0.33	14
	(5+6)-IV-4	30414	11684354	>100	1334	12310	10.15	116.11	0.30	13
	(5+6)-V-1	29520	12058604	>100	570	11948	23.05	122.85	0.29	13
	(5+6)-V-2	28850	12307150	>100	235	11677	54.54	125.93	0.28	12
	(5+6)-V-3	33459	12431221	>100	273	13543	54.57	125.84	0.33	14
	(5+6)-V-4	32790	12160092	>100	632	13272	23.08	122.79	0.32	14
	(5+6)-VI-1	31680	11613220	>100	1505	12822	9.37	115.14	0.31	13
	(5+6)-VI-2	29448	11575570	>100	1298	11919	10.10	116.13	0.29	13
	(5+6)-VI-3	32861	11652759	>100	1450	13301	10.09	116.05	0.32	14
	(5+6)-VI-4	30630	11675962	>100	1452	12398	9.40	115.12	0.30	13
	(5+6)-VII-1	29574	12046530	>100	551	11970	23.90	123.06	0.29	13
	(5+6)-VII-2	28796	12357736	>100	215	11655	59.61	126.10	0.28	12
	(5+6)-VII-3	33514	12478671	>100	250	13565	59.61	126.01	0.33	14
	(5+6)-VII-4	32735	12150173	>100	609	13250	23.95	123.00	0.32	14
	(5+6)-VIII-1	31862	11583341	>100	1441	12896	9.85	115.80	0.31	14
	(5+6)-VIII-2	29266	11734657	>100	1221	11845	10.67	116.67	0.29	12
	(5+6)-VIII-3	33044	11801354	>100	1383	13375	10.64	116.59	0.33	14
	(5+6)-VIII-4	30448	11643294	>100	1372	12324	9.88	115.80	0.30	13
9021	2	33439	9692958	>100	0	13535	>100	132.59	0.45	19
	(3+4)-I-1	26241	8742929	>100	916	10621	12.76	121.70	0.35	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-I-2	24840	8556141	>100	1249	10054	8.86	117.50	0.33	14
	(3+4)-I-3	22511	8622048	>100	1134	9111	8.84	117.37	0.30	13
	(3+4)-I-4	21110	9015790	>100	737	8544	12.74	121.31	0.28	12
	(3+4)-II-1	26570	9101143	>100	343	10754	34.53	127.73	0.36	15
	(3+4)-II-2	21900	8935117	>100	841	8864	11.59	120.40	0.29	13
	(3+4)-II-3	25451	8654019	>100	980	10301	11.56	120.77	0.34	15
	(3+4)-II-4	20781	9365254	>100	268	8411	34.58	127.38	0.28	12
	(3+4)-III-1	26386	8766385	>100	872	10680	13.47	122.20	0.35	15
	(3+4)-III-2	24695	8533925	>100	1287	9995	8.55	117.00	0.33	14
	(3+4)-III-3	22655	8572326	>100	1183	9170	8.52	116.91	0.30	13
	(3+4)-III-4	20965	9035527	>100	694	8486	13.46	121.83	0.28	12
	(3+4)-IV-1	27052	8943148	>100	516	10949	23.35	126.10	0.36	16
	(3+4)-IV-2	21418	8761326	>100	954	8669	10.00	118.87	0.29	12
	(3+4)-IV-3	25933	8498623	>100	1159	10496	9.96	119.19	0.35	15
	(3+4)-IV-4	20299	9179882	>100	386	8216	23.42	125.79	0.27	12
	(3+4)-V-1	26405	8768860	>100	868	10687	13.55	122.26	0.35	15
	(3+4)-V-2	25004	8580516	>100	1206	10120	9.23	118.04	0.34	14
	(3+4)-V-3	22347	8679543	>100	1078	9045	9.23	117.91	0.30	13
	(3+4)-V-4	20946	9038847	>100	687	8478	13.57	121.90	0.28	12
	(3+4)-VI-1	26619	9084881	>100	360	10774	32.92	127.56	0.36	15
	(3+4)-VI-2	21949	8952534	>100	830	8884	11.78	120.56	0.29	13
	(3+4)-VI-3	25402	8670203	>100	962	10281	11.76	120.94	0.34	15
	(3+4)-VI-4	20731	9346531	>100	280	8391	33.00	127.22	0.28	12
	(3+4)-VII-1	26550	8792489	>100	824	10746	14.35	122.77	0.36	15
	(3+4)-VII-2	24859	8558116	>100	1245	10062	8.89	117.55	0.33	14
	(3+4)-VII-3	22491	8629424	>100	1126	9103	8.89	117.44	0.30	13
	(3+4)-VII-4	20801	9058187	>100	644	8419	14.38	122.42	0.28	12
	(3+4)-VIII-1	27101	8927177	>100	534	10969	22.60	125.94	0.36	16
	(3+4)-VIII-2	21467	8778681	>100	943	8689	10.14	119.02	0.29	12
	(3+4)-VIII-3	25884	8514501	>100	1140	10477	10.11	119.36	0.35	15
	(3+4)-VIII-4	20249	9161191	>100	397	8196	22.69	125.63	0.27	12
	(5+6)-I-1	26241	8742929	>100	916	10621	12.76	121.70	0.35	15
	(5+6)-I-2	24840	8556141	>100	1249	10054	8.86	117.50	0.33	14
	(5+6)-I-3	22511	8622048	>100	1134	9111	8.84	117.37	0.30	13
	(5+6)-I-4	21110	9015790	>100	737	8544	12.74	121.31	0.28	12
	(5+6)-II-1	26570	9101143	>100	343	10754	34.53	127.73	0.36	15
	(5+6)-II-2	21900	8935117	>100	841	8864	11.59	120.40	0.29	13
	(5+6)-II-3	25451	8654019	>100	980	10301	11.56	120.77	0.34	15
	(5+6)-II-4	20781	9365254	>100	268	8411	34.58	127.38	0.28	12
	(5+6)-III-1	26386	8766385	>100	872	10680	13.47	122.20	0.35	15
	(5+6)-III-2	24695	8533925	>100	1287	9995	8.55	117.00	0.33	14
	(5+6)-III-3	22655	8572326	>100	1183	9170	8.52	116.91	0.30	13
	(5+6)-III-4	20965	9035527	>100	694	8486	13.46	121.83	0.28	12
	(5+6)-IV-1	27052	8943148	>100	516	10949	23.35	126.10	0.36	16
	(5+6)-IV-2	21418	8761326	>100	954	8669	10.00	118.87	0.29	12
	(5+6)-IV-3	25933	8498623	>100	1159	10496	9.96	119.19	0.35	15
	(5+6)-IV-4	20299	9179882	>100	386	8216	23.42	125.79	0.27	12
	(5+6)-V-1	26405	8768860	>100	868	10687	13.55	122.26	0.35	15
	(5+6)-V-2	25004	8580516	>100	1206	10120	9.23	118.04	0.34	14
	(5+6)-V-3	22347	8679543	>100	1078	9045	9.23	117.91	0.30	13
	(5+6)-V-4	20946	9038847	>100	687	8478	13.57	121.90	0.28	12
	(5+6)-VI-1	26619	9084881	>100	360	10774	32.92	127.56	0.36	15
	(5+6)-VI-2	21949	8952534	>100	830	8884	11.78	120.56	0.29	13
	(5+6)-VI-3	25402	8670203	>100	962	10281	11.76	120.94	0.34	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-VI-4	20731	9346531	>100	280	8391	33.00	127.22	0.28	12
	(5+6)-VII-1	26550	8792489	>100	824	10746	14.35	122.77	0.36	15
	(5+6)-VII-2	24859	8558116	>100	1245	10062	8.89	117.55	0.33	14
	(5+6)-VII-3	22491	8629424	>100	1126	9103	8.89	117.44	0.30	13
	(5+6)-VII-4	20801	9058187	>100	644	8419	14.38	122.42	0.28	12
	(5+6)-VIII-1	27101	8927177	>100	534	10969	22.60	125.94	0.36	16
	(5+6)-VIII-2	21467	8778681	>100	943	8689	10.14	119.02	0.29	12
	(5+6)-VIII-3	25884	8514501	>100	1140	10477	10.11	119.36	0.35	15
	(5+6)-VIII-4	20249	9161191	>100	397	8196	22.69	125.63	0.27	12
9022	2	60412	15852446	>100	0	24452	>100	128.08	0.49	21
	(3+4)-I-1	41481	15439796	>100	41	16790	>100	126.26	0.33	14
	(3+4)-I-2	41631	14747090	>100	1109	16850	16.71	119.19	0.33	14
	(3+4)-I-3	41865	14590224	>100	1118	16945	16.67	119.25	0.34	15
	(3+4)-I-4	42015	15607547	>100	42	17006	>100	126.19	0.34	15
	(3+4)-II-1	41441	13714399	>100	1753	16773	10.53	115.30	0.33	14
	(3+4)-II-2	41940	13633117	>100	2093	16975	8.92	113.23	0.34	15
	(3+4)-II-3	41556	13477223	>100	2079	16820	8.90	113.27	0.33	14
	(3+4)-II-4	42055	13874251	>100	1776	17022	10.54	115.23	0.34	15
	(3+4)-III-1	41525	15522046	>100	43	16808	>100	126.21	0.33	14
	(3+4)-III-2	41587	14824230	>100	1110	16832	16.69	119.14	0.33	14
	(3+4)-III-3	41909	14666713	>100	1121	16963	16.64	119.20	0.34	15
	(3+4)-III-4	41970	15688544	>100	43	16988	>100	126.14	0.34	15
	(3+4)-IV-1	41588	13962895	>100	1766	16833	10.49	115.12	0.33	14
	(3+4)-IV-2	41792	13874316	>100	2090	16916	8.90	113.08	0.34	15
	(3+4)-IV-3	41703	13720197	>100	2093	16880	8.87	113.10	0.34	14
	(3+4)-IV-4	41907	14119129	>100	1774	16962	10.52	115.08	0.34	15
	(3+4)-V-1	41406	15452128	>100	209	16759	88.21	125.07	0.33	14
	(3+4)-V-2	41555	14737202	>100	940	16820	19.67	120.34	0.33	14
	(3+4)-V-3	41941	14582955	>100	949	16976	19.68	120.41	0.34	15
	(3+4)-V-4	42090	15500320	>100	212	17036	88.36	125.05	0.34	15
	(3+4)-VI-1	41418	13716628	>100	1803	16764	10.23	114.95	0.33	14
	(3+4)-VI-2	41917	13630260	>100	2042	16966	9.14	113.56	0.34	15
	(3+4)-VI-3	41579	13475421	>100	2029	16829	9.12	113.62	0.33	14
	(3+4)-VI-4	42077	13877065	>100	1827	17031	10.25	114.90	0.34	15
	(3+4)-VII-1	41450	15533549	>100	211	16777	87.50	125.03	0.33	14
	(3+4)-VII-2	41511	14815055	>100	941	16802	19.64	120.29	0.33	14
	(3+4)-VII-3	41985	14660245	>100	952	16993	19.64	120.36	0.34	15
	(3+4)-VII-4	42046	15417414	>100	213	17018	87.69	125.08	0.34	15
	(3+4)-VIII-1	41566	13964328	>100	1816	16824	10.19	114.78	0.33	14
	(3+4)-VIII-2	41770	13872132	>100	2039	16906	9.12	113.41	0.34	14
	(3+4)-VIII-3	41726	13719182	>100	2043	16889	9.09	113.44	0.34	14
	(3+4)-VIII-4	41930	14121262	>100	1825	16971	10.23	114.75	0.34	15
	(5+6)-I-1	41481	15439796	>100	41	16790	>100	126.26	0.33	14
	(5+6)-I-2	41631	14747090	>100	1109	16850	16.71	119.19	0.33	14
	(5+6)-I-3	41865	14590224	>100	1118	16945	16.67	119.25	0.34	15
	(5+6)-I-4	42015	15607547	>100	42	17006	>100	126.19	0.34	15
	(5+6)-II-1	41441	13714399	>100	1753	16773	10.53	115.30	0.33	14
	(5+6)-II-2	41940	13633117	>100	2093	16975	8.92	113.23	0.34	15
	(5+6)-II-3	41556	13477223	>100	2079	16820	8.90	113.27	0.33	14
	(5+6)-II-4	42055	13874251	>100	1776	17022	10.54	115.23	0.34	15
	(5+6)-III-1	41525	15522046	>100	43	16808	>100	126.21	0.33	14
	(5+6)-III-2	41587	14824230	>100	1110	16832	16.69	119.14	0.33	14
	(5+6)-III-3	41909	14666713	>100	1121	16963	16.64	119.20	0.34	15
	(5+6)-III-4	41970	15688544	>100	43	16988	>100	126.14	0.34	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-IV-1	41588	13962895	>100	1766	16833	10.49	115.12	0.33	14
	(5+6)-IV-2	41792	13874316	>100	2090	16916	8.90	113.08	0.34	15
	(5+6)-IV-3	41703	13720197	>100	2093	16880	8.87	113.10	0.34	14
	(5+6)-IV-4	41907	14119129	>100	1774	16962	10.52	115.08	0.34	15
	(5+6)-V-1	41406	15452128	>100	209	16759	88.21	125.07	0.33	14
	(5+6)-V-2	41555	14737202	>100	940	16820	19.67	120.34	0.33	14
	(5+6)-V-3	41941	14582955	>100	949	16976	19.68	120.41	0.34	15
	(5+6)-V-4	42090	15500320	>100	212	17036	88.36	125.05	0.34	15
	(5+6)-VI-1	41418	13716628	>100	1803	16764	10.23	114.95	0.33	14
	(5+6)-VI-2	41917	13630260	>100	2042	16966	9.14	113.56	0.34	15
	(5+6)-VI-3	41579	13475421	>100	2029	16829	9.12	113.62	0.33	14
	(5+6)-VI-4	42077	13877065	>100	1827	17031	10.25	114.90	0.34	15
	(5+6)-VII-1	41450	15533549	>100	211	16777	87.50	125.03	0.33	14
	(5+6)-VII-2	41511	14815055	>100	941	16802	19.64	120.29	0.33	14
	(5+6)-VII-3	41985	14660245	>100	952	16993	19.64	120.36	0.34	15
	(5+6)-VII-4	42046	15417414	>100	213	17018	87.69	125.08	0.34	15
	(5+6)-VIII-1	41566	13964328	>100	1816	16824	10.19	114.78	0.33	14
	(5+6)-VIII-2	41770	13872132	>100	2039	16906	9.12	113.41	0.34	14
	(5+6)-VIII-3	41726	13719182	>100	2043	16889	9.09	113.44	0.34	14
	(5+6)-VIII-4	41930	14121262	>100	1825	16971	10.23	114.75	0.34	15
9023	2	35598	10880320	>100	0	14408	>100	131.28	0.43	18
	(3+4)-I-1	25935	9648760	>100	1221	10497	9.46	117.03	0.31	13
	(3+4)-I-2	25386	9738344	>100	1081	10275	10.45	118.21	0.31	13
	(3+4)-I-3	24668	9722279	>100	1053	9985	10.43	118.20	0.30	13
	(3+4)-I-4	24120	9630298	>100	1136	9763	9.45	117.04	0.29	13
	(3+4)-II-1	26132	10292933	>100	546	10577	21.30	123.92	0.31	14
	(3+4)-II-2	24303	10607941	>100	147	9837	73.80	128.00	0.29	13
	(3+4)-II-3	25752	10597354	>100	156	10423	73.62	128.01	0.31	13
	(3+4)-II-4	23923	10279959	>100	499	9683	21.34	123.95	0.29	12
	(3+4)-III-1	25960	9691631	>100	1160	10507	9.96	117.67	0.31	13
	(3+4)-III-2	25361	9695607	>100	1141	10265	9.90	117.57	0.30	13
	(3+4)-III-3	24694	9679528	>100	1114	9995	9.87	117.56	0.30	13
	(3+4)-III-4	24095	9672659	>100	1077	9752	9.96	117.68	0.29	13
	(3+4)-IV-1	26216	10442118	>100	338	10611	34.57	126.14	0.32	14
	(3+4)-IV-2	24219	10458543	>100	340	9803	31.72	125.78	0.29	13
	(3+4)-IV-3	25836	10447251	>100	364	10457	31.60	125.77	0.31	13
	(3+4)-IV-4	23839	10425708	>100	306	9649	34.67	126.16	0.29	12
	(3+4)-V-1	25934	9615403	>100	1245	10497	9.27	116.80	0.31	13
	(3+4)-V-2	25385	9704595	>100	1105	10275	10.23	117.98	0.31	13
	(3+4)-V-3	24669	9690574	>100	1073	9985	10.23	118.00	0.30	13
	(3+4)-V-4	24120	9598655	>100	1156	9763	9.29	116.84	0.29	13
	(3+4)-VI-1	26131	10282670	>100	553	10577	21.03	123.85	0.31	14
	(3+4)-VI-2	24302	10597249	>100	153	9836	70.70	127.94	0.29	13
	(3+4)-VI-3	25752	10587028	>100	162	10423	70.58	127.94	0.31	13
	(3+4)-VI-4	23923	10269697	>100	505	9683	21.08	123.88	0.29	12
	(3+4)-VII-1	25959	9658230	>100	1184	10507	9.76	117.44	0.31	13
	(3+4)-VII-2	25360	9661901	>100	1165	10265	9.69	117.34	0.30	13
	(3+4)-VII-3	24694	9648018	>100	1134	9995	9.69	117.36	0.30	13
	(3+4)-VII-4	24095	9640820	>100	1097	9753	9.78	117.48	0.29	13
	(3+4)-VIII-1	26215	10431814	>100	345	10611	33.86	126.07	0.32	14
	(3+4)-VIII-2	24218	10449807	>100	346	9803	31.13	125.71	0.29	13
	(3+4)-VIII-3	25836	10437126	>100	371	10457	31.03	125.71	0.31	13
	(3+4)-VIII-4	23839	10415242	>100	312	9649	33.99	126.10	0.29	12
	(5+6)-I-1	25935	9648760	>100	1221	10497	9.46	117.03	0.31	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-I-2	25386	9738344	>100	1081	10275	10.45	118.21	0.31	13
	(5+6)-I-3	24668	9722279	>100	1053	9985	10.43	118.20	0.30	13
	(5+6)-I-4	24120	9630298	>100	1136	9763	9.45	117.04	0.29	13
	(5+6)-II-1	26132	10292933	>100	546	10577	21.30	123.92	0.31	14
	(5+6)-II-2	24303	10607941	>100	147	9837	73.80	128.00	0.29	13
	(5+6)-II-3	25752	10597354	>100	156	10423	73.62	128.01	0.31	13
	(5+6)-II-4	23923	10279959	>100	499	9683	21.34	123.95	0.29	12
	(5+6)-III-1	25960	9691631	>100	1160	10507	9.96	117.67	0.31	13
	(5+6)-III-2	25361	9695607	>100	1141	10265	9.90	117.57	0.30	13
	(5+6)-III-3	24694	9679528	>100	1114	9995	9.87	117.56	0.30	13
	(5+6)-III-4	24095	9672659	>100	1077	9752	9.96	117.68	0.29	13
	(5+6)-IV-1	26216	10442118	>100	338	10611	34.57	126.14	0.32	14
	(5+6)-IV-2	24219	10458543	>100	340	9803	31.72	125.78	0.29	13
	(5+6)-IV-3	25836	10447251	>100	364	10457	31.60	125.77	0.31	13
	(5+6)-IV-4	23839	10425708	>100	306	9649	34.67	126.16	0.29	12
	(5+6)-V-1	25934	9615403	>100	1245	10497	9.27	116.80	0.31	13
	(5+6)-V-2	25385	9704595	>100	1105	10275	10.23	117.98	0.31	13
	(5+6)-V-3	24669	9690574	>100	1073	9985	10.23	118.00	0.30	13
	(5+6)-V-4	24120	9598655	>100	1156	9763	9.29	116.84	0.29	13
	(5+6)-VI-1	26131	10282670	>100	553	10577	21.03	123.85	0.31	14
	(5+6)-VI-2	24302	10597249	>100	153	9836	70.70	127.94	0.29	13
	(5+6)-VI-3	25752	10587028	>100	162	10423	70.58	127.94	0.31	13
	(5+6)-VI-4	23923	10269697	>100	505	9683	21.08	123.88	0.29	12
	(5+6)-VII-1	25959	9658230	>100	1184	10507	9.76	117.44	0.31	13
	(5+6)-VII-2	25360	9661901	>100	1165	10265	9.69	117.34	0.30	13
	(5+6)-VII-3	24694	9648018	>100	1134	9995	9.69	117.36	0.30	13
	(5+6)-VII-4	24095	9640820	>100	1097	9753	9.78	117.48	0.29	13
	(5+6)-VIII-1	26215	10431814	>100	345	10611	33.86	126.07	0.32	14
	(5+6)-VIII-2	24218	10449807	>100	346	9803	31.13	125.71	0.29	13
	(5+6)-VIII-3	25836	10437126	>100	371	10457	31.03	125.71	0.31	13
	(5+6)-VIII-4	23839	10415242	>100	312	9649	33.99	126.10	0.29	12
9024	2	81436	20878095	>100	0	32961	>100	126.48	0.49	21
	(3+4)-I-1	56535	20454983	>100	18	22883	>100	124.80	0.34	15
	(3+4)-I-2	57312	19295655	>100	1596	23197	15.98	117.28	0.35	15
	(3+4)-I-3	55022	19253455	>100	1536	22270	15.95	117.27	0.33	14
	(3+4)-I-4	55799	20414689	>100	18	22585	>100	124.81	0.34	15
	(3+4)-II-1	55098	18630453	>100	2299	22301	10.67	113.61	0.33	14
	(3+4)-II-2	57689	18319518	>100	2890	23350	8.89	111.42	0.35	15
	(3+4)-II-3	54645	18344013	>100	2744	22118	8.87	111.37	0.33	14
	(3+4)-II-4	57235	18604620	>100	2385	23166	10.69	113.64	0.35	15
	(3+4)-III-1	56634	20464989	>100	12	22923	>100	124.83	0.34	15
	(3+4)-III-2	57212	19286568	>100	1599	23157	15.93	117.25	0.35	15
	(3+4)-III-3	55122	19244023	>100	1545	22311	15.89	117.24	0.33	14
	(3+4)-III-4	55700	20424134	>100	12	22545	>100	124.84	0.34	15
	(3+4)-IV-1	55431	18629566	>100	2335	22436	10.57	113.51	0.34	14
	(3+4)-IV-2	57356	18319523	>100	2892	23215	8.83	111.33	0.35	15
	(3+4)-IV-3	54977	18342318	>100	2783	22252	8.80	111.27	0.33	14
	(3+4)-IV-4	56903	18604203	>100	2389	23032	10.60	113.55	0.34	15
	(3+4)-V-1	56843	20363072	>100	211	23008	>100	123.85	0.34	15
	(3+4)-V-2	57621	19529338	>100	1375	23322	18.66	118.33	0.35	15
	(3+4)-V-3	54713	19491779	>100	1305	22145	18.67	118.34	0.33	14
	(3+4)-V-4	55491	20322896	>100	205	22460	>100	123.86	0.34	15
	(3+4)-VI-1	55191	18595005	>100	2371	22339	10.36	113.29	0.33	14
	(3+4)-VI-2	57782	18354329	>100	2826	23387	9.10	111.73	0.35	15

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-VI-3	54552	18379475	>100	2673	22080	9.09	111.70	0.33	14
	(3+4)-VI-4	57143	18569689	>100	2449	23129	10.39	113.32	0.35	15
	(3+4)-VII-1	56943	20363122	>100	217	23048	>100	123.82	0.34	15
	(3+4)-VII-2	57521	19520250	>100	1378	23282	18.58	118.31	0.35	15
	(3+4)-VII-3	54813	19482172	>100	1313	22186	18.58	118.32	0.33	14
	(3+4)-VII-4	55391	20322755	>100	211	22420	>100	123.83	0.34	14
	(3+4)-VIII-1	55524	18593908	>100	2407	22473	10.27	113.18	0.34	15
	(3+4)-VIII-2	57449	18354208	>100	2828	23253	9.04	111.64	0.35	15
	(3+4)-VIII-3	54885	18377987	>100	2711	22215	9.02	111.59	0.33	14
	(3+4)-VIII-4	56810	18569402	>100	2453	22994	10.31	113.23	0.34	15
	(5+6)-I-1	56535	20454983	>100	18	22883	>100	124.80	0.34	15
	(5+6)-I-2	57312	19295655	>100	1596	23197	15.98	117.28	0.35	15
	(5+6)-I-3	55022	19253455	>100	1536	22270	15.95	117.27	0.33	14
	(5+6)-I-4	55799	20414689	>100	18	22585	>100	124.81	0.34	15
	(5+6)-II-1	55098	18630453	>100	2299	22301	10.67	113.61	0.33	14
	(5+6)-II-2	57689	18319518	>100	2890	23350	8.89	111.42	0.35	15
	(5+6)-II-3	54645	18344013	>100	2744	22118	8.87	111.37	0.33	14
	(5+6)-II-4	57235	18604620	>100	2385	23166	10.69	113.64	0.35	15
	(5+6)-III-1	56634	20464989	>100	12	22923	>100	124.83	0.34	15
	(5+6)-III-2	57212	19286568	>100	1599	23157	15.93	117.25	0.35	15
	(5+6)-III-3	55122	19244023	>100	1545	22311	15.89	117.24	0.33	14
	(5+6)-III-4	55700	20424134	>100	12	22545	>100	124.84	0.34	15
	(5+6)-IV-1	55431	18629566	>100	2335	22436	10.57	113.51	0.34	14
	(5+6)-IV-2	57356	18319523	>100	2892	23215	8.83	111.33	0.35	15
	(5+6)-IV-3	54977	18342318	>100	2783	22252	8.80	111.27	0.33	14
	(5+6)-IV-4	56903	18604203	>100	2389	23032	10.60	113.55	0.34	15
	(5+6)-V-1	56843	20363072	>100	211	23008	>100	123.85	0.34	15
	(5+6)-V-2	57621	19529338	>100	1375	23322	18.66	118.33	0.35	15
	(5+6)-V-3	54713	19491779	>100	1305	22145	18.67	118.34	0.33	14
	(5+6)-V-4	55491	20322896	>100	205	22460	>100	123.86	0.34	15
	(5+6)-VI-1	55191	18595005	>100	2371	22339	10.36	113.29	0.33	14
	(5+6)-VI-2	57782	18354329	>100	2826	23387	9.10	111.73	0.35	15
	(5+6)-VI-3	54552	18379475	>100	2673	22080	9.09	111.70	0.33	14
	(5+6)-VI-4	57143	18569689	>100	2449	23129	10.39	113.32	0.35	15
	(5+6)-VII-1	56943	20363122	>100	217	23048	>100	123.82	0.34	15
	(5+6)-VII-2	57521	19520250	>100	1378	23282	18.58	118.31	0.35	15
	(5+6)-VII-3	54813	19482172	>100	1313	22186	18.58	118.32	0.33	14
	(5+6)-VII-4	55391	20322755	>100	211	22420	>100	123.83	0.34	14
	(5+6)-VIII-1	55524	18593908	>100	2407	22473	10.27	113.18	0.34	15
	(5+6)-VIII-2	57449	18354208	>100	2828	23253	9.04	111.64	0.35	15
	(5+6)-VIII-3	54885	18377987	>100	2711	22215	9.02	111.59	0.33	14
	(5+6)-VIII-4	56810	18569402	>100	2453	22994	10.31	113.23	0.34	15
9025	2	62618	15812564	>100	0	25345	>100	128.09	0.50	22
	(3+4)-I-1	48535	15450969	>100	16	19645	>100	126.45	0.39	17
	(3+4)-I-2	47917	14508241	>100	1335	19394	15.98	118.96	0.39	17
	(3+4)-I-3	39627	14656039	>100	1106	16039	15.95	118.87	0.32	14
	(3+4)-I-4	39009	15159585	>100	13	15789	>100	126.58	0.31	14
	(3+4)-II-1	46139	13497094	>100	1925	18675	10.67	115.57	0.37	16
	(3+4)-II-2	44077	13072372	>100	2208	17841	8.89	113.47	0.35	15
	(3+4)-II-3	43466	13234587	>100	2183	17593	8.87	113.35	0.35	15
	(3+4)-II-4	41405	13211307	>100	1725	16759	10.69	115.74	0.33	14
	(3+4)-III-1	48239	15594280	>100	11	19525	>100	126.42	0.39	17
	(3+4)-III-2	48213	14639165	>100	1348	19514	15.93	118.87	0.39	17
	(3+4)-III-3	39331	14748999	>100	1102	15919	15.89	118.80	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-III-4	39305	15340834	>100	9	15909	>100	126.53	0.32	14
	(3+4)-IV-1	45152	13922929	>100	1902	18275	10.57	115.24	0.36	16
	(3+4)-IV-2	45065	13532023	>100	2272	18240	8.83	113.14	0.36	16
	(3+4)-IV-3	42479	13678370	>100	2150	17194	8.80	113.01	0.34	15
	(3+4)-IV-4	42392	13713266	>100	1780	17158	10.60	115.38	0.34	15
	(3+4)-V-1	48040	15461187	>100	178	19444	>100	125.46	0.39	17
	(3+4)-V-2	47422	14513001	>100	1132	19194	18.66	120.09	0.38	16
	(3+4)-V-3	40122	14646712	>100	957	16240	18.67	120.03	0.32	14
	(3+4)-V-4	39504	15209524	>100	146	15989	>100	125.57	0.32	14
	(3+4)-VI-1	45990	13493159	>100	1976	18615	10.36	115.23	0.37	16
	(3+4)-VI-2	43929	13067127	>100	2149	17780	9.10	113.81	0.35	15
	(3+4)-VI-3	43615	13236931	>100	2137	17653	9.09	113.69	0.35	15
	(3+4)-VI-4	41554	13219828	>100	1781	16819	10.39	115.41	0.33	14
	(3+4)-VII-1	47744	15598242	>100	182	19325	>100	125.37	0.38	17
	(3+4)-VII-2	47718	14647366	>100	1144	19314	18.58	120.00	0.38	17
	(3+4)-VII-3	39826	14802928	>100	954	16120	18.58	119.93	0.32	14
	(3+4)-VII-4	39800	15378796	>100	151	16109	>100	125.47	0.32	14
	(3+4)-VIII-1	45003	13919838	>100	1951	18215	10.27	114.90	0.36	16
	(3+4)-VIII-2	44916	13530568	>100	2211	18180	9.04	113.47	0.36	16
	(3+4)-VIII-3	42628	13679716	>100	2105	17254	9.02	113.35	0.34	15
	(3+4)-VIII-4	42541	13717530	>100	1837	17218	10.31	115.05	0.34	15
	(5+6)-I-1	48535	15450969	>100	16	19645	>100	126.45	0.39	17
	(5+6)-I-2	47917	14508241	>100	1335	19394	15.98	118.96	0.39	17
	(5+6)-I-3	39627	14656039	>100	1106	16039	15.95	118.87	0.32	14
	(5+6)-I-4	39009	15159585	>100	13	15789	>100	126.58	0.31	14
	(5+6)-II-1	46139	13497094	>100	1925	18675	10.67	115.57	0.37	16
	(5+6)-II-2	44077	13072372	>100	2208	17841	8.89	113.47	0.35	15
	(5+6)-II-3	43466	13234587	>100	2183	17593	8.87	113.35	0.35	15
	(5+6)-II-4	41405	13211307	>100	1725	16759	10.69	115.74	0.33	14
	(5+6)-III-1	48239	15594280	>100	11	19525	>100	126.42	0.39	17
	(5+6)-III-2	48213	14639165	>100	1348	19514	15.93	118.87	0.39	17
	(5+6)-III-3	39331	14748999	>100	1102	15919	15.89	118.80	0.32	14
	(5+6)-III-4	39305	15340834	>100	9	15909	>100	126.53	0.32	14
	(5+6)-IV-1	45152	13922929	>100	1902	18275	10.57	115.24	0.36	16
	(5+6)-IV-2	45065	13532023	>100	2272	18240	8.83	113.14	0.36	16
	(5+6)-IV-3	42479	13678370	>100	2150	17194	8.80	113.01	0.34	15
	(5+6)-IV-4	42392	13713266	>100	1780	17158	10.60	115.38	0.34	15
	(5+6)-V-1	48040	15461187	>100	178	19444	>100	125.46	0.39	17
	(5+6)-V-2	47422	14513001	>100	1132	19194	18.66	120.09	0.38	16
	(5+6)-V-3	40122	14646712	>100	957	16240	18.67	120.03	0.32	14
	(5+6)-V-4	39504	15209524	>100	146	15989	>100	125.57	0.32	14
	(5+6)-VI-1	45990	13493159	>100	1976	18615	10.36	115.23	0.37	16
	(5+6)-VI-2	43929	13067127	>100	2149	17780	9.10	113.81	0.35	15
	(5+6)-VI-3	43615	13236931	>100	2137	17653	9.09	113.69	0.35	15
	(5+6)-VI-4	41554	13219828	>100	1781	16819	10.39	115.41	0.33	14
	(5+6)-VII-1	47744	15598242	>100	182	19325	>100	125.37	0.38	17
	(5+6)-VII-2	47718	14647366	>100	1144	19314	18.58	120.00	0.38	17
	(5+6)-VII-3	39826	14802928	>100	954	16120	18.58	119.93	0.32	14
	(5+6)-VII-4	39800	15378796	>100	151	16109	>100	125.47	0.32	14
	(5+6)-VIII-1	45003	13919838	>100	1951	18215	10.27	114.90	0.36	16
	(5+6)-VIII-2	44916	13530568	>100	2211	18180	9.04	113.47	0.36	16
	(5+6)-VIII-3	42628	13679716	>100	2105	17254	9.02	113.35	0.34	15
	(5+6)-VIII-4	42541	13717530	>100	1837	17218	10.31	115.05	0.34	15
9026	2	86753	23585516	>100	0	35113	>100	125.91	0.46	20

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(3+4)-I-1	60492	21304647	>100	2711	24484	9.93	112.15	0.32	14
	(3+4)-I-2	60772	21935689	>100	1967	24598	13.75	115.43	0.32	14
	(3+4)-I-3	59993	21440618	>100	1946	24282	13.72	115.51	0.32	14
	(3+4)-I-4	60273	20842349	>100	2704	24396	9.92	112.23	0.32	14
	(3+4)-II-1	59991	21751650	>100	1940	24282	13.77	115.47	0.32	14
	(3+4)-II-2	60923	22962302	>100	556	24659	48.79	121.74	0.32	14
	(3+4)-II-3	59842	22777468	>100	547	24221	48.67	121.77	0.31	14
	(3+4)-II-4	60774	21638213	>100	1962	24598	13.79	115.51	0.32	14
	(3+4)-III-1	60531	21436050	>100	2577	24500	10.46	112.73	0.32	14
	(3+4)-III-2	60733	21802344	>100	2103	24582	12.86	114.83	0.32	14
	(3+4)-III-3	60032	21348642	>100	2084	24298	12.82	114.90	0.32	14
	(3+4)-III-4	60234	20933292	>100	2565	24380	10.45	112.83	0.32	14
	(3+4)-IV-1	60121	22199028	>100	1491	24334	17.95	117.47	0.32	14
	(3+4)-IV-2	60794	23283774	>100	96	24607	>100	123.83	0.32	14
	(3+4)-IV-3	59971	23239533	>100	95	24273	>100	123.84	0.32	14
	(3+4)-IV-4	60644	21949283	>100	1499	24546	18.01	117.54	0.32	14
	(3+4)-V-1	60488	21223467	>100	2838	24483	9.49	111.59	0.32	14
	(3+4)-V-2	60768	21839360	>100	2093	24596	12.92	114.87	0.32	14
	(3+4)-V-3	59997	21315323	>100	2066	24284	12.93	114.98	0.32	14
	(3+4)-V-4	60277	20720427	>100	2823	24397	9.51	111.72	0.32	14
	(3+4)-VI-1	59990	21728649	>100	1977	24281	13.51	115.31	0.32	14
	(3+4)-VI-2	60922	23002220	>100	519	24658	52.26	121.90	0.32	14
	(3+4)-VI-3	59843	22800287	>100	511	24222	52.17	121.94	0.31	14
	(3+4)-VI-4	60775	21600415	>100	1998	24599	13.54	115.35	0.32	14
	(3+4)-VII-1	60527	21316362	>100	2703	24498	9.97	112.19	0.32	14
	(3+4)-VII-2	60729	21724691	>100	2229	24580	12.13	114.28	0.32	14
	(3+4)-VII-3	60036	21223844	>100	2204	24300	12.13	114.38	0.32	14
	(3+4)-VII-4	60238	20810879	>100	2684	24382	9.99	112.32	0.32	14
	(3+4)-VIII-1	60119	22175862	>100	1528	24334	17.51	117.31	0.32	14
	(3+4)-VIII-2	60793	23324209	>100	59	24606	>100	124.00	0.32	14
	(3+4)-VIII-3	59972	23262508	>100	59	24274	>100	124.01	0.32	14
	(3+4)-VIII-4	60646	21910984	>100	1536	24547	17.58	117.38	0.32	14
	(5+6)-I-1	60492	21304647	>100	2711	24484	9.93	112.15	0.32	14
	(5+6)-I-2	60772	21935689	>100	1967	24598	13.75	115.43	0.32	14
	(5+6)-I-3	59993	21440618	>100	1946	24282	13.72	115.51	0.32	14
	(5+6)-I-4	60273	20842349	>100	2704	24396	9.92	112.23	0.32	14
	(5+6)-II-1	59991	21751650	>100	1940	24282	13.77	115.47	0.32	14
	(5+6)-II-2	60923	22962302	>100	556	24659	48.79	121.74	0.32	14
	(5+6)-II-3	59842	22777468	>100	547	24221	48.67	121.77	0.31	14
	(5+6)-II-4	60774	21638213	>100	1962	24598	13.79	115.51	0.32	14
	(5+6)-III-1	60531	21436050	>100	2577	24500	10.46	112.73	0.32	14
	(5+6)-III-2	60733	21802344	>100	2103	24582	12.86	114.83	0.32	14
	(5+6)-III-3	60032	21348642	>100	2084	24298	12.82	114.90	0.32	14
	(5+6)-III-4	60234	20933292	>100	2565	24380	10.45	112.83	0.32	14
	(5+6)-IV-1	60121	22199028	>100	1491	24334	17.95	117.47	0.32	14
	(5+6)-IV-2	60794	23283774	>100	96	24607	>100	123.83	0.32	14
	(5+6)-IV-3	59971	23239533	>100	95	24273	>100	123.84	0.32	14
	(5+6)-IV-4	60644	21949283	>100	1499	24546	18.01	117.54	0.32	14
	(5+6)-V-1	60488	21223467	>100	2838	24483	9.49	111.59	0.32	14
	(5+6)-V-2	60768	21839360	>100	2093	24596	12.92	114.87	0.32	14
	(5+6)-V-3	59997	21315323	>100	2066	24284	12.93	114.98	0.32	14
	(5+6)-V-4	60277	20720427	>100	2823	24397	9.51	111.72	0.32	14
	(5+6)-VI-1	59990	21728649	>100	1977	24281	13.51	115.31	0.32	14
	(5+6)-VI-2	60922	23002220	>100	519	24658	52.26	121.90	0.32	14

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-VI-3	59843	22800287	>100	511	24222	52.17	121.94	0.31	14
	(5+6)-VI-4	60775	21600415	>100	1998	24599	13.54	115.35	0.32	14
	(5+6)-VII-1	60527	21316362	>100	2703	24498	9.97	112.19	0.32	14
	(5+6)-VII-2	60729	21724691	>100	2229	24580	12.13	114.28	0.32	14
	(5+6)-VII-3	60036	21223844	>100	2204	24300	12.13	114.38	0.32	14
	(5+6)-VII-4	60238	20810879	>100	2684	24382	9.99	112.32	0.32	14
	(5+6)-VIII-1	60119	22175862	>100	1528	24334	17.51	117.31	0.32	14
	(5+6)-VIII-2	60793	23324209	>100	59	24606	>100	124.00	0.32	14
	(5+6)-VIII-3	59972	23262508	>100	59	24274	>100	124.01	0.32	14
	(5+6)-VIII-4	60646	21910984	>100	1536	24547	17.58	117.38	0.32	14
9027	2	38682	11500657	>100	0	15657	>100	130.71	0.44	19
	(3+4)-I-1	27391	10585082	>100	846	11086	14.41	120.72	0.31	13
	(3+4)-I-2	27570	10147048	>100	1349	11159	9.10	115.99	0.31	14
	(3+4)-I-3	26429	10121816	>100	1296	10697	9.08	115.98	0.30	13
	(3+4)-I-4	26608	10562242	>100	823	10770	14.40	120.74	0.30	13
	(3+4)-II-1	26845	10903054	>100	487	10866	24.54	124.14	0.30	13
	(3+4)-II-2	27442	10324043	>100	1154	11107	10.59	117.77	0.31	13
	(3+4)-II-3	26556	10299776	>100	1119	10749	10.57	117.76	0.30	13
	(3+4)-II-4	27154	10925134	>100	492	10991	24.58	124.13	0.31	13
	(3+4)-III-1	27416	10623994	>100	802	11097	15.22	121.16	0.31	13
	(3+4)-III-2	27544	10109312	>100	1392	11149	8.81	115.56	0.31	14
	(3+4)-III-3	26455	10083727	>100	1341	10708	8.79	115.55	0.30	13
	(3+4)-III-4	26583	10601303	>100	778	10759	15.22	121.18	0.30	13
	(3+4)-IV-1	26930	10770746	>100	637	10900	18.82	122.65	0.31	13
	(3+4)-IV-2	27357	10197213	>100	1299	11073	9.38	116.34	0.31	13
	(3+4)-IV-3	26641	10171694	>100	1270	10783	9.34	116.31	0.30	13
	(3+4)-IV-4	27069	10793446	>100	638	10956	18.88	122.65	0.31	13
	(3+4)-V-1	27442	10638045	>100	780	11107	15.66	121.38	0.31	13
	(3+4)-V-2	27621	10198260	>100	1284	11180	9.58	116.62	0.31	14
	(3+4)-V-3	26378	10175262	>100	1226	10677	9.58	116.65	0.30	13
	(3+4)-V-4	26557	10616483	>100	754	10749	15.69	121.42	0.30	13
	(3+4)-VI-1	26860	10886533	>100	508	10872	23.56	123.93	0.30	13
	(3+4)-VI-2	27458	10339580	>100	1134	11114	10.78	117.96	0.31	13
	(3+4)-VI-3	26541	10315945	>100	1098	10743	10.76	117.97	0.30	13
	(3+4)-VI-4	27139	10908917	>100	512	10984	23.61	123.92	0.31	13
	(3+4)-VII-1	27467	10677128	>100	736	11117	16.62	121.82	0.31	13
	(3+4)-VII-2	27595	10160358	>100	1328	11169	9.25	116.20	0.31	14
	(3+4)-VII-3	26403	10137131	>100	1271	10687	9.25	116.22	0.30	13
	(3+4)-VII-4	26532	10655584	>100	709	10739	16.65	121.86	0.30	13
	(3+4)-VIII-1	26945	10754266	>100	658	10906	18.24	122.44	0.31	13
	(3+4)-VIII-2	27373	10212582	>100	1280	11079	9.52	116.53	0.31	13
	(3+4)-VIII-3	26626	10187819	>100	1249	10777	9.49	116.52	0.30	13
	(3+4)-VIII-4	27054	10777403	>100	658	10950	18.30	122.45	0.31	13
	(5+6)-I-1	27391	10585082	>100	846	11086	14.41	120.72	0.31	13
	(5+6)-I-2	27570	10147048	>100	1349	11159	9.10	115.99	0.31	14
	(5+6)-I-3	26429	10121816	>100	1296	10697	9.08	115.98	0.30	13
	(5+6)-I-4	26608	10562242	>100	823	10770	14.40	120.74	0.30	13
	(5+6)-II-1	26845	10903054	>100	487	10866	24.54	124.14	0.30	13
	(5+6)-II-2	27442	10324043	>100	1154	11107	10.59	117.77	0.31	13
	(5+6)-II-3	26556	10299776	>100	1119	10749	10.57	117.76	0.30	13
	(5+6)-II-4	27154	10925134	>100	492	10991	24.58	124.13	0.31	13
	(5+6)-III-1	27416	10623994	>100	802	11097	15.22	121.16	0.31	13
	(5+6)-III-2	27544	10109312	>100	1392	11149	8.81	115.56	0.31	14
	(5+6)-III-3	26455	10083727	>100	1341	10708	8.79	115.55	0.30	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-III-4	26583	10601303	>100	778	10759	15.22	121.18	0.30	13
	(5+6)-IV-1	26930	10770746	>100	637	10900	18.82	122.65	0.31	13
	(5+6)-IV-2	27357	10197213	>100	1299	11073	9.38	116.34	0.31	13
	(5+6)-IV-3	26641	10171694	>100	1270	10783	9.34	116.31	0.30	13
	(5+6)-IV-4	27069	10793446	>100	638	10956	18.88	122.65	0.31	13
	(5+6)-V-1	27442	10638045	>100	780	11107	15.66	121.38	0.31	13
	(5+6)-V-2	27621	10198260	>100	1284	11180	9.58	116.62	0.31	14
	(5+6)-V-3	26378	10175262	>100	1226	10677	9.58	116.65	0.30	13
	(5+6)-V-4	26557	10616483	>100	754	10749	15.69	121.42	0.30	13
	(5+6)-VI-1	26860	10886533	>100	508	10872	23.56	123.93	0.30	13
	(5+6)-VI-2	27458	10339580	>100	1134	11114	10.78	117.96	0.31	13
	(5+6)-VI-3	26541	10315945	>100	1098	10743	10.76	117.97	0.30	13
	(5+6)-VI-4	27139	10908917	>100	512	10984	23.61	123.92	0.31	13
	(5+6)-VII-1	27467	10677128	>100	736	11117	16.62	121.82	0.31	13
	(5+6)-VII-2	27595	10160358	>100	1328	11169	9.25	116.20	0.31	14
	(5+6)-VII-3	26403	10137131	>100	1271	10687	9.25	116.22	0.30	13
	(5+6)-VII-4	26532	10655584	>100	709	10739	16.65	121.86	0.30	13
	(5+6)-VIII-1	26945	10754266	>100	658	10906	18.24	122.44	0.31	13
	(5+6)-VIII-2	27373	10212582	>100	1280	11079	9.52	116.53	0.31	13
	(5+6)-VIII-3	26626	10187819	>100	1249	10777	9.49	116.52	0.30	13
	(5+6)-VIII-4	27054	10777403	>100	658	10950	18.30	122.45	0.31	13
9028	2	41121	12963468	>100	0	16644	>100	129.61	0.41	18
	(3+4)-I-1	29357	12551729	>100	357	11882	36.59	124.59	0.29	13
	(3+4)-I-2	29776	11918485	>100	1123	12052	11.81	117.68	0.29	13
	(3+4)-I-3	28109	11685132	>100	1062	11377	11.79	117.83	0.28	12
	(3+4)-I-4	28529	12435119	>100	347	11547	36.56	124.66	0.28	12
	(3+4)-II-1	28431	11796250	>100	999	11508	12.67	118.49	0.28	12
	(3+4)-II-2	29829	11580585	>100	1492	12073	8.90	114.45	0.29	13
	(3+4)-II-3	28057	11351534	>100	1407	11356	8.88	114.59	0.28	12
	(3+4)-II-4	29454	11950274	>100	1034	11922	12.69	118.40	0.29	13
	(3+4)-III-1	29358	12568637	>100	336	11883	38.85	124.78	0.29	13
	(3+4)-III-2	29776	11897663	>100	1143	12052	11.59	117.50	0.29	13
	(3+4)-III-3	28110	11663786	>100	1082	11378	11.57	117.64	0.28	12
	(3+4)-III-4	28528	12457187	>100	327	11547	38.83	124.86	0.28	12
	(3+4)-IV-1	28434	11724815	>100	1068	11509	11.86	117.86	0.28	12
	(3+4)-IV-2	29826	11511828	>100	1562	12072	8.50	113.85	0.29	13
	(3+4)-IV-3	28060	11281519	>100	1475	11357	8.47	113.97	0.28	12
	(3+4)-IV-4	29452	11895797	>100	1102	11921	11.89	117.77	0.29	13
	(3+4)-V-1	29419	12660262	>100	250	11907	52.38	125.59	0.29	13
	(3+4)-V-2	29838	12009597	>100	1016	12077	13.07	118.65	0.29	13
	(3+4)-V-3	28048	11775501	>100	955	11353	13.08	118.82	0.28	12
	(3+4)-V-4	28467	12528183	>100	242	11522	52.46	125.68	0.28	12
	(3+4)-VI-1	28450	11768933	>100	1032	11515	12.28	118.19	0.28	12
	(3+4)-VI-2	29847	11607201	>100	1461	12081	9.10	114.74	0.29	13
	(3+4)-VI-3	28039	11378320	>100	1375	11349	9.08	114.88	0.28	12
	(3+4)-VI-4	29436	11919085	>100	1065	11914	12.30	118.11	0.29	13
	(3+4)-VII-1	29419	12677305	>100	229	11908	57.14	125.78	0.29	13
	(3+4)-VII-2	29837	11988327	>100	1037	12077	12.81	118.46	0.29	13
	(3+4)-VII-3	28049	11754094	>100	975	11353	12.81	118.63	0.28	12
	(3+4)-VII-4	28466	12550311	>100	221	11522	57.26	125.87	0.28	12
	(3+4)-VIII-1	28452	11697560	>100	1100	11516	11.52	117.57	0.28	12
	(3+4)-VIII-2	29845	11538308	>100	1530	12080	8.68	114.14	0.29	13
	(3+4)-VIII-3	28041	11308244	>100	1442	11350	8.66	114.26	0.28	12
	(3+4)-VIII-4	29433	11864737	>100	1134	11913	11.56	117.49	0.29	13

Elm.	Cmb	V [kg]	Vd [kg]	CsV (>2.30)	H [kg]	Hd [kg]	CsH (>1.10)	Qd [kg/cmq]	qe [kg/cmq]	w [mm]
	(5+6)-I-1	29357	12551729	>100	357	11882	36.59	124.59	0.29	13
	(5+6)-I-2	29776	11918485	>100	1123	12052	11.81	117.68	0.29	13
	(5+6)-I-3	28109	11685132	>100	1062	11377	11.79	117.83	0.28	12
	(5+6)-I-4	28529	12435119	>100	347	11547	36.56	124.66	0.28	12
	(5+6)-II-1	28431	11796250	>100	999	11508	12.67	118.49	0.28	12
	(5+6)-II-2	29829	11580585	>100	1492	12073	8.90	114.45	0.29	13
	(5+6)-II-3	28057	11351534	>100	1407	11356	8.88	114.59	0.28	12
	(5+6)-II-4	29454	11950274	>100	1034	11922	12.69	118.40	0.29	13
	(5+6)-III-1	29358	12568637	>100	336	11883	38.85	124.78	0.29	13
	(5+6)-III-2	29776	11897663	>100	1143	12052	11.59	117.50	0.29	13
	(5+6)-III-3	28110	11663786	>100	1082	11378	11.57	117.64	0.28	12
	(5+6)-III-4	28528	12457187	>100	327	11547	38.83	124.86	0.28	12
	(5+6)-IV-1	28434	11724815	>100	1068	11509	11.86	117.86	0.28	12
	(5+6)-IV-2	29826	11511828	>100	1562	12072	8.50	113.85	0.29	13
	(5+6)-IV-3	28060	11281519	>100	1475	11357	8.47	113.97	0.28	12
	(5+6)-IV-4	29452	11895797	>100	1102	11921	11.89	117.77	0.29	13
	(5+6)-V-1	29419	12660262	>100	250	11907	52.38	125.59	0.29	13
	(5+6)-V-2	29838	12009597	>100	1016	12077	13.07	118.65	0.29	13
	(5+6)-V-3	28048	11775501	>100	955	11353	13.08	118.82	0.28	12
	(5+6)-V-4	28467	12528183	>100	242	11522	52.46	125.68	0.28	12
	(5+6)-VI-1	28450	11768933	>100	1032	11515	12.28	118.19	0.28	12
	(5+6)-VI-2	29847	11607201	>100	1461	12081	9.10	114.74	0.29	13
	(5+6)-VI-3	28039	11378320	>100	1375	11349	9.08	114.88	0.28	12
	(5+6)-VI-4	29436	11919085	>100	1065	11914	12.30	118.11	0.29	13
	(5+6)-VII-1	29419	12677305	>100	229	11908	57.14	125.78	0.29	13
	(5+6)-VII-2	29837	11988327	>100	1037	12077	12.81	118.46	0.29	13
	(5+6)-VII-3	28049	11754094	>100	975	11353	12.81	118.63	0.28	12
	(5+6)-VII-4	28466	12550311	>100	221	11522	57.26	125.87	0.28	12
	(5+6)-VIII-1	28452	11697560	>100	1100	11516	11.52	117.57	0.28	12
	(5+6)-VIII-2	29845	11538308	>100	1530	12080	8.68	114.14	0.29	13
	(5+6)-VIII-3	28041	11308244	>100	1442	11350	8.66	114.26	0.28	12
	(5+6)-VIII-4	29433	11864737	>100	1134	11913	11.56	117.49	0.29	13
	Minimi coeff. sic.									
9010	2			>100						
9014	(3+4)-III-3						8.38			

Wmax=22, Wmin=12

Verifica a scorrimento globale delle fondazione

Comb. = Combinazione di verifica

N[kg] = Sforzo normale

Hd[kg] = Azione orizzontale depurata dalle azioni assorbite da pali e plinti su pali

R[kg] = Resistenza allo scorrimento $R = \text{Area} \cdot c + N \cdot \tan(\phi)$

CS = R/Hd

CSd = Coefficiente di sicurezza di progetto

Area delle strutture di fondazione a contatto con il terreno **A=448.0314 m²**

Comb.	N	Hd	R	CS.	CSd	ver
	kg	kg	kg			
2	2115794	0	942012	--	1.10	Si
(3+4)-I-1	1472252	69311	655489	9.46	1.10	Si
(3+4)-I-2	1473143	75060	655885	8.74	1.10	Si

Comb.	N	Hd	R	CS.	CSd	ver
(3+4)-I-3	1470016	75060	654493	8.72	1.10	Si
(3+4)-I-4	1470906	69311	654890	9.45	1.10	Si
(3+4)-II-1	1470430	68562	654677	9.55	1.10	Si
(3+4)-II-2	1473399	74369	656000	8.82	1.10	Si
(3+4)-II-3	1469759	74369	654379	8.80	1.10	Si
(3+4)-II-4	1472728	68562	655701	9.56	1.10	Si
(3+4)-III-1	1471935	65768	655348	9.96	1.10	Si
(3+4)-III-2	1473459	78133	656026	8.40	1.10	Si
(3+4)-III-3	1469699	78133	654352	8.37	1.10	Si
(3+4)-III-4	1471223	65768	655031	9.96	1.10	Si
(3+4)-IV-1	1469374	64674	654208	10.12	1.10	Si
(3+4)-IV-2	1474455	77214	656469	8.50	1.10	Si
(3+4)-IV-3	1468704	77214	653909	8.47	1.10	Si
(3+4)-IV-4	1473784	64674	656171	10.15	1.10	Si
(3+4)-V-1	1470344	70795	654639	9.25	1.10	Si
(3+4)-V-2	1471235	73108	655036	8.96	1.10	Si
(3+4)-V-3	1471923	73108	655342	8.96	1.10	Si
(3+4)-V-4	1472814	70795	655739	9.26	1.10	Si
(3+4)-VI-1	1469857	70326	654423	9.31	1.10	Si
(3+4)-VI-2	1472827	72654	655745	9.03	1.10	Si
(3+4)-VI-3	1470331	72654	654634	9.01	1.10	Si
(3+4)-VI-4	1473301	70326	655956	9.33	1.10	Si
(3+4)-VII-1	1470028	67277	654498	9.73	1.10	Si
(3+4)-VII-2	1471552	76307	655177	8.59	1.10	Si
(3+4)-VII-3	1471606	76307	655201	8.59	1.10	Si
(3+4)-VII-4	1473131	67277	655880	9.75	1.10	Si
(3+4)-VIII-1	1468802	66486	653953	9.84	1.10	Si
(3+4)-VIII-2	1473882	75611	656215	8.68	1.10	Si
(3+4)-VIII-3	1469276	75611	654164	8.65	1.10	Si
(3+4)-VIII-4	1474356	66486	656426	9.87	1.10	Si
(5+6)-I-1	1472252	69311	655489	9.46	1.10	Si
(5+6)-I-2	1473143	75060	655885	8.74	1.10	Si
(5+6)-I-3	1470016	75060	654493	8.72	1.10	Si
(5+6)-I-4	1470906	69311	654890	9.45	1.10	Si
(5+6)-II-1	1470430	68562	654677	9.55	1.10	Si
(5+6)-II-2	1473399	74369	656000	8.82	1.10	Si
(5+6)-II-3	1469759	74369	654379	8.80	1.10	Si
(5+6)-II-4	1472728	68562	655701	9.56	1.10	Si
(5+6)-III-1	1471935	65768	655348	9.96	1.10	Si
(5+6)-III-2	1473459	78133	656026	8.40	1.10	Si
(5+6)-III-3	1469699	78133	654352	8.37	1.10	Si
(5+6)-III-4	1471223	65768	655031	9.96	1.10	Si
(5+6)-IV-1	1469374	64674	654208	10.12	1.10	Si
(5+6)-IV-2	1474455	77214	656469	8.50	1.10	Si
(5+6)-IV-3	1468704	77214	653909	8.47	1.10	Si
(5+6)-IV-4	1473784	64674	656171	10.15	1.10	Si
(5+6)-V-1	1470344	70795	654639	9.25	1.10	Si
(5+6)-V-2	1471235	73108	655036	8.96	1.10	Si
(5+6)-V-3	1471923	73108	655342	8.96	1.10	Si
(5+6)-V-4	1472814	70795	655739	9.26	1.10	Si
(5+6)-VI-1	1469857	70326	654423	9.31	1.10	Si
(5+6)-VI-2	1472827	72654	655745	9.03	1.10	Si
(5+6)-VI-3	1470331	72654	654634	9.01	1.10	Si
(5+6)-VI-4	1473301	70326	655956	9.33	1.10	Si
(5+6)-VII-1	1470028	67277	654498	9.73	1.10	Si
(5+6)-VII-2	1471552	76307	655177	8.59	1.10	Si

Comb.	N	Hd	R	CS.	CSd	ver
(5+6)-VII-3	1471606	76307	655201	8.59	1.10	Si
(5+6)-VII-4	1473131	67277	655880	9.75	1.10	Si
(5+6)-VIII-1	1468802	66486	653953	9.84	1.10	Si
(5+6)-VIII-2	1473882	75611	656215	8.68	1.10	Si
(5+6)-VIII-3	1469276	75611	654164	8.65	1.10	Si
(5+6)-VIII-4	1474356	66486	656426	9.87	1.10	Si

Francolise lì, gennaio 2018

Il progettista

Ing. Francesco COLARULLO